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The pre-depositional history of the Applecross Formation, Northwest Highlands, Scotland.

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BSc (Hons)



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Abstract

The provenance of Applecross Formation sedimentary rocks (Torridon Group, Northwest Scotland) is a topic of significant debate owing to difficulties in clearly correlating various datasets for the region (detrital mineral studies, sedimentology, and palinspastic restorations) to create an accepted palaeogeographic reconstruction. This study aims to elucidate the source area of Applecross sedimentary rocks and modes of deposition and transportation.

LA-ICP-MS ²⁰⁶Pb/²³⁸U dating of detrital zircon samples from various stratigraphic levels within the Applecross Formation type area is utilised to assess variations in the source over time. Sampling is spread through ~2000m of stratigraphy, along a ~15km outcrop parallel transect between Applecross and Loch Kishorn. Data reduction is undertaken using Iolite data reduction software.

U-Pb detrital zircon peaks of Mesoproterozoic (1280-1520Ma) and late Palaeoproterozoic (1680-1980Ma) age are dominant throughout the Applecross Formation. Minor early Palaeoproterozoic (2191-2265Ma) and Archean components up to 3346±43Ma are present. These data are in broad agreement with detrital zircon data from elsewhere in the Applecross Formation presented by Rainbird, Hamilton and Young (2001) and Krabbendam et al. (2017), suggesting a uniform input of well mixed sediment from a single source. Terranes in the foreland basin of the Grenville Orogen are favoured as source areas, with transport in an orogen axial foreland trunk system. Detrital Zircon U-Pb geochronology is combined with sedimentological context to determine depositional style. Deposition is interpreted to occur in a large scale distributive system similar to the Okavango Delta, Botswana, with unconfinement occurring during an extensional phase of the Grenville Orogen associated with rotation of Baltica relative to Laurentia at the time of deposition (see Rivers, 1997; Cawood et al., 2007). This proposal correlates known detrital mineral and sedimentological datasets. Further work is required to support the model; additional detrital zircon datasets are required to confirm the validity of a single sediment input. Further evidence for localised extension in the Applecross region is required to substantiate unconfinement of an established foreland trunk river system.

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Author's Declaration

I declare that except where explicit reference is made to the contribution of others, that this thesis is the result of my own work and has not been submitted for any other degree at the University of Glasgow or any other institution.

Samuel John Holmes

Chapter 1 Introduction

The Torridon Group of Northwest Scotland forms the dramatic mountains and landscapes of the Scottish seaboard. The group is a sedimentary succession divided into four formations: the lowermost Diabaig Formation at the base of the sequence, overlain by the coarser Applecross and Aultbea Formations (classified as a single formation by Stewart, 2002). The Torridon Group is overlain by the Cailleach Head Formation. The Torridon Group was deposited by a number of fluvial processes in a pre-vegetation landscape; understanding the context of these processes is key to interpreting the landscape of the Mesoproterozoic. This study will focus on elucidating the source area of the Applecross Formation, which is the most extensive formation within the Torridon Group.

The source area of the Applecross Formation sandstones is a matter of debate. Numerous proposals have been made in an effort to elucidate the proximity and age of potential basement and supracrustal sources; in spite of this, it is difficult to bring the available evidence together in a unifying theory as several datasets appear to contradict each other. The style of transport and deposition are also a key topic of discussion. Ongoing collection of palaeocurrent data frequently leads to new proposals concerning the regional structure of the Applecross Formation. For example, it is unclear whether structures such as the Cape Wrath Megafan (see Williams, 2001) represent isolated features within braidplain settings or exposed remnants of a broader belt of alluvial fans as subsequent datasets lend support to different settings.

Understanding the precise nature of the Applecross Formation will provide insight into the relationship between ongoing fluvial styles and processes in modern landscapes and those in ancient, pre-vegetation fluvial systems. Such understanding has implications for our understanding of processes in remote locations and potential applications in the search for liquid water on other planets.

1.1 Objectives

This study aims to clarify the provenance of the Applecross sandstones and the style of their deposition. This is to be achieved through production of a new and

extensive U-Pb detrital zircon dataset, covering both a range of stratigraphic levels within the Applecross Formation and a geographic transect within the formation type area at Applecross; these will be compared with previous lowquanta datasets for the formation from Rainbird, Hamilton and Young (2001) and Krabbendam *et al.* (2017).

Detrital zircon U-Pb data will be used to establish possible basement sources for the Applecross Formation. To further elucidate the source, this study will assess previous proposals of both source area and fluvial regime. Potential sources will be further constrained by extant sedimentological evidence from previous authors. This study will attempt to unify geochronological and sedimentological evidence to determine the most likely source of sediments for the Applecross Formation and the processes of deposition.

1.2 Setting

The outcrop of the Applecross Formation extends for ~200km through the Northwest Highlands of Scotland (Figure 1) forming a high relief landscape with abundant exposure (Figure 2). The Applecross Formation alone is ~3500m thick, however Stewart (2002) supports reclassification of the Aultbea Formation as part of the Applecross Formation providing a total thickness of ~4500m (See Figure 3). The vertical extent of exposure provides opportunity to assess the stratigraphy of the formation directly in the field. The Applecross Formation is largely homogenous, consisting of coarse arkosic sandstones with a varied pebble suite (see Moorbath, 1969; Williams and Foden, 2011,Table 2, section 3.2.2); occasional mud clasts also occur.



Figure 1: Extent of Torridonian outcrop in Northwest Scotland. After (Rainbird, Hamilton and Young, 2001; Krabbendam *et al.*, 2017). The Torridon Group is confined to the Northwest Highlands west of the Moine Thrust zone, lithologies extend into the Minch basin to the west.



Figure 2: Photograph of Creag a Chumhaing taken from grid reference OS428, 7944 4120. Viewing direction 154°. Creag a Chumhaing lies in the Applecross type area near Loch Kishorn. Exposure of this type is typical of the Applecross type area and localities further north in mainland Scotland.

The Applecross Formation underwent early diagenesis between 994±48Ma and 977±39Ma (Turnbull, Whitehouse and Moorbath, 1996), placing a minimum age of deposition at ~980Ma. During this period Northwest Scotland formed a promontory on the edge of the Laurentian craton, which formed the core of the supercontinent Rodinia (Pisarevsky *et al.*, 2003; Cawood *et al.*, 2007, 2010; Bingen *et al.*, 2008; Li *et al.*, 2008; Rainbird *et al.*, 2017). At the time of deposition Laurentia and Baltica (Scandinavian craton) were undergoing a complex accretion and collision process involving rotation of Baltica around Laurentia and several periods of extension (Rivers, 1997; Cawood *et al.*, 2007), see Figure 4. Accretion of Rodinia lead to the formation of the extensive Grenville-Sveconorwegian Orogen along the southern boundary of Laurentia and Baltica; it is likely that the Applecross Formation, although not influenced by Grenville Orogen.

The Applecross Formation was deposited on a Lewisian palaeolandscape. Since the 1800's, the palaeoclimate at the time of deposition has been interpreted as warm and semi-arid, on the basis of abundant red sandstones; however midpalaeolatitudes (30°-40°S) and a position closer to the Laurentian interior may have provided a cooler, more temperate setting (van de Kamp and Leake, 1997; Owen and Santos, 2014).



Figure 3: Simplified schematic stratigraphy of the Torridon Group. After (Selley, 1965; Stewart and Donnellan, 1992; Rainbird, Hamilton and Young, 2001; Williams, 2001; Stewart, 2002; Krabbendam, Prave and Cheer, 2008; Williams and Foden, 2011; Krabbendam *et al.*, 2017). The Torridon Group is deposited directly onto a Lewisian landscape, with formations such as the Diabaig varying significantly in thickness. (Stewart, 2002). The Applecross Formation overlies the Diabaig. Some workers (Stewart, 2002) have proposed that division of the Applecross and Aultbea is a misclassification, preferring to interpret them as a single formation. Both the Applecross and Aultbea Formations vary greatly in thickness, with estimates of thickness for the Aultbea ranging from ~500m to ~2000m; subsequently the thicknesses displayed are intended to be representative of the maximum thickness and may not resemble specific localities. The Cailleach Head Formation tops overlies the Aultbea Formation, in the study area (Applecross Peninsula) the formation is unseen. Further north the Cailleach Head Formation is overlain unconformably by the Eriboll Formation (Stewart, 2002; Krabbendam *et al.*, 2017).

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Figure 4: Relative positions of Laurentia and Baltica at (A) ~1200Ma and (B) during deposition of the Torridon. After (Li *et al.*, 2008; Cawood *et al.*, 2010; Williams and Foden, 2011; Krabbendam *et al.*, 2017; Rainbird *et al.*, 2017). Between 1200Ma (A)-980Ma (B) Baltica rotated around and in relation to Laurentia. This complex rotation may have facilitated periods of localised extension coeval with deposition of the Torridon Group.

1.3 Detrital zircon geochronology

The robust nature and high crystallization temperature of zircon render the mineral resilient to weathering processes and erosion. Zircon is able to survive multiple cycles of deposition and reworking, after initial removal from magmatic or metamorphic basement sources. Uranium commonly replaces zirconium in the crystal lattice of zircon. The combination of these features render zircon an excellent chronometer for provenance studies. By generating detrital zircon U-

Pb datasets over different levels in the Applecross Formation, variations in the source over time can be measured and comparisons may be drawn between zircon age clusters and terranes of relevant age. Comparison of conclusions from geochronological provenance studies with known sedimentological context and palaeogeographic reconstructions allows for robust determination of possible source areas.

1.4 Previous work

Current understanding of the Applecross Formation and related units has been developed by numerous authors, particularly since the 1960's with the advancement of detrital mineral studies.

Williams (1966) identified broadly northwest to west-northwest radial palaeocurrents in the Applecross Formation, interpreting these as the product of two large coalescing alluvial fans deposited at the foot of a retreating mountain front to the immediate northwest. Sediments were interpreted to be sourced from weathered Lewisian basement within the retreating belt (Williams, 1966).

Later analysis of palaeocurrents and sedimentology in the Applecross Formation revealed the presence of large scale bar structures (Nicholson, 1993) interpreted as the product of large scale rivers present alongside the fan deposits. A greater degree of variability in palaeoflow than previously recognised suggests that regional flow vectors may not support fan formation throughout the Applecross Formation (Nicholson, 1993). Nicholson (1993) instead supports deposition in a broader extensional basin setting, without active basin bounding faults, with sediment supplied by rivers over 500km in length.

Further evidence and constraints for a distal Applecross source area are provided by detrital zircon analysis (Rainbird, Hamilton and Young, 2001). Detrital zircon data support a source area in the foreland of the Grenville Orogen. Deposition by a northeast flowing foreland trunk river system axial to the Grenville Orogen is proposed (Rainbird, Hamilton and Young, 2001), supporting the distal fluvial setting of Nicholson (1993). Any northeast flowing trunk river system would be required to turn approximately east or southeast to generate the observed palaeocurrents in the Applecross Formation (Figure 5).



Figure 5: Alteration of flow direction in distal channels. Trunk river systems flowing to the northeast would require a significant change in direction to provide the palaeocurrents seen in the Applecross Formation outcrop.

The presence of a large scale alluvial fan with an overall east-directed flow is confirmed by extensive palaeocurrent analysis at Cape Wrath (Williams, 2001). In light of evidence for large scale rivers (Nicholson, 1993) Williams (2001) proposes deposition of the Applecross Formation in two main stages;

- Deposition of the ~50km diameter Cape Wrath Megafan, following uplift of an adjacent source area to the northwest;
- 2. Deposition of the southern Applecross Formation in a braidplain setting at the distal end of alluvial fans, following uplift of the source area further to the southwest.

The proposed proximal source area may have reached up to 250km west from the Outer Hebrides, with uplift occurring along the line of the Minch Fault or Outer Hebrides Fault Zone (OHFZ) (Williams, 2001) supporting a syn-depositional extensional setting.

Previous interpretations of the Applecross Formation as the result of deposition in an extensional basin are refuted by Kinnaird *et al.* (2007). Kinnaird *et al.* (2007) interpret the Applecross Formation as a non-marine molasse deposited by distal river systems and genetically unrelated to the adjacent Sleat and Stoer Groups.

Williams and Foden (2011) attempt to create a compromise model between detrital mineral datasets and local stratigraphic and palaeocurrent evidence, as some distal source proposals are not compatible with palaeocurrents observed in the Applecross Formation. A supracrustal series overlying the Lewisian to the west-northwest is proposed as the source area, with minimal contributions from the local Lewisian basement (Williams and Foden, 2011). The setting is proposed to be extensional with sediment filling the basin laterally from the relatively uplifted proximal source area (Williams and Foden, 2011). In response, Krabbendam and Rainbird (2012) refute the proposal of a proximal supracrustal source area citing a lack of evidence for such an outcrop, or for movement of appropriate age along the Minch Fault.

Owen and Santos (2014) support both a distal source and a distributive setting in a study of soft sediment deformation within the Applecross Formation. Ielpi and Ghinassi (2015) detail the drainage patterns of the Applecross Formation at the Stoer Peninsula, identifying low sinuosity braided rivers with well-defined but rarely preserved levees and abundantly preserved bar sheets. Evidence for discharge cycles is presented and the potential for distal transport in the Applecross Formation fluvial system supported.

Further detrital zircon studies constrain potential extant source areas to the proximal Canadian sector of the Grenville Orogen (Krabbendam *et al.*, 2017), which represents a distal source to the southwest. Distal transport in a trunk river system is supported (Krabbendam *et al.*, 2017), however transport to the northeast remains unjustified to the observed east-southeast palaeocurrents in the Applecross Formation.

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The proposals outlined are difficult to rectify with each other as strong evidence for a Grenvillian source area is presented, however few proposals attempt to explain the difference between observed flow vectors (southeast) and the proposed direction of travel from the source area (northeast). A robust determination of the setting and regional fluvial style within the extant Applecross outcrop is required to understand the palaeogeographic relationship between the sediments and their source, and subsequently to provide better context to the Applecross Formation.

In this thesis, new detrital zircon samples from the Applecross Formation are collected and prepared. Zircon grains are separated from sandstones through conventional crushing, washing, and density separation techniques prior to hand picking and mounting of grains in resin. Cathodoluminescence (CL) images of polished grains are produced using the ISAAC (Imaging Spectroscopy and Analysis Centre) SEM at the University of Glasgow. New LA-ICP-MS (Laser Ablation-Inductively Coupled Plasma-Mass Spectrometry) U/Pb ages for the Applecross Formation are presented (see Chapter 3, Results) and discussed (see Chapter 4, Discussion) in order to clarify the source of Applecross sedimentary rocks and their mode of deposition (see Chapter 5, Conclusions).

1.5 Rodinia configuration

Deposition of the Torridon Group occurred between 994±48Ma and 977±39Ma (Rb-Sr whole rock study of lower and middle Torridonian respectively, Turnbull, Whitehouse And Moorbath, 1996; Rainbird, Hamilton And Young, 2001). The unconformably underlying Stoer Group is interpreted to be significantly older (1199±70Ma; e.g. Turnbull, Whitehouse and Moorbath, 1996, ~1180Ma from Stewart, 2002). The unconformity represents a time interval of 200-300Ma between 1177-994Ma (Williams, 2001).

In order to understand the depositional setting and provenance of the Applecross Formation (Torridon Group), it is important to consider the configuration and tectonics of the supercontinent Rodinia, widely believed to have incorporated the majority of continental plates at the time of deposition of the Torridon Group (Rivers, 1997; Rainbird *et al.*, 1997, 2017; Dalziel, Mosher and Gahagan, 2000; Rainbird, Hamilton and Young, 2001; Pisarevsky *et al.*, 2003; Cawood *et al.*, 2007, 2010; Bingen *et al.*, 2008; Li *et al.*, 2008; Williams and Foden, 2011; Krabbendam *et al.*, 2017). Precise continental configuration varies between authors, however the Laurentian craton is commonly placed near the core of Rodinia, on the basis of evidence for late Neoproterozoic passive margins around the craton (see Bond, Nickeson and Kominz, 1984; Pisarevsky *et al.*, 2003; Davidson, 2008), (See Figure 6, Figure 7).

In previous provenance studies of the Torridonian two primary models for the relative position of the Laurentian and Baltican cratons have been utilised (Figure 7). Williams and Foden (2011) utilise models after Li *et al.* (2008) and Cawood *et al.* (2010) positioning Baltica adjacent to Greenland and Amazonia at the time of deposition (Figure 7A). This configuration supports an oroclinal configuration for the Grenville Orogen when correlated with the Sveconorwegian Orogen in Baltica, passing near or through the southern parts of Scotland and Ireland (present position), see (Pisarevsky *et al.*, 2003; Piper and Darabi, 2005; Cawood *et al.*, 2007; Bingen *et al.*, 2008; Li *et al.*, 2008; Williams and Foden, 2011; Krabbendam *et al.*, 2017).



Figure 6: Cratonic layout of supercontinent Rodinia. After (Pisarevsky *et al.*, 2003). Possible reconstruction of the supercontinent Rodinia at 990Ma, coeval with deposition of the Applecross Formation. Grey bands display orogens of Grenvillian age.

This study is primarily concerned with the nature and provenance of Applecross Formation sediments in the Torridon Group; subsequently only the immediately relevant cratons are discussed further, namely Laurentia, Baltica, and Amazonia (see Figure 6, Figure 7).

Reconstructions of Rodinia at the time of deposition of the Stoer Group (~180Ma prior to deposition of the Applecross and associated formations, Williams and Foden, 2011) position Baltica widdershins of its late Mesoproterozoic position relative to Laurentia (see Figure 7A) (Li *et al.*, 2008; Cawood *et al.*, 2010). Krabbendam *et al.*, (2017) utilise a less drastically oroclinal model of the Grenville Orogen (Figure 7B) to establish a provenance for the Sleat Group. Although this layout for the orogen and resultant foreland provide a good fit with the Sleat and Morar (correlated with the lower Torridon in Krabbendam *et al.*, 2017) palaeocurrents, no explanation is given for the discordance of Applecross Formation palaeocurrents with the north easterly flowing orogen axial trunk river system proposed by Krabbendam *et al.* (2017). Applecross Formation palaeocurrents support a flow direction to the southeast (Gracie and Stewart, 1967; Nicholson, 1993; Williams, 2001; Owen and Santos, 2014; lelpi

and Ghinassi, 2015). In an oroclinal setting taking into account the clockwise rotation and movement of Baltica relative to Rodinia between 1265-1000Ma (Cawood *et al.*, 2010), an orogen axial foreland basin may facilitate southeastward flow during the deposition of the Applecross Formation whilst preserving northeastward flow into the earlier Sleat Formation.



Figure 7: Schematic continental configuration of Laurentia, Baltica, and Amazonia. After (Li *et al.*, 2008; Cawood *et al.*, 2010; Williams and Foden, 2011; Krabbendam *et al.*, 2017; Rainbird *et al.*, 2017) Comparison of the continental layouts adopted by different authors. **A)** Configuration adopted by this study displaying Laurentia, Baltica and Amazonia in their positions ~950-1000Ma, coeval with Torridonian deposition. **B)** After (Krabbendam *et al.*, 2017; Rainbird *et al.*, 2017). Configuration displaying Laurentia and Baltica in their earlier Palaeoproterozoic positions. Blue lines indicate the approximate position of Grenville-Sveconorwegian fronts, red arrows indicate broad flow directions of possible orogen axial rivers entering the Torridonian (highlighted).

Within Laurentia, a variety of fluvial systems and source areas for the Torridon Group have been proposed. An extensional half graben setting invoking a supracrustal source overlying a previously uplifted Lewisian terrane along the western margin of the Minch is supported by Stewart and Donnellan (1992) and Williams and Foden (2011). This proximal source is based on palaeocurrents within the Torridon Group, indicating the presence of a megafan ~50km wide with an apex ~30km west of the Scottish mainland in the Cape Wrath member at the norther end of the exposure (Williams, 2001; Williams and Foden, 2011). The southern end of the basin is in this model filled laterally by braidplain deposits suggested to represent the distal deposits of a series of alluvial fans further west (Williams, 1969; Williams, 2001; Williams and Foden, 2011), although Nicholson (1993) refutes the presence of alluvial fans in the southern exposures of the Torridonian.

Alternative viewpoints include those of Rainbird, Hamilton and Young (2001) and Krabbendam *et al.* (2017) who support distal sediment transport in an orogen axial trunk river system from a distal source. This model is supported by evidence for pan-continental river systems across Laurentia (Rainbird *et al.*, 1997) distributing detritus from the Grenville Orogen to basins throughout Laurentia (see Krabbendam *et al.*, 2017). This fluvial system provides transport broadly to the northeast relative to the present position of the Torridonian, however transport direction may have varied with local structure and tectonics.

1.6 Grenville configuration and basements

Palaeocurrents within the Applecross Formation indicate transport from Laurentia in the west (south east palaeocurrents, see Gracie and Stewart, 1967; Nicholson, 1993; Williams, 2001; Owen and Santos, 2014). The proximity of the source varies between authors, with grain abrasion supporting a more distal source for the Applecross than that of the Sleat and Stoer Groups (Rainbird, Hamilton and Young, 2001). In light of these suggestions, Laurentian basement and sediments are of key interest as potential source areas, particularly those of composition suitable to form the arkoses of the Applecross Formation (primarily quartzofeldspathic crystalline rocks and pre-existing sedimentary sequences). At the time of deposition of the Torridon Group, basement rocks and orogens from a broad range of time periods are present across Laurentia (see Figure 8). Archean cratons (<2500Ma are located across central Laurentia, Greenland, and the Rockall Plateau, as well as areas of Baltica to the east (Rivers, 1997; Li et al., 2008; Krabbendam et al., 2017; Rainbird et al., 2017). There is evidence for Early-mid Palaeoproterozoic orogens (2500-1900Ma) in southern Canada and the United States (present position), Rockall Plateau, and Baltica (Rivers, 1997; Li et al., 2008), with late Palaeoproterozoic belts occurring in adjacent areas (Rivers, 1997; Cawood et al., 2007; Li et al., 2008; Krabbendam et al., 2017; Rainbird et al., 2017). Rivers (1997) highlights major Palaeoproterozoic-Mesoproterozoic orogenic fronts in Laurentia (Figure 8b), which may have formed areas of relief during this period. Orogens within the 1820-1600Ma period are focused in southern Laurentia, with some occurences in Baltica (Figure 8A) (Krabbendam et al., 2017; Rainbird et al., 2017). The Makkovik-Ketilidian-Rhinian events (collectively referred to as the MKR) are found in southern Greenland and possibly on the Rockall Plateau (Rivers, 1997; Krabbendam et al., 2017; Rainbird et al., 2017). Emplacement of a granite-rhyolite belt into and onto pre-existing crust occurred between 1500-1300Ma in central Laurentia, concluding shortly before earliest for events preceding the Grenville Orogen (Rivers, 1997; Cawood et al., 2007; Li et al., 2008; Krabbendam et al., 2017; Rainbird et al., 2017). Crystalline rocks between 1300-950Ma occur in east Greenland and northern Laurentia (Figure 8) (Li et al., 2008). Mesoproterozoic AMCG (anorthositemangerite-charnockite granites) plutonic suites are found in eastern Canada (Rainbird et al., 2017). Arc related rocks between 1300-1100Ma are found on the rear side of the Grenville Orogen (Li et al., 2008) and subsequently are not of interest to this study. During the late Mesoproterozoic (1200-1100Ma) a midcontinent rift system developed in central Laurentia (Vervoort et al., 2007).

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Figure 8: A) Basement rock ages in Laurentia and Baltica. B) Orogens in Laurentia, C) Basement rock ages in East Canada. A) After (Rivers, 1997; Pisarevsky *et al.*, 2003; Li *et al.*, 2008; Cawood *et al.*, 2010; Krabbendam *et al.*, 2017), Basement and terrane ages in Laurentia and Baltica highlighting possible source areas for the Applecross detrital zircon suite. The location of the Torridon Group is highlighted adjacent to Baltica and Greenland. The approximate location of the Rockall Plateau is displayed northwest of the Torridon Group, between Greenland, Baltica and Laurentia B) After (Rivers, 1997). Major Terranes and orogens of Laurentia likely to have affected pan continental river systems. C) After (Rivers, 1997). Basement ages in the Canadian sector of the Grenville Orogen.

The Grenville Orogen occurred between 1080-950Ma across eastern Canada, the USA (present positions), Baltica (Sveconorwegian Orogen), and possibly Amazonia (Sunsas Orogen) (Figure 8 Pisarevsky *et al.*, 2003; Bingen *et al.*, 2008; Li *et al.*, 2008; Cawood *et al.*, 2010; Krabbendam *et al.*, 2017; Rainbird *et al.*, 2017). Numerous protolith suites are incorporated into the Grenville Orogen. These are outlined in Figure 8C (after Rivers, 1997; Krabbendam *et al.*, 2017). Rocks from the MKR (1820-1720Ma), trans-Labrador, and Matazal (1700-1600Ma), Pinwarian and granite-rhyolite province (1520-1380Ma), AMCG plutonic suite (1400-1300Ma), Elzevirian (1300-1200Ma), Shawingan and Adironian (1200-1100Ma) are incorporated into the proximal Grenville Orogen in eastern Canada (Rivers, 1997; Krabbendam *et al.*, 2017) along with some Archean material. As a result of this, it is possible for these protolith ages to appear in detrital zircon suites derived directly from the Grenville Orogen as only the core of the orogen is likely to reset or generate new zircon ages; an 'orogenic lid' preserves older material (Krabbendam *et al.*, 2017).

Cawood et al. (2007) note that prior to the final formation of Rodinia (~1200-1000Ma), Laurentian sedimentary basin fill is likely to be dominated by detritus from ongoing arc magmatism, adding that the final stages of collision (continentcontinent) will see more detritus derived from reworking of older material. This may contribute to the presence of sandstone pebbles containing detrital zircon of Grenvillian age within the Applecross Formation (Rogers et al., 1990; Williams and Foden, 2011). Pebbles from the Applecross Formation also yield detrital zircon ages of 2875-2628Ma, 1662-1625Ma, and 1193-1088Ma (Rogers et al., 1990; Williams and Foden, 2011), which are consistent with the peak ages from this study for the Applecross Formation itself. Moorbath et al. (1967) offer further K-Ar and Rb-Sr ages for pebbles from the Applecross Formation, with K-Ar fuschite-schist ages from 1654-1798Ma and various pebbles with Rb-Sr ages between 1524±50ma, 1516±40Ma, 1358±35ma, and 1275±40Ma. The varied pebble suite supports reworking of source material for the Applecross Formation. The similarity between Applecross pebble detrital zircon ages and detrital zircon ages from the sediment itself suggests similar sources or reworking of an older sedimentary formation directly related to the Applecross Formation- perhaps fluvial deposits lain down and later removed during the Sleat-Applecross unconformity.

During the construction of Rodinia a number of orogenic events occurred, creating relief across Laurentia. This topography creates an additional constraint on possible courses for fluvial systems during the Grenville Orogen and deposition of the Torridonian. Rivers (1997) outlines late Palaeoproterozoic collisional and accretionary orogenic fronts in Laurentia (see Figure 8B). The youngest of these fronts formed at least 600Ma prior to deposition of the Torridonian. The mid-continental rift system (MCR) in central Laurentia provides a possible western boundary more contemporary with the Torridon Group (1100-1090Ma, Rivers 1997) (Figure 8B), potentially constraining any orogen axial river system supplying the Torridonian to the eastern Grenvillian foreland (east Canada, present position). Beyond Laurentia, Baltica is undergoing rotation and collision with Rodinia during this period (Cawood et al., 2010) (Figure 7). This movement led to an accretionary event coeval with the end of, but disparate from, the Grenville/Sveconorwegian Orogen known as the Valhalla Orogen focussed around an ocean known as the Asgard sea between Laurentia, Baltica, and Amazonia (Cawood et al., 2010). Sedimentary successions within the Valhalla Orogen are approximately coeval with Torridonian deposition, occurring between 1030-980Ma and 910-870Ma (Cawood et al., 2010).

1.6.1 Rockall Plateau

The Rockall Plateau is a microcontinent isolated during the opening of the lapetus and Atlantic oceans (Roberts *et al.*, 1970; Roberts, Ardus and Dearnley, 1973) (Figure 8A). Intermediate granulites of Grenvillian age (987±5Ma) (Miller, Matthews and Roberts, 1973) and Precambrian acid granulites (Roberts, Ardus and Dearnley, 1973) have been recovered from Rockall Bank, indicating a continuation of Lewisian lithologies beyond the Outer Hebrides and extension of Grenvillian metamorphism as far as southern Rockall.

A number of early Neoproterozoic deposits containing Grenvillian detritus are highlighted in Figure 8B (after Krabbendam *et al.*, 2017). These deposits provide evidence for large scale continental river systems, such as those discussed by Rainbird *et al.* (1997, 2017); Rainbird, Hamilton and Young (2001); Krabbendam, Prave and Cheer (2008); Krabbendam *et al.* (2017). Rainbird *et al.* (1997, 2017) interpret these fluvial systems to transport material to the northwest across Laurentia with proximal deposits in the Middle Run basin and further east in the central Laurentian MCR. Subsequently the southeasterly Applecross palaeocurrents require a change in vector in fluvial systems in eastern Laurentia compared to those in western Laurentia, either by a change in direction or by presence of a disparate fluvial system in the Canadian sector of the Grenville Orogen, perhaps separated by the MCR.

Potential source areas of Grenvillian age incorporating older lithologies can also be found in the Sveconorwegian sector in Baltica (Figure 8A); sourcing the Applecross from this area however would require flow directions at 180° to those observed (approximately southeast in the Applecross Formation, see Gracie and Stewart, 1967; Nicholson, 1993; Williams and Foden, 2011; Owen and Santos, 2014; Ielpi *et al.*, 2017). In summary, the Sveconorwegian sector can be ruled out as a direct source.

1.7 Palaeocurrents and sedimentology

The Applecross Formation consists of largely homogenous arkoses with occasional mud clasts and a varied pebble suite (see Williams, 1966; Williams, 2001). Soft sediment deformation is seen throughout the formation, indicating a high sediment influx combined with a high water table (see Figure 24 section 3.2.2, Owen, 1995; Owen and Santos, 2014). Cross bedding has been observed in a variety of orientations (see Figure 25, section 3.2.2) and in many cases can be characterised as lateral accretion of bar deposits (Nicholson, 1993; Ghinassi and lelpi, 2017). Sandstones are typically channelised. Structures and lithologies indicate a fluvial system with high, possibly seasonal discharge and frequent avulsion typical of braidplain systems within the broader temporal framework of the Torridon Group.

1.7.1 Torridon Group setting

The Torridon Group coarsens upwards from locally derived fan and lacustrine deposits in the Diabaig Formation into higher energy braidplain and megafan deposits within the Applecross and Aultbea Formations, prior to an eventual reduction in energy and sediment supply within the Cailleach Head Formation (See Figure 3, section 1.2). This may reflect an increase in sediment influx

between the Diabaig and Applecross Formations (Stewart, 2002) as a result of increased relief or denundation of the source area.

Initial Applecross deposition occurs around 977±32Ma (Turnbull, Whitehouse and Moorbath, 1996), coeval with the later stages of the Grenville Orogen. This would create relief in suitable source areas to provide a high influx of sediment to the Torridon if a distal source is accepted. Extension related to an extensional phase of the Grenville Orogen along the Minch basin may also provide relative relief for a proximal source (Williams, 2001; Williams and Foden, 2011). Krabbendam and Rainbird (2012) note a lack of direct evidence for movement of this age along the Minch Fault; however this does not strictly preclude the possibility as later movements are likely to have obscured such evidence. Further work on the early movements of the Minch basin is required to clarify this argument. The settings and variations in style of each Torridon Group formation is discussed in further detail.

1.7.2 Diabaig Formation

The Diabaig Formation at the base of the Torridon Group is characterised by locally derived sandstones and breccias filling Lewisian palaeovalleys (Park *et al.*, 2002; Stewart, 2002). Breccias within the formation have been interpreted as wedges filling the valley sides, with shales forming in lacustrine settings on the valley floors (Park *et al.*, 2002). The upper section of the formation is characterised by sandstones displaying eastward palaeocurrents, taken to indicate the presence of Applecross style rivers (Park *et al.*, 2002; Santos and Owen, 2016).

1.7.3 Applecross Formation

The Applecross Formation comprises up to 4500m thickness of coarse sandstones, generally interpreted to represent braided fluvial deposits (Selley, 1965; Rainbird, Hamilton and Young, 2001; Williams, 2001; Stewart, 2002; Williams and Foden, 2011; Krabbendam *et al.*, 2017; Rainbird *et al.*, 2017). Palaeocurrents within the Applecross Formation dominantly support flow to the southeast (Gracie and Stewart, 1967; Nicholson, 1993; Williams, 2001; Owen and Santos, 2014; Ielpi *et al.*, 2017). The 450m thick Cape Wrath member supports this regional flow direction; the member has been interpreted as a megafan -50km wide with an apex -30km west of the Scottish mainland as opposed to the more distal braidplain facies seen further south in the formation (Williams, 2001; Williams and Foden, 2011). The Applecross Formation therefore shows multiple outcrop-lateral fluvial facies along its extensive outcrop. Williams and Foden (2011) suggest that the outcrop exposed today represents a diagonal transect of the original basin, interpreting the Cape Wrath member in the north to be proximal to the source (or basin edge) with braidplain deposits further south representing distal elements of the same system. In contrast to this interpretation of fans in the Applecross Formation Krabbendam and Rainbird (2012) argue that the Cape Wrath member represents an individual fan, facilitated by a localised obstacle. Eventual burial caused fan formation to cease. Palaeosols and weathering profiles within the Cape Wrath member suggest a warm, arid environment during deposition (Williams, 2001; Williams and Foden, 2011)

1.7.4 Aultbea Formation

The Aultbea Formation conformably overlies the Applecross Formation and similarly consists of arkosic sandstones with some grey shales (Williams and Foden, 2011). Some workers consider the separation of the Applecross and Aultbea Formations to be a misclassification, preferring them to be considered a single formation (Stewart, 2002). Palaeocurrents indicate that transport within the Aultbea Formation is similar to that within the Applecross Formation.

1.7.5 Cailleach Head Formation

The Cailleach Head Formation lies at the top of the Torridon Group. The formation consists of upward coarsening cyclothems including grey shales and red sandstones (Stewart, 2002) indicative of fluvial and lacustrine processes (van de Kamp and Leake, 1997).

Chapter 2 Methodology

2.1 Preliminary fieldwork and sample collection

2.1.1 Study area

This study focuses on the Applecross Peninsula, south of Loch Torridon. Sampling was undertaken entirely within the Applecross Formation, along a transect of ~12.5km between Loch Kishorn and Applecross Bay (see Appendix 1).

The sample area was selected on the basis of its proximity to the Moine Thrust, extensive outcrop of a single formation, and accessibility. Additionally information on local lithology pertinent to the study was reviewed from the literature (see Thomson *et al.*, 1999; Piper and Darabi, 2005; Persano *et al.*, 2007; Hudson, 2011; Ellis *et al.*, 2012; Krabbendam *et al.*, 2017). In the field, a stratigraphic log was constructed to provide further context to the area.

2.1.2 Sampling regime

Sampling outcrops were chosen on the basis of field observations and scatter along the transect. Ideal sampling localities contain coarse immature sandstones that include cross bedding structures or heavy mineral laminae. At localities where no such outcrop exists an increased sample size of finer, more mature rock was collected to increase the probability of finding suitable apatite and zircon crystals. Samples were collected in-situ from outcrop only.

When collecting samples, the outcrop was first photographed; key features were noted including hand specimen descriptions and measurements. Localities were numbered in order of visit, with both OS grid references and latitude/longitude noted. Additionally GPS systems were used to mark localities and create a map of ground covered for reference. Collected samples were labelled according to locality of collection and whole rocks cleaned prior to processing.

2.2 Laboratory protocol

2.2.1 Mineral separation

2.2.1.1 Crushing

Samples were initially described in hand specimen prior to being broken up by percussion and with a hydraulic rock splitter. Samples were next passed through coarse then fine jaw crushers until only sand remains. All equipment was cleaned thoroughly between samples to prevent contamination.

2.2.1.2 Washing

Crushed samples were washed to remove clay and other light minerals. Each sample was placed in a bucket with clean water. The sample was agitated until the lightest minerals become suspended in the water column. Water was carefully poured off and the process repeated until light minerals cease to become suspended.

Washed samples were placed in labelled trays in a low temperature oven to dry overnight. Dry samples were taken for sieving.

2.2.1.3 Sieving

Single grains of apatite and zircon were required for analysis; as such each sample was sieved to separate a sub 500 µm fraction. Remaining coarse material was labelled and stored, or crushed and washed again if too small a fraction was recovered. Between samples sieves were carefully cleaned to remove all lodged grains from the gauze.

2.2.1.4 Magnetic separation

As apatite and zircon were non-magnetic, magnetic minerals were removed from the samples. Magnetic separation was performed in two stages to prevent apparatus from clogging.

Vertical magnetic separation: Samples were first placed into a vertical Frantz magnetic separator calibrated to divide material into two streams of magnetic

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and non-magnetic material. Efficient separation was achieved by adjustment of magnet strength and distance of the sample from the magnet. Samples were stored in a hopper at the top of the equipment and a stream of material moved past the magnet by gravity (see Figure 9A). The non-magnetic material falls under the influence of gravity and lands in a container below the hopper. Magnetic material was pulled towards the magnet as it falls, creating the second stream of material, landing in a collection pot below the magnet. The magnetic material was labelled and stored. Non-magnetic material was labelled and sent for horizontal magnetic separation.



Figure 9: Frantz magnetic separators. A) Vertical magnetic separator. Samples were stored in the hopper visible at the top of the equipment. Samples fall past the magnet and were separated into two streams; magnetic material was pulled towards the magnet and was collected in the black container. Non-magnetic material simply falls under the influence of gravity and was collected in the grey container.

Horizontal magnetic separation: Vertical separation removes only the most magnetic grains, such as magnetite, due to the high rate of flow. The remainder of the magnetic material was removed by passing the sample through a horizontal Frantz magnetic separator. Samples were placed in a hopper that releases a steady stream of material into the separation track, which runs through the magnet and was separated, along its length, into two parts by a ridge (see Figure 9B). The track was tilted at a shallow angle so that gravity counteracts the magnetic force. Magnet strength and track angle must be calibrated for each sample. The magnetic material was attracted by the magnet and therefore was directed into the section of the track nearer to the magnet; the non-magnetic material was pulled down the slope to the lower track, further from the magnet, by the influence of gravity. Each fraction was collected in a container at the end of the track; magnetic material was labelled and stored. Non-magnetic material was sent for density separation.

2.2.1.5 Density separation

Remaining samples contain a small amount of zircon and apatite compared to a large bulk of quartz and other light minerals. Zircon and apatite are heavy minerals (~3.93-4.73 g/ml and ~3.16-3.23 g/ml respectively) in comparison to quartz (2.65 g/ml). Lithium heteropolytungstates (LST) separating fluid has a density of 2.8±0.02g/ml, falling between the heavy and light mineral groups present in the samples. Each sample was placed into a separating funnel and suspended in LST. Samples were stirred gently for 30 minutes to allow light and heavy grains to move past one another and to avoid flocculation. Samples were next allowed to settle until a clear divide was seen between the heavy and light sections. Heavy minerals were then poured out of the funnel, filtered from the LST and cleaned using deionised water. Light minerals were labelled and stored. Heavy minerals were placed into sample vials and labelled for assessment of apatite and zircon content.

2.2.1.6 Sample assessment, picking, and mounting

The remaining sample fractions contain a relatively pure separate of zircon and apatite. To confirm this each sample was assessed for zircon and apatite abundance under a reflected light picking microscope. Zircons are typically recognised by their rectangular cross section and overall cuboid shape, with prismatic tips on intact crystals. Apatites are typically recognised by their hexagonal cross section and flat tips, giving them a "barrel like" appearance. Additionally, zircons have a high relief while apatites possess a lower relief; subsequently zircon can appear to have a sharper border when viewed under the picking microscope. Relief was used to assist identification where grains were damaged and therefore difficult to distinguish through morphology. During this phase different populations of zircon and apatite were identified; each population must be sampled to ensure accurate interpretation of data.
Grains were picked directly onto mounting slides. A strip of double-sided adhesive tape was applied to a glass slide, and washers applied to this tape. Grains were picked from the sample and applied directly to the adhesive tape within the washers, a method developed at the University of Glasgow (Figure 10). Grains were arranged in a grid pattern where possible to improve ease of location during analysis.



Figure 10: Grain mount preparation. In preparation for grain mounting double-sided adhesive tape was applied to a glass slide. The adhesive tape serves a dual purpose; firstly it allows the washer to be attached to the slide to contain resin later in the preparation of the sample mount. Secondly, the adhesive tape allows picked grains to be arranged in an ordered grid without risk of any grain becoming dislodged or loose. Grains in this sample are small; however the grid can be made out within the far portion of the washer.

Once slides have been filled with a given set of grains a two part epoxy resin was mixed. The resin must be mixed well in equal parts to ensure a clear glass-like finish. The epoxy was stirred gently to prevent the inclusion of gas during mixing, as any bubbles will tend to stick to grains. This leads to loss of grains during polishing as the resin will not adequately hold them. Once mixed the resin was poured into the washers. A sheet of plastic was placed over the washers to prevent adhesion and a glass plate placed on top. Weight was applied to the top of the plate to compress the resin into the washers and prevent the formation of bubbles. Once the resin has set (after ~2-3 days) the washers were removed from the glass slides. The washer was cut away from the resin disk containing the grains. The disk and grains were polished incrementally with p1200, p2500, and p4000 grinding paper. p800 paper was unnecessarily coarse and causes loss of grains from the disk face. Disks were finished with a 1 μ m and 0.3 μ m aluminium oxide solution providing a suitable surface for SEM imaging and laser ablation.

Between and after each stage of polishing, disks were washed in and ultrasonic bath for 30 seconds to remove any residual grit or aluminium oxide. Additionally the grinding paper was cleaned with distilled water between polishing to remove any loose grains. Once polishing was complete reference points *A*, *B*, and *C* were marked on three corners of the grid to orient the disk when viewing grains (Figure 11).



Figure 11: Completed grain mount. Polished and grain mount for SA10. The copper disks visible are labelled *A*, *B*, and *C*. Each disk includes a grid with the respective letter at the centre, and a larger letter on the rim. The letters and grids can be used to orient the grain mount and were used as reference points when producing spot coordinates for analysis.

2.2.2 Analysis

2.2.2.1 SEM cathodoluminescence and secondary electron imaging

Once polished, each sample disk was cleaned in an ultrasonic wash and methanol to remove all excess polishing powder and fingerprints. Cleaned samples were carbon coated to improve electron flow during imaging with the scanning electron microscope (SEM).

Imaging was undertaken at the Imaging Spectroscopy and Analysis Centre (ISAAC) at the University of Glasgow utilising the FEI Quanta 200F environmental SEM.

Samples were imaged using both a panchromatic cathodoluminescence detector and secondary electron detectors. This allowed analysis of zoning, inclusions, and the topography of the polished sample to ensure suitable ablation sites can be selected for LA-ICP-MS analysis (see Figure 12). Samples SA2, SA3.1, SA4, SA5, SA7, SA8, SA10 and SA21 were selected for analysis on the basis of sample size and geographic spread across the study transect. 50-100 zircons from each sample were imaged.



Figure 12: CL (Cathodoluminescence) and SE (Secondary Electron) images, sample SA_10_0915. Zircon SA10_0915 cathodoluminescence (CL) image with composite CL and secondary electron image (mix). 20µm spots 1 and 2 were marked for laser ablation analysis in distinct compositional zones. Ideally a third spot would be placed in the bright rim of the crystal at the right of the image, however the zone was too small. Radial fractures in the crystal suggest a greater concentration of uranium in the crystal rim.

Cathodoluminescence images show the internal structure of zircon (Figure 12). Assessment of the internal structure of each zircon to be analysed were made in order to choose sites for analysis which would not be contaminated by inclusions, radiation damage, or ablation of multiple zones.

2.2.2.2 Sample mapping

The locations of laser targets selected in section 2.2.2.1 were mapped to provide targeting coordinates for the laser. Sample mounts were fixed to a glass slide and placed under a Zeiss Axioplan 2 imaging microscope. The microscope stage was controlled by a joystick and spots were logged using FTStage software. Reference points at *A*, *B*, and *C* were marked first for future alignment of the grain mount (see 2.2.1.6). Ablation points were then marked in numerical order. Spot labels and numbers were entered into a database created to contain the data (see Appendix 2). The database was used to verify that spot numbers

provided by the FTStage application were in the correct sequence. Completed coordinate files were saved in .CSV format to be imported into the laser control software.

2.2.3 Laser Ablation-Inductively Coupled Plasma-Mass Spectrometry (LA-ICP-MS)

LA-ICP-MS analysis combines laser ablation (LA) systems with inductively coupled plasma-mass spectrometry (ICP-MS) to enable sampling and analysis of individual zones within individual crystals using spots or time resolved transects of multiple zones by ablating along a line (Figure 13). Material ablated from the sample by the laser was transported to the mass spectrometer by a carrier gas. Analysis was undertaken using a RESOlution SE laser ablation system in combination with the iCAP RQ ICP-MS system.



Figure 13 Cathodoluminescence image of zircon SA2_0004 (this study). A) 30µm spot targeting a single zone at the core of the zircon. When analysing single spots corrections for downhole fractionation are required. B) 30µm wide line to analyse multiple zones continuously. This method was applied where spatial variations in composition were of interest.

2.2.3.1 Laser setup

Samples for analysis were mounted in a holder (Figure 14) with Plesovice Zircon standards and NIST 610 glass (see section 2.2.3.3). Samples were adjusted to ensure consistent orientation and height in the holder. A scanned image of the sample holder was created for reference during analysis.



Figure 14: (A) Sample holder for use in LA-ICP. (B) Sample loading procedure for LA-ICP. (A) Samples were mounted in each of the holes visible in the holder, which was then scanned using a conventional scanner to produce a reference image containing the location of each sample. (B) Once the sample holder has been prepared it was loaded into the ICP-MS ablation chamber for analysis.

Once the samples were mounted in the holder, the sample exchange sequence was begun. The sample chamber was drained of carrier gas and the subsequent vacuum re-pressurised. The sample holder was mounted in the sample chamber and the hatch sealed. The vacuum within the chamber was re-established and the chamber backfilled with carrier gasses. The scanned image of the sample holder was aligned with the live microscope feed allowing easy location of individual disks.

Analysis sequences for the laser were created by importing previously prepared .CSV files for each sample (2.2.2.2). Additional laser spots were added to each sequence for NIST and Plesovice standards at the beginning and end of each analysis, with one measurement of each for every five samples.

Single spot analysis with a 30µm spot diameter was used to target individual zones while minimising downhole fractionation effects (Diwakar *et al.*, 2014). A fluence of 4.5J.cm⁻² was found to effectively ablate sampled zircon with a 3.0Hz repetition rate.

2.2.3.2 ICP-MS setup

During analysis the ICP-MS receives material ablated by the LA system and measures a pre-selected set of atomic weights relating to the isotopes required.

²⁰⁴Pb (common lead) was measured to correct for any non-radiogenic lead in the sample. ¹⁹⁸Hg was measured to correct for interference, to verify that there was no magnesium in the sample and therefore any 204 isotopes found are ²⁰⁴Pb.

*²⁰⁶Pb and ²³⁸U, *²⁰⁷Pb and ^{235U,} *²⁰⁸Pb and ²³²Th ('*' indicates radiogenic origin) are the parent-daughter end members of their respective radioactive decay chains and all were measured to provide accurate U-Pb ages from the analysis.

2.2.3.3 Standards

Appropriate standards were vital to monitor the production of accurate and reliable data for analysis. The use of multiple standard materials improves integrity as internal standards of known composition can be used to calibrate analysis, and natural zircon standards of known age can be used to test the accuracy of the analysis.

The LA-ICP-MS system was tuned using NIST 610 glass standards (*NIST - SRM 610 Trace Elements in Glass*, accessed 24/07/2018). NIST 610 was used throughout analysis to track background variations and convert the CPS (counts per second) provided by the ICP-MS for each isotope into concentrations in ppm.

Plesovice zircon standards were used alongside NIST 610 to track variations during analysis and to determine the accuracy of each analysis. Plesovice Zircon standards have a ²⁰⁶Pb/²³⁸U age of 337.13±0.37Ma using the ID-TIMS method, with U concentration ranging between 465-3084ppm (Sláma *et al.*, 2008). Plesovice standards were analysed prior to unknowns to prove analysis was reliable and reproducible. Once the accuracy of the age calculations was determined, samples of unknown age were analysed. Additional Plesovice standards in each analysis sequence monitor the reliability of each run.

2.2.4 Data reduction

Due to the small zone widths in the zircons sampled there was little leeway for error in targeting. Subsequently all ablated spots were assessed under an optical microscope prior to data reduction to determine whether spots have crossed zones or uncovered inclusions leading to inaccurate isotope measurements (Figure 15).



Figure 15:reflected light and secondary electron images of grain SA10_0316. Spot SA10_0316_1 was visible in the centre of the grain. Although no inclusion was visible prior to analysis, a subsurface inclusion has been cut and can be seen in both reflected light and SEM secondary electron imagery.

Data tables were produced using Igor pro v6.37 data reduction software (available from *lolite Software*, 2018). Plesovice Zircon standard deviation was calculated based on the final ²⁰⁶Pb/²³⁸U ages of all Plesovice analysis in this study. The accuracy of the Plesovice standards was calculated by comparing calculated age to true age (Equation 1). Precision was be calculated by dividing standard deviation by average calculated age (Equation 2).

Equation 1

 $\frac{true\,age}{average\,calculated\,age} = \%\ accuracy$

Equation 2

 $\frac{Standard\ deviation}{average\ calculated\ age} = \%\ precision$

Any calculated Plesovice ages lying more than 2σ (σ = standard deviation of calculated ages) above or below the true age (337.13±0.37Ma, Sláma *et al.*, 2008b) were removed. The sample from which each age was removed and the total number of ages removed were recorded. Standard deviation was recalculated with the remaining ages and the process repeated until precision and accuracy start to drop.

Once the standard age was determined, the reduction of sample data was begun. The reliability of measurements in a given sample was estimated based on the number of Plesovice standard ages measured that had to be removed calculate the accurate standard age. If, within the same run of ten determined Plesovice standard ages four of them need to be removed, then there has been a problem with that particular LA-ICP-MS analysis session, or with the data reduction. The sample ages will not be as reliable as a separate sample in which all Plesovice standard ages were accurate.

2.2.4.1 Kernel density estimates and probability density plots

Probability density plots (PDP's) have in the past proven to be a popular tool for data visualisation in geochronology. However, this method has been found to provide misleading displays when working with precise measurements (Vermeesch, 2012).

In geochronology, PDP frequency distribution was based on the age of each data point in combination with its analytical uncertainty. This method produces clusters of peaks in densely populated areas; however as the overlap was based on analytical uncertainties rather than age deviation these clusters cannot reliably be assumed to display the true distribution of probable age (Vermeesch, 2012).

In response to this issue, kernel density estimates (KDE's) have been proposed as a scientifically grounded alternative. KDE plots were calculated using the age of each data point in combination with the standard deviation of that data point (as $\pm x$ Ma) as Gaussian bell curves. The overlap of these bells was then stacked to produce the KDE. As overlap was generated by age standard deviations, an accurate representation of data distribution was be created. This method was detailed in full by (Vermeesch, 2012).

Figure 16 plots both KDE and PDP's for samples SA10, SA3.1, and SA2 (this study). The KDE for SA10 displays a trimodal distribution, with the bandwidth defined by the maximum standard deviation (in Ma) for that dataset. The PDP plotted alongside instead displays a number of disparate spikes, with clustering around the three major peaks of the KDE. In a dataset such as this, the clusters

are discernible, however the KDE is clearer and makes outliers easier to discern, as it accounts for age deviation.



Figure 16: Comparison of PDPs and KDEs. Kernel density estimates (KDE, thick blue curve) and probability density plots (PDP, thin black peaks) for samples from this study. Plots were created using 'density plotter' software (Vermeesch, 2012). A, C, and E have a bandwidth = σ (standard deviation in Ma). B, D, and E have a bandwidth = 2σ . KDE's in A, C, E display age trends within the dataset clearly, whilst PDP's in the same graphs display a large number of sharp spikes which are difficult to interpret in samples with a large number of data points (SA10) and comparatively easy to interpret in a sample with few data points (SA2). This is not a beneficial trait in data analysis. By altering the bandwidth to 2σ in B, D, E, we see a significant change in resolution of the KDE, however the PDP remains unchanged. This is because PDP's do not consider age deviation and instead rely on analytical uncertainty.

This study utilises KDE's for data visualisation. For ease of comparison all plots cover a standard time axis of 0-3600Ma. Plots were constructed using 'Density Plotter' (Vermeesch, 2012) available from

(http://www.ucl.ac.uk/~ucfbpve/densityplotter/), a java based KDE and PDP platform. 'Density plotter' provides an 'adaptive distribution' feature which determines bandwidth across a plot based on the local density of data to provide ideal resolution in both dense and sparse areas of the plot. In this study the adaptive distribution model led to oversmoothing of plots (see Figure 17A).

Subsequently each bandwidth was defined by the maximum standard deviation in the dataset for that sample (Figure 17B). Bandwidths lower than this definition would lead to undersmoothing of the plot. Exceptions to this rule were made in sample SA21 as the maximum standard deviation of 460Ma was indicative of poor data quality, subsequently the sample was re-analysed. Data from the subsequent reliable analysis of SA21 was labelled SA21_C.

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Figure 17: KDE bandwidth comparison. A) The KDE produced using 'adaptive distribution' for sample SA10. The entire dataset is smoothed into a unimodal peak spanning ~1000Ma. Compare to B) the KDE produced using a bandwidth of σ (standard deviation in Ma) for the same sample. This is the maximum viable resolution as lower bandwidths would cease to represent the data accurately. The KDE now displays a generally trimodal distribution and more clearly displays outlying data.

Chapter 3 Results

3.1.1 Zircon textures in Cathodoluminescence

3.1.1.1 Zoning

Zones in zircon represent different phases of crystal growth and may vary in composition dependant upon composition of the source melt for each zone. In CL imagery variations in zone composition are highlighted by variations in colour between zones (see

Figure 18, SA4_0800, SA8_0409, SA8_0501). Zone colouration in CL is primarily controlled by variations in U and Hf concentration (Hanchar and Hoskin, 2003). Oscillatory zoning is present in some grains (

Figure 18, SA10_0011). Analysis was targeted at individual zones to provide ages for distinct zircon forming events. Where multiple zones were ablated the age produced was dismissed as unreliable as a combination of the ages of each zone.



Figure 18: CL and BSE images of zircon texture and ablation pits. SA2_0404: Zircon metamiction in CL. SA4_0800: Euhedral zircon displaying oscillatory zoning and minor inclusions visible as bright spots. SA4_0902: Relict zircon containing fractures and inclusions displaying bright overgrowth zone on rim. SA5_0810: Zircon displaying oscillatory zoning, minor inclusions, and radial fractures. Overgrowth present on crystal rim. SA8_0409: Euhedral crystal displaying variations in zone composition highlighted in CL images by zone brightness. Minor inclusions visible as dark and bright spots throughout. Radial fracturing is visible in some zones. SA8_0501: Euhedral zircon formed around an included core. Radial fractures are present around the zircon core. SA10_0011: Euhedral zircon displaying a high degree of oscillatory zoning. SA10_0002: SE image displaying ablated pits in zircon. Pits are typically steep sided with a flat base.

3.1.1.2 Metamorphic overgrowths

Regional metamorphic events may lead to conditions suitable for the formation of metamorphic zircon. Metamorphic zircon forming on the rim of a pre-existing crystal create thin zones known as overgrowths (see Figure 18, SA4_0902, SA5_0810). Where analysis was possible metamorphic overgrowths provide important insight into the timing of orogenic and other metamorphic processes to have affected the zircon, however overgrowths were not typically large enough for analysis.

3.1.1.3 Metamictization

Radioactive decay of uranium isotopes in zircon causes decay of the crystal lattice leading to a total loss of structure and zoning within the crystal as seen in Figure 18 (SA2_0404). This process is known as metamictization. Loss of original zoning in metamict crystals renders them unsuitable for LA-ICP-MS analysis.

3.1.1.4 Fracturing

Radial fracturing occurs in zircon due to radioactive decay of uranium isotopes. Where uranium is more highly concentrated in the rim of a crystal radial fractures are seen in the rim (

Figure 18, SA5_0810, SA8_0409, SA8_0501). Where uranium concentration is greater in the crystal core radiation induced fractures are more likely to be seen in the core. Some fractures may be related to regional stress and strain or transport of the crystal. Where high degrees of radiation damage and fracturing are present it is likely that ages produced from the area are unreliable. Areas of dense fracturing were avoided during analysis.

3.1.1.5 Inclusions

Fluid and mineral inclusions are often found in zircon. In CL images inclusions typically appear as either dark or bright areas depending upon their composition (see

Figure 18, SA4_0800, SA4_0902, SA5_0810, SA8_0409, SA8_0501). Inclusions will generate unreliable ages in targeted during analysis. In zircon with minor inclusions or sparse larger inclusions spots are positioned to avoid inclusions. Where inclusions lay near to or on a major fracture the entire fracture was avoided during analysis.

3.1.1.6 Ablation pit morphology

Ablation pits were imaged using SE imaging to provide topographic information on the ablation site. Pits typically were typically steep sided with level bases (Figure 18, SA10_0002). Plesovice Zircon standard mean ages are presented prior to discussion of unknown ages.

3.1.2 Plesovice Zircon standards

3.1.2.1 Standards data

Plesovice Zircon standards have a ²⁰⁶Pb/²³⁸U age of 337.13±0.37Ma (see section 2.2.3.3). Plesovice Zircon is measured prior to and during analysis of unknowns to ensure consistently accurate results. Total mean age for Plesovice Zircon in this study is 337.46Ma with two standard deviations of 11.67Ma, providing a mean accuracy of 99.90% and precision of 1.07%. Mean ages for standard measurements taken during analysis of unknowns vary (see Table 1).

			2		
	Mean	Standard Standard		Accuracy	Precision
	Age	Deviation	Deviations	(% correct age)	(% variation)
Total	336.781	3.60	7.19	99.90%	1.07%
Standalone	337.375	2.38	4.75	99.93%	0.70%
SA2	337.271	4.60	9.20	99.96%	1.36%
SA3.1	337.635	6.64	13.28	99.85%	1.97%
SA4	337.027	2.12	4.24	99.97%	0.63%
SA5	339.471	14.50	29.01	99.31%	4.27%
SA7	337.060	2.95	5.90	99.98%	0.88%
SA8	336.996	2.17	4.33	99.96%	0.64%
SA10	337.091	0.27	0.55	99.99%	0.08%
SA21C	336.969	1.55	3.10	99.99%	0.46%

Table 1: Mean standards data by sample. Mean standard ages for Plesovice standardsmeasured during analysis of each sample. Accuracy is calculated as a percentage of the correctage, higher %accuracy indicates greater concordance with published ages. Precision is calculatedas the percentage of variation between ages in a given sample, lower %precision indicates lowervariability. Sample SA21C displays the highest accuracy and precision, whilst SA3.1 and SA5display the lowest indicating measurements of poorer quality.

Standard ages are typically above 99.93% accuracy (within 0.07% of published Plesovice ages). Notable exceptions to this are SA3.1 Plesovice measurements (see Table 1) which has an accuracy of 99.85% (within 0.15% of published ages) and SA5 which has an accuracy of 99.31% (within 0.69% of published ages). The highest quality Plesovice data obtained during analysis of unknowns was from sample SA10 with an accuracy of 99.99% (within 0.01% of published ages).

Unknown zircon ages are presented using visual representations of the larger dataset.

3.2 LA-ICP-MS ages: Applecross Peninsula

3.2.1 Kernel Density Estimates (KDE)

Results are here visualised using KDE plots. KDEs are preferred over probability density plots (PDPs) as they provide a more realistic interpretation of the possible age spectrum in the sample (see Methodology, section 2.2.4.1). KDEs are plotted using 'Density Plotter' (Vermeesch, 2012) software available at 'http://www.ucl.ac.uk/~ucfbpve/densityplotter/'.

KDEs are plotted on a standard timeline of 0-3600Ma for ease of comparison. Bandwidth is defined by the maximum 2σ value of all ages within that sample. Within each sample, cores are plotted separately as they determine the maximum age of each grain.



3.2.1.1 SA2 - SA 3.1

Figure 19: KDE; SA2-SA3.1. KDE plots displaying data for samples SA2 (A, B) and SA3_1 (C, D) with grain cores and grain rims, plotted separately. SA2 is plotted at a bandwidth of 58Ma, SA3_1 is plotted with a bandwidth of 73Ma (2σ)

Although the number of analyses is limited, sample SA2 rims display a bimodal trend (Figure 19A); a minor peak is positioned around 1322Ma with a more prominent peak occurring later, at around 1620Ma. Figure 19B displays a bimodal trend for grain cores in SA2 with a pronounced peak at 1076Ma and second at 1657Ma, coinciding with the larger peak displayed by rims in the same sample.

Sample SA3_1 is slightly oversmoothed due to a high maximum 2σ value for the sample. The KDE is broadly unimodal, although two clusters can be discerned in Figure 19C (grain rims); a major peak occurs around 1287Ma, with a poorly defined older peak around 1630Ma. Figure 19D (grain cores) displays the inverse for cores of the same sample, with a major peak around 1710Ma and a poorly defined hummock between 1120-1360Ma. Four grains in Sample SA3_1 (two core ages and two rims) give ages in excess of 2600Ma: SA3_1_0302_1 provides a core age of 2730±30Ma from a rounded grain with minimal fracturing and brown tint; SA3_1_0608_1 provides a core age of 2648±66Ma in a larger grain containing a defined core. SA3_1_0306_1 has a ²⁰⁶Pb/²³⁸U age of 2780±30Ma from a clearly defined zone near the rim; some red spots indicative of radiation damage are present in the grain, but are avoided during the analysis. SA3_1_0908_2 has a ²⁰⁶Pb/²³⁸U age of 2640±36Ma from an area of oscillatory zoning, just outside the grain core.





Figure 20: KDE; SA4-SA7. KDE plots displaying data for sample SA4 (A, B) and SA7 (C, D). SA4 is plotted with a bandwidth of 41Ma, SA7 is plotted with a bandwidth of 32Ma (29).

Rims in sample SA4 (Figure 20A) show a low peak at 1111Ma, followed by a gradual increase in age density from 1300-1600Ma, with a major peak at 1733Ma. Only a small number of cores are measured in SA4 (Figure 20 B), producing peaks at 1295Ma and 1610Ma. Due to the low volume of core data in this sample, any core interpretations must be taken as provisional.

Rim analysis in SA7 (Figure 20C) shows a bimodal trend. The youngest peak has a small component peaking at 1206Ma before a main peak at 1348Ma. The older major peak in the sample lies at 1630Ma with a tight cluster of four grains. A single grain rim provides an age of 1789±21Ma. Core analysis of SA7 (Figure 20D) includes only three grains, which do not cluster at the bandwidth used. Spot SA7_0001_2 has a ²⁰⁶Pb/²³⁸U age of 1140±29Ma. Spot SA7_0306_1 has a ²⁰⁶Pb/²³⁸U age of 1686±29Ma. Spot SA7_0402_1 has a ²⁰⁶Pb/²³⁸U age of 1511±17Ma. Grains SA7_0306_1 and SA7_0402_1 begin to coalesce, however as the points do not cluster strongly they should be taken as single grain ages and not KDE peaks.





Figure 21: KDE; SA5. KDE plots showing data from sample SA5. Plots A, B have a bandwidth of maximum 29 within the sample. Plots C, D have a bandwidth of maximum 1 σ within the sample. Spot targeting was poor during analysis of SA5 due to ablation of multiple zones, inclusions, or resin as desired ablation sites were missed. This lead to a depleted dataset. Post-analysis assessment of ablated spots provided some usable data, however as a result of the poor quality of the analysis the KDE plots are oversmoothed, with bandwidth based on maximum 2σ . To better understand the distribution of smoothed peaks, a second pair of KDEs based on a 1σ bandwidth are plotted; however these peaks should be interpreted with caution.

Rims in SA5 (Figure 21A) display a broadly bimodal trend at 1398Ma and 1836Ma respectively. The peaks in Figure 21A are of similar magnitude and with no defined divide; by comparison, in Figure 21C (KDE at 1σ), the relationship

between the two peaks is clearer. A divide exists in the dataset between ~1650Ma - 1720Ma. As the dataset for this sample is limited and of low quality it is likely that this gap is an artefact of analysis.

Spot SA5_0707_2 provides a maximum age of 3071±36Ma. The analysed spot is located in a clearly defined zone between the rim and core of the grain. Although some discolouration is present, it is focused around the tip of the grain furthest from the ablation site.

SA5 core analyses provide two ages. SA5_0603_1 has a ²⁰⁶Pb/²³⁸U age of 2205±94Ma, SA5_0706_2 has a ²⁰⁶Pb/²³⁸U age of 1618±61Ma. Due to the low number of data, points SA5 core ages are interpreted as single ages.

3.2.1.4 SA8



Figure 22: KDE; SA8. KDE plots showing data from sample SA8. Plots A, B have a bandwidth of 86Ma (2σ). Plots C, D have a bandwidth of 43Ma (1σ).

KDEs based on 2σ bandwidth for SA8 are reliable, however a second plot at 1σ (Figure 22) provides a higher resolution to assess broad clusters within the KDE.

Rims in SA8 show a bimodal trend (Figure 22 A) with peaks at 1148Ma and 1628Ma. Two grains provide ages in excess of 2400Ma; SA8_0203_2 has a ²⁰⁶Pb/²³⁸U age of 2581±61Ma. SA8_0312_1 has a ²⁰⁶Pb/²³⁸U age of 2863±86Ma from a fragment.

Figure 22B shows a broadly unimodal trend in SA8 core data, with a peak at 1343Ma. A single grain (SA8_0204_1) has a 206 Pb/ 238 U age of 2263±49Ma. Figure 22 D has a bandwidth of 1 σ providing higher KDE resolution. Higher 2 σ uncertainties are related to grains over 2Ga in age, therefore this level of smoothing is more appropriate for the main peak in the KDE. Increased resolution shows two additional clusters in the sample which do not stand apart from the unimodal trend. Two clusters are present, one between 1060Ma-1150Ma and the other between 1600Ma-1680Ma.



3.2.1.5 SA10 - SA21C

Figure 23: KDEs; SA10-SA21C. KDE plots displaying data for samples SA10 (A, B) and SA21C (C, D). SA10 is plotted with a bandwidth of 26Ma (2σ). SA21C is plotted with a bandwidth of 43Ma (2σ).

Figure 23A shows a trimodal trend for rim ages in sample SA10. Dominant peaks are present at 1317Ma and 1752Ma. An older a peak at 2758Ma consists of two grain rims. SA10_0011_2 has a 206 Pb/ 238 U age of 2758±14Ma from an area of oscillatory zoning near the crystal tip; some brown colouration is present nearby but is avoided by the spot. SA10_0405_2 has a 206 Pb/ 238 U age of 2755±21Ma from a broad, clear zone between the core and rim of the grain.

Core data in sample SA10 display a trimodal distribution of data (Figure 23,B) with outlying single grains. A defined peak is present at 1166Ma. Two similar peaks at 1396Ma and 1504Ma are interpreted as phases of a single event. A final major peak occurs at 1657Ma, followed by an individual grain (SA10_0109_2)

with an age of 1980±26Ma. A maximum core age is defined by SA10_0407_1 with an age of 2252±11Ma.

Sample SA21C grain rims (Figure 23C) show a bimodal trend with minor interstitial elements. A tight cluster of ages provides a major peak at 1116Ma, followed by a minor peak at 1304Ma. The second major cluster is found at 2728Ma, with a small number of single grain ages between the two main clusters. A single grain (SA21C_0202_1) has a ²⁰⁶Pb/²³⁸U age of 3346±43Ma. Grain SA21C_0202 has an even, faint red hue throughout the crystal, however CL (cathodoluminescence) imagery indicates that zones in the ablation area are intact, despite the fact that the spot is adjacent to a fracture.

Grain cores in SA21C (Figure 23D) display a trimodal distribution of ages. The first major peak occurs at 1248Ma with the second peak at 1762Ma. The third cluster shown in the KDE consists of two data points ~600Ma apart and are treated as single grain ages. SA21C_0005_1 has a 206 Pb/ 238 U age of 2942±42Ma, SA21C_0206_1 has a 206 Pb/ 238 U age of 2716±28Ma.

General trends within each sample are presented above, it is also important to consider the variations between each sample in a stratigraphic context.

3.2.2 Stratigraphic succession

Samples are taken entirely within the Applecross Formation, from various stratigraphic levels. Sedimentary features include heavy mineral laminae, cross bedding (various), laminations, granules from 1mm upwards, soft sediment deformation, and some accretions. The context log (Figure 24) provides important detail on the sedimentary succession of the Applecross Formation, however no samples taken directly from the logging area were analysed. Stratigraphic relationships between analysed samples are determined using local geological maps (available online at https://www.bgs.ac.uk/data/maps/maps. cfc?method=viewRecord&mapId=10903, Geikie *et al.*, 1973). By placing KDEs in relative stratigraphic positions, variations in detrital zircon U-Pb age over time can be assessed (see Figure 26, Figure 27).

184 m of Applecross sandstone are logged for geological context (Figure 24) on the southeast face of Sgurr a'Chaorachain (GPS 57.40762). The entirety of the logged succession is quartzo-feldspathic sandstone of varying coarseness, with rare localised mud clasts. Granules are found in a number of units with varying coarseness and abundance. The lithology is mature and homogenous (see Table 2), suggesting that sediment has been transported from a distal source. Grains are often angular to sub rounded (Table 2), indicating that although the degree of sorting is high, high levels of rounding have not been achieved. This could be related to the resistance of bulk minerals to erosion. The structures present (coarse cross bedding, heavy mineral laminae, soft sediment deformations) indicate a high sediment influx and rate of flow within a fluvial regime at the time of deposition.

Structures favouring heavy mineral deposition (cross bedding, heavy mineral laminae, story surfaces, etc.) are preferentially sampled to improve zircon yield for analysis. Whilst depositional processes can lead to a natural bias in ages, this is difficult to quantify and is likely to be outweighed by analytical biases (Sláma *et al.*, 2008).





Figure 24: Applecross context log. Context log taken approximately midway along the sample transect including palaeocurrent directions and sedimentary features of the succession. GPS positions and sampling locations within the logging area are included. Lithology is feldspathic sandstone throughout with silt present in localised laminations.

The primary focus of this study is the U-Pb dating of the Applecross Formation, however a small sample of paleocurrent data were collected to indicate the direction of the sediment source (Figure 25). Palaeocurrents taken from the log section plus two additional measurements from sampling localities 21 and 24 indicate a broadly west and southwest flow regime. This could be interpreted as indicating a source area to the northeast; it is noteworthy however, that the palaeocurrent measurements were taken individually across several sample locations and may not be characteristic of the outcrops at which they were observed. Palaeocurrents within the Applecross Formation are typically to the south east indicating a source to the north west (Gracie and Stewart, 1967; Nicholson, 1993; Williams, 2001; Owen and Santos, 2014).

Sample depths given below estimated using structure contours, with depths stated relative to sample SA10. A graphical representation can be found in Figure 26.

Sample SA10 is the lowest stratigraphic sample analysed and provides a comparative base to the sample succession (Figure 26). Sample SA8 occurs approximately 677m stratigraphically above SA10, and is roughly level with the top of the context log (670m). SA7 and SA5 are found approximately 870m and 894m stratigraphically above SA10, respectively. SA4 and SA21C form a similarly close pair approximately 990m and 1004m above SA10. SA2 and SA3.1 form the uppermost set of samples approximately 1869m and 1898m stratigraphically above SA10. The age variation between zircon populations in these samples is discussed below.

3.2.2.1 Age variation through stratigraphy

Age clusters from individual samples must be considered in a stratigraphic context. Core analyses (Figure 26, Figure 27: left column) typically include a clustered component of varying precision around 1680Ma. In the lower to middle sections of the sequence (SA10 and SA8) grain cores also display clusters around 1150Ma, with single grains and pairs of grains around 2250Ma. A greater portion

of grain cores clustering around 1000-1100Ma are present in SA8 (~677m, top of context log).

Sample	Colour	Cement	Grain Size (µm)	Sorting	Sphericity	Rounding	Support	Consolidation	Lithology	Notes
SA1	Pink	Fine white cement	1000	Poorly sorted	Low	Rounded- angular	Grain supported	Good	Quartzo-feldspathic sandstone	Pebbles and granules up to 4mm.
SA2	Pink-grey	None/ Interlocking grains	500-750	Poorly sorted	Low	Angular- some sub rounded pebbles	Grain supported	Good	Quartzo-feldspathic sandstone	Small pebbles and granules up to 3mm.
SA3.1	Pink	None/ interlocking grains	375-750	Poorly sorted	Moderate- low	Sub rounded	Grain supported	Good	Quartzo-feldspathic sandstone	Granules and pebbles up to 10mm. Sample includes a large 'blob' of coarse material, possibly a clast.
SA3.2	Dark pink	Fine white cement	500-750	Moderately sorted	Moderate- low	Angular	Grain supported	Good	Quartzo-feldspathic sandstone	Granules up to 2mm.
SA4	Pink-grey	Fine white cement	500-1000	Moderately sorted	Moderate- high	Sub rounded- occasionally well rounded	Grain supported	Good	Quartzo-feldspathic sandstone	Granules present, comprised of K-feldspar and quartz.
SA5	Dark pink	Fine white cement	187-375	Well Sorted	Moderate- low	Sub angular	Grain supported	Good	Quartzo-feldspathic sandstone	Contains occasional granules.
SA6	Dark pink	Fine white cement	187-250	Well Sorted	Moderate	Sub angular	Grain supported	Good	Quartzo-feldspathic sandstone	Mica is up to 750µm in some coarser bands of up to 2cm thickness.
SA7	Pink	None/ interlocking grains	187	Very well sorted	Low	Sub angular- sub rounded	Grain supported	Good	Quartzo-feldspathic sandstone	
SA8	Dark Pink	None/ interlocking grains	187-250	Well Sorted	Low	Sub rounded	Grain supported	Good	Quartzo-feldspathic sandstone	Muscovites tend to be localised and of greater grain size (up to $500\mu m$).
SA21	Pink	Fine white cement	250-375	Poorly sorted	Low	Angular	Grain supported	Good	Quartzo-feldspathic sandstone	Some grains up to 750µm.
SA23	Pink	None/ interlocking grains	250	Well sorted	Low	Sub angular	Grain supported	Good	Quartzo-feldspathic sandstone	
SA24	Pink	None/ interlocking grains	187	Very well sorted	Low	Very angular	Grain supported	Good	Quartzo-feldspathic sandstone	

 Table 2: Hand specimen descriptions.
 Hand specimen descriptions for samples from which grains have been analysed.



Applecross context log palaeocurrent indicators (n=12)

Figure 25: Applecross context log palaeocurrent indicators. Rose diagram displaying palaeocurrent measurements taken in this study. Notice that the sample size is small and therefore could only refer to locally defined flows. Flow indicators (cross bedding) have a mean flow direction of 233.75°

Samples SA7and SA5 are stratigraphically close (~24m) and lie ~2.7km apart geographically. SA7 has a depleted core dataset with only three ages: 1140±29Ma, 1511±17Ma, and 1686±29Ma. SA5 is similarly depleted in core data providing ages of 2205±94Ma and 1618±61Ma. Viewed together, three grains from SA7 and SA5 are clustered between 1500Ma-1700Ma, in line with clusters around 1680Ma seen in the lower stratigraphy. The oldest core from SA5 correlates approximately with oldest single grains in SA10 and SA8.

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Age cluster comparison within stratigraphy

Figure 26: KDE peak changes over stratigraphy upper. KDEs for samples SA10 (A, B), SA8 (C, D), SA7 (E, F), SA5 (G, H), and SA4 (I, J), with stratigraphic position relative to SA10 (uppermost analysed sample) on the left.



Figure 27: KDE peak changes over stratigraphy lower. KDEs for samples SA21C (K, L), SA2 (M, N), and SA3.1 (O, P) in stratigraphic order. For relative stratigraphic position see Figure 26. SA4 and SA21C are approximately halfway through the sampled stratigraphy (~990m and 1004m above SA10). Single grain cores are present which correlate to the large clusters around 1680Ma present near the base of the sequence. This component is still present, however it represents a lower proportion of grain ages. SA4 and SA21C core ages are dominated by clusters around 1120Ma-1280Ma with an additional cluster around 1760Ma displayed in SA21C. SA21C cores have maximum single grain ages of 2716±44Ma and 2942±421Ma

SA2 and SA3.1 represent the uppermost sampled stratigraphy (~1869m and 1898m above SA10). Core age clusters are split between a primary cluster of 1600Ma-1700Ma cores correlating with clusters in the lowermost stratigraphy, and a secondary cluster in SA 3.1 between ~1120Ma-1440Ma. SA2 has a youngest core age of 1039±47Ma. SA3.1 includes maximum core ages of 2648±66Ma and 2730±39Ma.

Rim analyses of samples SA10 and SA8 (lowermost and log-correlated samples) again show age clusters between 1600Ma-1720Ma matching the core analysis clusters around 1680Ma in the same samples. SA8 displays a minimum single grain age of 1083±29Ma from rim analysis compared to a minimum single grain

age of 1018±14Ma from core analysis. SA10 and SA8 each contain single grain rim ages in excess of core ages, 2755±21Ma from SA10, 2581±61Ma and 2863±86Ma from SA8.

SA7 and SA5 (middle of stratigraphy) rim analyses display small clusters and single grain ages which are in general agreement with the lowermost samples, including a small cluster around 1880Ma in SA5 correlating to a single grain from SA10. SA5 provides a maximum single grain rim age of 3071±36Ma. SA7 rims display two small clusters around 1200Ma and 1300Ma, correlating with a single core of similar age, as well as the youngest clusters in SA8.

SA4 and SA21C (middle of stratigraphy) rim analyses show clusters equivalent to core analyses of the same samples, however core clusters in the range of 1120Ma-1280Ma are replaced by clusters between 1040Ma-1150Ma. SA21C rim analysis includes a cluster around ~2720Ma correlating with single grain cores of similar age. SA21C rim analysis gives a maximum single grain (rim) age for all samples of 3346±43Ma (SA21C_0202_1).

SA2 (uppermost sampled stratigraphy) rim analysis display similar oldest age clusters to core analysis of the same sample, however only a single grain rim is equivalent to the youngest core age cluster. An older cluster around 1280Ma-1400Ma is present in place of the core cluster and is consistent with rim ages in other samples. SA3.1 (uppermost sampled stratigraphy) rim analysis displays clusters of similar age to core analysis in the same sample. Where core analysis shows a trend towards older ages, rim analysis displays and inverse set of peaks with a trend towards younger grain ages.

3.2.2.2 Age variation through stratigraphy summary

The lowermost sampled stratigraphy is shown to contain predominantly Mesoproterozoic population with a significant Palaeoproterozoic component. Rim analysis of the lowermost stratigraphy continues to show predominantly Mesoproterozoic populations with a slightly greater proportion of Palaeoproterozoic ages compared to core analysis of the same samples. Additionally rim analysis provide evidence of an Archaean zircon population in the lower part of the sample stratigraphy otherwise unseen in core analysis of the same samples.

The middle of the sampled stratigraphy is here shown to have a younger bulk of core ages, with greater maximum core ages. Rim analyses show a weaker trend towards younger ages. Archean components of the core analysis are reinforced by rim analysis, however it is shown that the lower stratigraphy also includes a component of Archean zircon.

The uppermost stratigraphy is shown to have similar core ages to the lowermost stratigraphy, with a greater density of ages present in younger clusters than the uppermost stratigraphy. Oldest single cores are similar in age to those found in the middle of the sequence (Palaeoproterozoic- Archean). Rim analysis reinforces the trend towards younger ages in the uppermost sampled stratigraphy seen in core analysis

3.3 Ablation spots

3.3.1 Ablation sites

Ablation sites are positioned within individual core or rim zones of grains (see methodology, sections 2.2.2- 2.2.3) as in Figure 28. During ablation of samples laser targeting was out by up to 40µm in some instances. The position of spots in CL images are corrected post-ablation to show where actual ablation occurred and not sites at which it was intended to occur. Subsequently a number of data points are rejected from the analysis based on crystal texture at the site of ablation, see Figure 28, Figure 29, Figure 30, Appendix 2.



Figure 28: CL and SE images, SA3.1_0406. Grain SA3.1_0406 CL (cathodoluminescence, left) with combined CL and secondary electron (right) imagery. Spot 1 (SA3.1_0406_1) is positioned within the core of the grain clearly visible in the CL image.



Figure 29: Pre-ablation CL and post-ablation SE images, SA10_0316. Grain SA10_0316 in Cl (cathodoluminescence, left) pre-ablation and secondary electron post-ablation image. Spot SA10_0316_2 is marked on the left and ablated on the right. Although no inclusion is visible in the CL image (left) subsurface inclusions have clearly been cut in the post-ablation image (right).



Figure 30: CL and SE images, SA3.1_0507. Grain SA3.1_0507 in CL (cathodoluminescence, left) with combined CL and secondary electron image (right). Spot SA3.1_0507_1 is marked on the CL image and has been corrected to show the site of ablation. The spot was originally intended to be entirely with the zone in which its right half sits and has shifted by ~20µm to the left due to poor adjustment of laser targeting prior to analysis. As the spot not only crosses multiple zones, but also cuts the resin in which the grain is mounted it must be rejected from the analysis.



Figure 31: Transmitted light image, SA8_0309. Plain light image of grain SA8_0309 showing discolouration in the area of ablation indicative of radiation damage.

3.3.2 Table of ablated spots

During data reduction, a number of ablated spots are rejected from the data set due to poor quality. Data points are not rejected on the basis of nonconcordance or undesirable fit. Rejection criteria are based around poor crystal or spot quality and include spots which have (due to errors in laser targeting) missed the crystal entirely, missed the planned ablation site and crossed clearly defined zones, missed the crystal site and hit resin, or struck areas of crystal with strong evidence of radiation damage, metamictization, or other undesirable textures. Reasons for exclusion are given in Appendix 2. As it is likely that a number of non-ideal ablation sites will be present in a large dataset it is necessary to verify the quality of analysis after data has been obtained.

3.3.3 Analysis quality

The KDE for SA8 displayed in shows a minor peak later than any seen elsewhere in the study. This peak relates to two grains of young age (later ages than the accepted depositional age of the Applecross Formation) included here to demonstrate some of the criteria for exclusion of grains and analysed spots from final interpretation. It should be noted that the ages produced during analysis are not considered valid grounds for exclusion.

Sample SA8_0309_1 provides a ²⁰⁶Pb/²³⁸U age of 927+-14Ma, ~53Ma later than deposition of the Applecross Formation. SEM CL (Cathodoluminescence) imagery (Figure 32A) display some alteration and inclusions within the grain, however a zone within the grain appeared viable for analysis and a spot was included. Transmitted light images (Figure 32B) taken post-ablation reveal radiation damage (visible as a brown/orange tint) in the region of the ablated spot. This damage is less visible in the CL images and is likely to have affected the results.



Figure 32: Cathodoluminescence (CL) and transmitted light images of sample SA8_0309. A) CL and secondary electron composite images display several areas of alteration visible as lighter grey areas and inclusions visible as dark spots, often with associate alteration. B) PPL and XPL transmitted light images. The PPL displays a clear brown tint associated with radiation damage in the grain, more visible here than in the CL image. XPL is here used to assess the ablation pit (top left of grain. As the grain has been polished thin there is a risk of cutting through to the grain mount, particularly where ablation is sited near the rim. In small grains birefringence is clearly visible as displayed here and can be used to determine whether a spot has cut through the grain entirely as the resin remains dark; if the ablation pit hits resin this would be visible by a lack of colour.

Sample SA8_0505_1 provided a ²⁰⁶Pb/²³⁸U age of 814+-14Ma, ~164Ma later than deposition of the Applecross Formation. CL images (Figure 33A) display clear zoning, however areas of alteration are visible around the core zones. An effort was made to analyse a clear area of the grain core, however it is clear from the position of the ablated spot (Figure 33B) that an area of alteration adjacent to the inclusion visible above the spot in both images was ablated during analysis and is likely responsible for the ages calculated.



Figure 33: Cathodoluminescence (CL) and transmitted light images of sample SA8_0505. A) CL and secondary electron composite images highlight alteration within the crystal core. Alteration is here visible as lighter areas. Small inclusions are visible as dark spots; note the inclusion in the upper-middle part of the grain. This inclusion has an area of alteration extending around and below it as a light grey smudge. B) Transmitted light and reflected light images showing the final location of the ablation pit. Note the proximity of the pit to areas of ablation visible and described in the CL imagery.

As these analyses are deemed unreliable they are not included in further

discussions or KDEs.

Chapter 4 Discussion

4.1 Detrital zircon age data

Kernel density estimates (KDEs) for samples from this study are replotted with a standard bandwidth of 50Ma for ease of comparison (Figure 34). See Chapter 3 for overview of KDEs. Samples are arranged in stratigraphic order to highlight development of and changes in source ages over 1900m of the 4500m succession. Figure 34A compares KDE's combining both core and rim values for all samples as per the methodology of Zimmermann et al. (2018). The comparison highlights the breadth of detrital ages present, with localities typically showing major Palaeo-Mesoproterozoic peaks with additional Archean components, though these are of lower abundance and do not appear in some low quantity samples (see Figure 27, section 3.2.2). The breadth of ages suggests diverse sources for the Applecross Formation. Some reworking is evident from the pebble suite (Williams, 2001; Stewart, 2002), which may account for part of this diversity. Multiple sources suggest that the source area was a large catchment. Figure 34B displays a visualisation of peak age variations within the Mesoproterozoic, Palaeoproterozoic, and Archean. Earliest deposition (SA10) displays a high influx of Proterozoic zircon, dominantly of early Mesoproterozoic age. A number of late-Palaeoproterozoic grains are also present, with a minor peak in the early-Palaeoproterozoic and individual Archean grains.


Figure 34:KDE (kernel density estimate) variation through stratigraphy. A) U-Pb detrital zircon KDEs for the Applecross Formation in stratigraphic order. B) Comparative schematic of stratigraphic relationships between samples and variations in dominant peak ages through stratigraphy. See text for full discussion.

~677m stratigraphically above this level a sample of similar size (SA8) shows a consistent influx of late-Palaeoproterozoic age; however the primary Mesoproterozoic peak shifts towards the mid-Mesoproterozoic (~1128Ma)- Figure 34A. Early-Mesoproterozoic grains are present, but no longer dominant. This subtle change may relate to incision of the river system into magmatic rocks. Minor early-Palaeoproterozoic and Archean grains remain present.

Above SA8 the succession includes a greater ratio of older detrital zircon. SA7 (870m) and SA5 (894m) display early-Mesoproterozoic peaks similar to the base of the sequence. The late-Palaeoproterozoic peaks of these samples are dominant and a distinct gap is present between them. SA5 has a Palaeoproterozoic peak at ~1874 Ma which aligns with a paucity of similar ages in SA7. The inferred gap between these samples is likely to relate to the low sample size from the locality. The Archean component of SA5 is older than that seen at the base of the sequence with a peak at ~3069 Ma.

Samples SA4 and SA21C (~100m stratigraphically above) display the reverse trend, with peaks rapidly shifting towards younger ages in each period. SA4 (~990m) contains a comparatively small proportion of Mesoproterozoic detritus with ages spread across the era, a primary peak occurring at ~1715 Ma, in the mid-late Palaeoproterozoic. No Archean grains are present in this sample. SA21C (1004m), conversely, displays a major mid-Mesoproterozoic peak at ~1128 Ma, with a 'shoulder' at ~1260 Ma. A Palaeoproterozoic peak at 1763 Ma is similar in age to the Palaeoproterozoic peak in SA4. An early Archean peak is present at 2731 Ma, similar to Archean peaks seen in SA8 and SA10. One Archean grain with an age of 3346±43Ma is present. If the increase in population ages in SA5 and SA7 relate to incision of the channel into older material in the source area then it is likely that the abrupt decrease in population ages between SA4 and SA21C represent a more dramatic event in the source area, such as channel adjustment by faulting.

Within the uppermost stratigraphy -samples SA2 (~1869m) and SA3.1 (~1898m)the dominant detrital zircon ages display late-Palaeoproterozoic peaks, with a more even spread between the late-Palaeoproterozoic and mid-late Mesoproterozoic occurring in the larger sample size of SA3.1.



Figure 35: Comparison of detrital zircon suites from localities in the Applecross and Aultbea Formations. After (Rainbird, Hamilton and Young, 2001; Krabbendam *et al.*, 2017). A) U-Pb detrital zircon PDPs (probability density plot) for the Applecross and Aultbea Formations after (Rainbird, Hamilton and Young, 2001). B) U-Pb detrital zircon KDEs (kernel density estimate) for the Applecross and Aultbea Formations after (Krabbendam *et al.*, 2017). C) U-Pb detrital zircon KDEs for the Applecross Formation (this study). D) Map of the Torridon Group after (Krabbendam *et al.*, 2017) displaying sample localities for plots in A, B, C. Localities are within the Applecross Formation unless otherwise stated. Localities after (Rainbird, Hamilton and Young, 2001; Krabbendam *et al.*, 2017). Comparison of plots shows similar peaks across all areas of the Applecross and Aultbea Formation sampled supporting a single sediment input into the system. KDE peaks and data throughout samples from this study are similar to those of Rainbird, Hamilton and Young (2001), and of Krabbendam *et al.* (2017) for Applecross and Aultbea samples (Figure 35) taken from Enard Bay and Guinard Bay respectively (Figure 35D), supporting a single well mixed input of detrital zircon into these areas of the Torridon Group. This may have been facilitated by a broad source area with detritus undergoing mixing during prolonged transport in a distal fluvial system.

Figure 36A (multi-dimensional scaling plot/MDS) displays the closest detrital zircon population relationships between samples from this study (within the Applecross Formation). Solid lines indicating nearest neighbours show that position within the stratigraphy is not the key factor determining population similarity; samples SA7 and SA2 are similar in the MDS, but relatively distant stratigraphically. It is likely that small sample size for some localities has influenced population similarity by excluding or exaggerating low abundance detrital zircon populations.

Figure 36B (cumulative distribution function/CDF) is intended to display subtle variations in sample peak ages through the stratigraphy. Krabbendam *et al.* (2017) display a clear younging trend for Palaeoproterozoic peaks through the regional stratigraphy (Loch na Dal fm.- Beinn na Seamraig fm.- Kinloch fm.- Applecross fm.- Aultbea fm.). Samples at a local stratigraphy scale (Figure 36B, this study) do not show such a trend; CDF trends overlap throughout the stratigraphy in no discernable pattern. This trend reinforces consistency in the Applecross source area over the course of deposition and thorough mixing of detrital zircon signatures prior to distribution of sediment within the sampled Applecross sandstones. Applecross Formation CDFs show a similar trend of consistently present Mesoproterozoic peaks with subordinate Palaeoproterozoic peaks and minor Archean populations to that seen in Krabbendam *et al.* (2017), figure 9b, p78.



Figure 36: A) MDS (multi-dimensional scaling) plot, B) CDF (cumulative distribution function) plot, C) KDEs (kernel density estimate) for comparison with Krabbendam et al.(2017) p78, fig 9a,b,c. A) solid lines display greater similarity between samples, dashed lines show less similarity. B) CDF displays samples from this study in stratigraphic order. C) KDEs plotted using 'provenance' software, see (Vermeesch, 2012). A, B, and C display only data collected in this study.

Figure 36C displays a replot of sample KDEs in stratigraphic order using the 'provenance' software package specifically for comparison with Krabbendam *et al.* (2017), figure 9c, p 78. See 'Results' sections 3.2.1-3.2.2 (this paper) and associated text for discussion of KDE trends in this study alone. Applecross and Aultbea KDEs from Krabbendam *et al.* (2017) display strong late-mid Palaeoproterozoic peaks, with peaks present across the majority of the Mesoproterozoic. The Applecross Formation displays a minor Archean peak. With the exception of a small number of early-Palaeoproterozoic peaks present in this study, the data presented is in close agreement with the detrital zircon data of Krabbendam *et al.* (2017).

Assessment of detrital zircon populations from the Applecross Formation provides insight into possible source areas of sediment in the Applecross Formation.

4.2 Source areas

Detrital zircon ages from this study and others (see Rainbird, Hamilton and Young, 2001; Cawood *et al.*, 2007; Krabbendam *et al.*, 2017) suggest extensive source areas for detrital zircon in the Applecross Formation distal enough to facilitate thorough mixing of the detrital zircon signal. Transport and deposition may have been directly from a Grenville Orogen axial trunk river system (Nicholson, 1993; Rainbird, Hamilton and Young, 2001; Krabbendam *et al.*, 2017) or via prior deposition in consolidated sediments/metasediments more proximal to the Applecross Formation.

As discussed in Error! Reference source not found.1.7.3 (this paper) palaeocurrents and stratigraphy support transport of sediments from the northwest (Gracie and Stewart, 1967; Nicholson, 1993; Williams, 2001; Owen and Santos, 2014; Ielpi and Ghinassi, 2015) with distributive fan formation at Cape Wrath (Williams and Foden, 2011). Braidplain deposits in the southwest of the Applecross Formation (Ielpi and Ghinassi, 2015) may represent the distal deposits of alluvial fans further west (Williams and Foden, 2011). It is necessary to consider all available terranes in order to determine the most likely source area of the Applecross Formation.



Figure 37: A) Comparison of Applecross detrital zircon ages to Laurentian basement ages. B) Basement ages in Laurentia and Baltica. C) Basement ages in the Canadian sector of the Grenville Orogeny. Correlation of Applecross KDEs (this study) with basement ages in Laurentia.

Potential source areas for the majority of peaks can be found in magmatic and metamorphic basement rocks. A notable gap in magmatism occurs between 1420-1500Ma in Laurentia, peaks in this gap may have been sourced from supracrustal sequences in Laurentia. B) After (Rivers, 1997; Pisarevsky *et al.*, 2003; Li *et al.*, 2008; Cawood *et al.*, 2010; Krabbendam *et al.*, 2017; Rainbird *et al.*, 2017). C) After.(Rivers, 1997).

Terranes suitable to provide sections of the Applecross Formation detrital zircon suite are discussed in detail prior to the construction of a depositional model.

4.2.1 Archean-early Palaeoproterozoic

Archean cratonic rocks are found across Rodinia (see Figure 37B), particularly around the core of the continent away from later accretionary and collisional zones. The Superior craton of Laurentia and the North Atlantic Craton of southern Greenland (Rivers, 1997; Rainbird, Hamilton and Young, 2001) may have contributed Archean detrital zircon to a Laurentian trunk river system supplying the Torridon. The North Atlantic Craton (Greenland) may also have been within the catchment of a more proximal Torridonian source area.

4.2.2 Palaeoproterozoic

Early-mid Palaeoproterozoic orogens provide zircon ages from 2500-2000Ma from Laurentia, Greenland, and are inferred on the Rockall Plateau (Rivers, 1997; Li *et al.*, 2008).

2000-1800Ma cratonic rocks related to final assembly of fragments around Archean nuclei (Cawood *et al.*, 2007) are exposed in central and western Laurentia, Greenland, and the Canadian sectors of the Grenville Orogen. The new Quebec and Torngat Orogens (1920-1790Ma) also occur in the Canadian sector of the Grenville Orogen (Rivers, 1997), providing a more likely source for the low quantities of mid-late Proterozoic zircon than the more substantial suites further west.

Age densities from this study begin to increase at ~1890Ma, around the onset of the 1900-1720Ma Makkovik and Penokean accretions (Rivers, 1997) in Canada and Greenland. Later orogens include the Matazal (1700-1600Ma) terranes in Labrador and more distally in the southwestern sector of Laurentia (Krabbendam *et al.*, 2017; Rainbird *et al.*, 2017). A high concentration of detrital zircon from the Applecross Formation falls within this period and was most likely derived from the more proximal block in the Canadian sector of the Grenville province.

4.2.3 Early Mesoproterozoic age gap

The early Mesoproterozoic in Laurentia is dominated by a gap in magmatism from ~1.6-1.5Ga (Karlstrom *et al.*, 2001) during which few Laurentian zircon sources are formed. This implies a non-Laurentian provenance for detrital zircon of this age in Laurentian basins (Doe *et al.*, 2013) and subsequently it is likely that zircon of this age in the Torridon is derived from recycled sediments sourced from an area of active magmatism outside Laurentia. This is supported by a lull, but not absence, of detrital zircon ages for this period from the Applecross Formation Figure 37A.

Sedimentary successions containing detrital zircon of 1600-1490Ma age include the Purcell Supergroup in the northern Laurentia (Doe *et al.*, 2013) and the Hess Canyon Group of southern Arizona. Deposits more proximal to the western Grenville province include the Yankee Joe and Blackjack Formations deposited around 1488±9Ma (Doe *et al.*, 2012). The Missouri line (Van Schmus *et al.*, 1993) represents a 1500Ma accretionary province in the granite-rhyolite terrane; however no zircon has been dated from the subcrop to fill the magmatic gap (Doe *et al.*, 2012, after (Van Schmus *et al.*, 1993).

4.2.4 Mid-late Mesoproterozoic

Pinwarian (1495-1445Ma, Cawood *et al.*, 2007) terranes in eastern Laurentia (Cawood *et al.*, 2007; Krabbendam *et al.*, 2017) may have contributed to major Mesoproterozoic detrital zircon peaks in the Applecross Formation. The granite-rhyolite terrane of central Laurentia (~1500-1300Ma, Rivers, 1997; Krabbendam *et al.*, 2017; Rainbird *et al.*, 2017) extends along the later Grenville front offering a distal source for detrital zircon of this age.

The period 1300-1100Ma includes a number of terranes forming protoliths to the Grenville Orogen. Elzevirian (1300-1200Ma) rocks include localised intrusions in the Canadian sector, along with the 1100-1200Ma Shawingan terrane (Rivers, 1997; Krabbendam *et al.*, 2017). Further west the 1200-1100Ma midcontinent rift (MCR) in central Laurentia is a possible distal site for reworking of the associated

basin sediments (Rivers, 1997; Krabbendam *et al.*, 2017; Rainbird *et al.*, 2017) to be incorporated into the Applecross Formation from a distal source.

4.2.5 Grenville Orogen (1200-900Ma)

Individual zircon forming events of appropriate age such as the Grenville Orogen must also be discussed as they may provide zircon of a given age across a broad geographic area.

Accretion and collision associated with the Grenville-Sunsas-Sveconorwegian Orogens occurred from ~1200-900Ma (Rivers, 1997; Cawood *et al.*, 2007; Krabbendam *et al.*, 2017). The Grenvillian sector represents an abundant source for late Mesoproterozoic-early Neoproterozoic detrital zircon in the Applecross Formation. Final collisional events may have uplifted older protolith terranes, generating a greater potential for denundation of those areas.

4.2.6 Summary

Combined with reconstructions of the supercontinent Rodinia (see section 1.5, this paper) and the Grenvillian setting (see section 1.6, this paper) the sedimentary data (see section 1.7, this paper) indicate transport of detrital zircon from Laurentia, in the west. Figure 37A highlights basement rocks likely to provide detrital zircon to the river systems of Laurentia. Figure 37A overlays the time periods covered by each potential source with KDEs from the Applecross Formation (this study) in stratigraphic order. It is evident from peaks and point clusters that the zircon suite of the Applecross Formation is broad and likely sourced from a number of terranes. Abundant detrital zircon is sourced from terranes with ages between 1800-1600Ma and 1500-1100Ma including the 1500-1300Ma granite-rhyolite terranes (Davidson, 2008), 1200-1100Ma MCR and Mesoproterozoic AMCG plutonic suites (Rivers, 1997). The 1200-900Ma Grenville Orogen (Van Kranendonk and Kirkland, 2013; Krabbendam *et al.*, 2017) provides a portion of detrital zircon of this age alongside older material uplifted as an 'orogenic lid' (see Krabbendam et al., 2017). Palaeoproterozoic events including the 1900-1720Ma Penokean-Makkovik accretions (Rivers, 1997) may account for a portion of older detrital zircon peaks.

4.3 Palaeogeographic reconstructions

A number of transport and depositional regimes have been proposed to explain the sedimentology and detrital zircon suite of the Torridonian. Proposals include deposition of the Applecross Formation as proximal fan deposits relating to tectonic movement along the western boundary of the Minch basin (Williams, 2001; Williams and Foden, 2011) and deposition as part of an orogen axial Grenville foreland trunk river system extending from distal sources across Laurentia (Rainbird, Hamilton and Young, 2001; Krabbendam *et al.*, 2017).

Previous models are discussed in the context of new and existing evidence, a revised depositional model for the Applecross Formation is proposed.

4.3.1 Proximal fan deposits

The Torridonian as exposed today is truncated by the Moine Thrust in the east and the Minch Fault in the west. Williams and Foden (2011) suggest a western boundary of deposition along the Outer Hebrides Fault Zone (OHFZ), facilitated by a half-graben basin downthrown on the Minch side of the OHFZ. Ongoing tectonics during deposition are supported by the presence of dilational sand dykes throughout the Applecross Formation and by sediment transport perpendicular to the OHFZ with variable coarseness through the succession, representing periodic reactivation of faults (Williams and Foden, 2011). The tectonic setting for the formation of a half graben at the time of Applecross deposition may be facilitated by periods of extension during the Grenville Orogeny (Rivers, 1997; Cawood *et al.*, 2007). The Cape Wrath Megafan indicates a distributional apex ~30km west of mainland Scotland, in the region of the OHFZ (Williams and Foden, 2011).

Williams and Foden (2011) suggest general fining in the southern Applecross Formation, compared to the Cape Wrath member in the north, indicating that the Applecross, as exposed today, represents an oblique transect of the original basin. In this proposal Cape Wrath represents zones proximal to faulting and the southern Applecross Formation represents areas more distal from fan apexes. Based on the composition of the Applecross sedimentary rocks and pebble suite (see Moorbath *et al.*, 1967) Williams and Foden (2011) propose a supracrustal source area overlying the Lewisian beyond the OHFZ, noting that proximal drainage in this style (see Figure 38) would require a catchment of at least 10⁴km².



Figure 38: A) Schematic diagram displaying fan and braided deposits laterally filling the Applecross basin. B) Satellite image of fans of similar scale to the Cape Wrath member in the Tarim Basin, China. A) After (Williams, 2001; Williams and Foden, 2011). Williams and Foden (2011) propose a proximal source for the Torridon Group beyond the Minch Fault and Outer Hebrides Fault Zone (OHFZ). Sediment from the relatively uplifted source area form alluvial fan deposits proximally with braidplains forming beyond the fans. B) After (Google Earth V 9.2.71.3, 2018). Displays a fan similar in scale to the proposed Cape Wrath Megafan, however it is relatively isolated with braidplain facies occurring alongside the extant fan. Extant examples such as this lend weight to the proposal of Williams and Foden (2011). A proximal source requires a supracrustal series, for which there is as yet no evidence, to provide the Applecross Formation detrital zircon suite and sediment composition.

Flaws in this proposal include a lack of extant evidence for the supracrustal series, noted by Krabbendam and Rainbird (2012). KDEs for detrital zircon in different areas of the Applecross Formation display similar populations, suggesting that either a previously deposited sediments forming the supracrustal series were highly homogenous, or that mixing of populations was able to occur during transport to a single fan apex. Basement sources are unlikely to be proximal as a greater disparity or lower diversity of detrital zircon ages would be expected, and few basement sources of Grenvillian age are available proximally to generate the detrital zircon peaks seen.

4.3.2 Grenvillian foreland trunk river system

Alternative datasets have lead to the significantly different proposal of a distal source area largely precluding deposition in multiple large scale fan deposits.

The detrital zircon suite of the Applecross Formation (see Results, section 3.2.1) spans an interval of ~1100Ma, between ~1000-2100Ma, indicating an extensive source area. Several authors have identified the Grenville Orogen as a potential source (notably Rainbird, Hamilton and Young, 2001; Krabbendam *et al.*, 2017), suggesting an orogen axial trunk river system in the foreland of the orogen (Figure 39). The presence of pan-continental river systems in Laurentia is well established (Rainbird *et al.*, 1997, 2017). Basement lithologies in the Grenville foreland provide potential sources for almost the entire Applecross detrital zircon suite, with the exception of the ~1600-1520ma gap in Laurentian magmatism (Karlstrom *et al.*, 2001), which may have been provided by reworking of previous basin deposits in the foreland (see section 4.2.3, this paper). Krabbendam *et al.* (2017) suggests a number of terranes in the Canadian sector of the Grenville Orogen as sources.



Figure 39: A) Schematic diagram displaying fluvial regime for distal transport of sediment from the Grenville Orogen. B) Modern analogue of (A); satellite image of the Gaghara River, India. A) Small distributary fans fill the Grenvillian foreland basin laterally. Orogen axial drainage occurs when channels reach the forebulge preventing further drainage away from the orogenic front. The fluvial regime of the orogen axial system is unknown as little is preserved in the rock record. B) After (Google Earth V 9.2.71.3, 2015a). Image is oriented to North. Distributary and distributary channels are visible flowing south from the Himalayas into the Gaghara river. Additional channels supply some sediment from the forebulge south of the river.

Krabbendam *et al.* (2017) propose several stages of development in the Grenvillian foreland basin, initiating with a narrow basin during deposition of the upper Sleat underlying the southern Torridon Group. The basin is interpreted to widen by the time of Applecross deposition, accommodating the broader extent of this formation (Krabbendam *et al.*, 2017). This model of transport provides clear, extant sources for the Applecross detrital zircon suite, combined with sufficient transport to provide an evenly distributed signal across the Applecross Formation.

Palaeocurrents within the Applecross Formation flow to the southeast. The model of Krabbendam *et al.* (2017) conversely implies transport to the northeast, although there is scope within the model to accommodate both possibilities. The key issue with this proposal lies in comparative widths of the Applecross Formation (~200km) and proposed orogen axial channel. In order to produce the brainplain facies and alluvial fans of the Applecross Formation the channel would need to supply sediment to the full ~200km width of the formation whilst maintaining flow perpendicular to the exposed outcrop (Figure 40). No provision is made in the model of Krabbendam *et al.* (2017) for a switch from a distal trunk system to the distributive systems required to generate this width of outcrop with similar detrital zircon signatures across the exposure.



Figure 40: Distribution of trunk river to supply the Applecross Formation. Initial trunk river flow direction after (Krabbendam *et al.*, 2017). Flow from the source area in the Krabbendam *et al.* (2017) model brings sediment from the southwest, perpendicular to observed palaeocurrents in the Applecross Formation. A possible solution is migration of the trunk system over time to deposit the full width of the Applecross Formation as braidplain facies.

4.3.3 Distally sourced distributive system

The key issue in determining the provenance of the Applecross Formation lies in the difficulty of reconciling the sedimentology and the detrital zircon geochronology. The sedimentology suggests a proximal source (Williams, 2001; Williams and Foden, 2011), whereas detrital zircon provenance studies indicate distal transport across Laurentia (Nicholson, 1993; Rainbird, Hamilton and Young, 2001; Owen and Santos, 2014; Krabbendam *et al.*, 2017). Unifying the proposals outlined in the previous sections requires conversion of an established foreland basin river system into a broad distributive system at its distal end. This scenario is initially considered unlikely, as it requires loss of confinement from the foreland basin to enable a distributive system to form.

An extant example of a similar system exists in northwestern Botswana (Figure 41). The Okavango Delta (a large scale alluvial fan) represents a ~150-200km wide inland distributive system fed by a trunk river system sourced from the Angolan Highlands (Hutchins, 1976). The Okavango Delta lies in a region underlain by Archean granitoid gneisses, quartz-feldspar porphyry (Kgwebe Formation), quartzites, shales, and limestones. The structure itself is underlain by fluvial sands and windblown deposits (Hutchins, 1976).



Figure 41: Satellite image of the Okavango Delta, Botswana. Annotations after (McCarthy *et al.*, 1997; image after Google Earth V 9.2.71.3, 2015b). The 'Panhandle' and alluvial fan areas of the Okavango Delta, Botswana. Distribution at the distal end of a trunk river system occurs due to change in slope related to extensional tectonics (see (Pike, 1970; Hutchins, 1976; McCarthy, Stanistreet and Cairncross, 1991; McCarthy *et al.*, 1997).

Channel morphology above the delta apex is meandering and bedload dominated, with minimal suspended load and channel width progressively narrowing down the delta (McCarthy, Stanistreet and Cairncross, 1991). Drainage leaks through defined channel levees due to a lack of suspended load to clog the peat which forms the levees (McCarthy, Stanistreet and Cairncross, 1991) to supply the perennial swamps present across the delta, draining overland at right angles to the main channels (Hutchins, 1976; McCarthy, Stanistreet and Cairncross, 1991; McCarthy *et al.*, 1997).

The Okavango Delta distributary system occurs due to a loss of confinement at the apex, with slope variations across the fan determined primarily by bedload and local tectonics (Hutchins, 1976; McCarthy *et al.*, 1997). Several faults alter the reach of seasonal flooding on the delta; seismic evidence indicate that the lower delta may have developed on an an arm of the East Africa rift system (Scholz, 1975; Hutchins, 1976). Although direct evidence is difficult to acquire due to the remote location of the delta and near total superficial cover, gravity surveys suggest some faults may have up to 1000m throw (Hutchins, 1976). The influence of tectonics on local drainage is highlighted by anecdotal reports of the Boro channel becoming a major distributary after an earthquake in 1952 (see Pike, 1970; Wilson, 1973) and by coincidence of slope changes in the delta with major fault lines, including a change in gradient from 1:5570 to 1:3400 at the delta apex where the Gumare Fault facilitates a loss of channel confinement (McCarthy *et al.*, 1997).

Fluvial style in the Okavango is not a perfect match for the high energy braided channels of the Applecross and Aultbea Formations; however a number of similarities can be drawn with the model of Applecross fluvial dynamics proposed by Owen and Santos (2014). A scarcity of mud lenses in the Applecross likely lead to increased permeability (Owen and Santos, 2014). Although clay beds are present underlying the sediments of the Okavango Delta (McCarthy, Stanistreet and Cairncross, 1991) suspended load is minimal, preventing peat levees in the system from becoming clogged and allowing leakage from channel bodies (McCarthy, Stanistreet and Cairncross, 1991). The Applecross Formation contains abundant soft sediment deformation not associated directly with flood events, having likely formed in areas of the system that remained waterlogged while inactive (Owen and Santos, 2014), a setting facilitated by high water

tables and seen in the perennial swamps in interchannel areas of the Okavango Delta (Hutchins, 1976; McCarthy, Stanistreet and Cairncross, 1991; McCarthy *et al.*, 1997).

In the Okavango Delta loss of discharge due to evaporation and transpiration allow only 2% of input flow at the apex to leave the fan edge (Nichols and Fisher, 2007). Transpiration is unlikely to have influenced the pre-vegetation Torridonian river systems, however rates of evaporation would not have been hindered by shade and groundcover from plants. Considering the similarities of sediments in the Okavango Delta and the Applecross Formation, it is possible that a similarly high degree of flow loss would occur in a Mesoproterozoic fan similar to the Okavango and subsequently a closed basin setting may not prohibit a terrestrial system.

The differences in morphology can be attributed to a number of possible influences, including the stabilising effect of modern vegetation and greater abundance of clays in the Okavango Delta (McCarthy, Stanistreet and Cairncross, 1991; McCarthy *et al.*, 1997), local climate, and slope angle relating to local tectonics. Although not an ideal sedimentological match for the Applecross, the Okavango Delta demonstrates the viability of a distally sourced, confined trunk river system forming a fan with radius great enough to provide sediment to the entire width of a group such as the Torridonian- extent of Torridonian ~200km (Sutton and Watson, 1964; Williams and Foden, 2011), width of Okavango Delta ~150km (Nichols and Fisher, 2007)-in an extensional tectonic setting (Pike, 1970; Scholz, 1975; Hutchins, 1976; McCarthy, Stanistreet and Cairncross, 1991; McCarthy *et al.*, 1997).

Alluvial fans in the Tarim basin may provide an alternative modern analogue to the Cape Wrath member; fans up to ~50km across contain conglomerates and sands in braided stream deposits (Wei *et al.*, 2013). Proximal fluvial systems similar to those supplying fans in the Tarim basin are unlikely to provide zircon suites as diverse or evenly distributed as those seen in the Applecross Formation without a source area at least 10⁴km² (see Williams and Foden, 2011) distributing from a single apex; fans emanating from multiple apexes would likely show greater variations than present. The aridity of the Tarim basin precludes the waterlogging required to facilitate soft sediment deformation such as that seen in the Applecross Formation.

A mode of deposition similar to that of the Okavango Delta fits the extensional half-graben setting proposed for the Applecross by Williams and Foden (2011) and the well-mixed detrital zircon record of the formation (this study, Rainbird, Hamilton and Young, 2001; Cawood *et al.*, 2007; Krabbendam *et al.*, 2017). The possibility of Applecross deposition in an extensional basin is further supported by periods of extension between Baltica and Laurentia in the period 1000-950Ma (Cawood *et al.*, 2004, 2007), coeval with deposition of the Torridonian. Extension in this period may have led to unconfinement of the orogen axial channel and formation of an alluvial fan on the scale of the Okavango Delta (Figure 42).



Figure 42: Proposed distributive fluvial regime for deposition of the Applecross Formation. 1) Detrital zircon geochronology supports an extensive Laurentian source area with transport occurring along a Grenvillian foreland basin in a trunk river system. 2) Palaeocurrents and sedimentology in the Applecross Formation support a local distributive system. Extensional faulting may have facilitated formation of a large alluvial fan similar in scale to the Okavango Delta, Botswana. 3) The apparent difference between distributive facies in the northern Applecross Formation and braidplain facies in the southern part of the formation may be an artefact of the

preserved outcrop and the scale of the original fan. A transect across the schematic fan may preserve parallel streams in the south whilst indicating a smaller fan similar to the Cape Wrath member further north. The fan schematic displayed is traced from satellite imagery of the Okavango Delta.

Chapter 5 Conclusions

5.1 Work done

In this study ²⁰⁶Pb/²³⁸U analysis of detrital zircon from the Applecross Formation is combined with sedimentological context to further elucidate the provenance and depositional style of the sediments. Sampling is undertaken on the Applecross Peninsula, along an east-west transect incorporating ~2000m of Applecross stratigraphy.

Detrital zircon ages display dominant clusters in the early-mid Mesoproterozoic (~1128-1397Ma) and late Palaeoproterozoic (~1630-1873Ma) with minor early Palaeoproterozoic (~2191Ma) and Archean (~2691-3069Ma) clusters. The oldest detrital zircon from sample SA21C has a ²⁰⁶Pb/²³⁸U age of 3346±43Ma. The youngest detrital zircon from sample SA8 has a ²⁰⁶Pb/²³⁸U age of 1018±14Ma. Detrital age peaks indicate that ages cover a ~1100Ma interval, from 1000-2100Ma with a lull between 1600-1500Ma, coincident with a major gap in magmatism in Laurentia.

Palaeocurrents and sedimentology within the Applecross Formation support a source to the west or northwest, possibly as part of a distributive system. On this basis Baltica is ruled out as a source, whilst Laurentia, Greenland, and the Rockall Plateau are considered geographically viable in models of continental configuration at the time of deposition.

Viable primary sources for detrital zircon suitable to generate the signature seen in the Applecross Formation are found along the extent of the Grenville Orogen foreland, particularly in the Canadian sector. Supracrustal formations such as the Yankee Joe and Blackjack Formations are suitable to provide reworked zircon within the 1600-1500Ma magmatic gap in Laurentia. Other workers propose a totally removed proximal supracrustal series as the source for the Applecross Formation (see Williams and Foden, 2011). A distal system transporting sediment from the Grenville foreland is preferred, combining elements from multiple previous models.

5.2 Palaeogeographic reconstructions

5.2.1 Previous work

Two primary transport and depositional regimes have been proposed for the Applecross Formation supported by different datasets;

- Sourcing from proximal supracrustal or removed basement rocks west of the Minch prior to deposition as a series of alluvial fan and braidplain facies is supported by palaeocurrent and sedimentological evidence from the Applecross Formation itself (see Nicholson, 1993; Williams, 2001; Williams and Foden, 2011). This proposal suffers from a lack of evidence for the proposed supracrustal series, which would have been at least 10⁴km² (Williams and Foden, 2011) to have supplied the volume of sediment required to produce the Applecross Formation.
- 2. The detrital zircon suite of the Applecross Formation (this study and others, see Rainbird, Hamilton and Young, 2001; Cawood *et al.*, 2007; Krabbendam *et al.*, 2017) supports distal source areas in the foreland of the Grenville Orogen. This extensive source area has the potential to provide the entire observed detrital zircon suite from basement and supracrustal rocks along its length. As yet most authors have not attempted to justify the proposed trunk river system with the distributive fans and broad braidplain facies of the Applecross exposure (see section 4.2 this study). Similar detrital zircon signatures throughout the Applecross support a single source or apex for these channels.

5.2.2 Distally sourced distributive model

On the basis of detrital zircon provenance analysis, evidence for distributive facies in the Applecross Formation, and extensional phases of Grenville tectonics coeval with deposition of the Applecross Formation, a Grenville foreland source area is supported. Transport of sediment occurred in an orogen axial trunk river system, providing thorough mixing of material from various terranes. Deposition occurred during extensional tectonics relating to the rotation of Baltica around Laurentia, which lead to loss of channel confinement to the west or northwest of the Minch Fault and Outer Hebrides Fault Zone (OHFZ) facilitating the formation of a large distributive fan similar in structure to the Okavango Delta, Botswana, or that proposed by Owen and Santos (2014), see Figure 41, Figure 42 section 4.3.3.

5.3 Further work

Further work is required to confirm current models of Applecross deposition:

- 1. Additional detrital zircon studies within areas of the formation not yet represented are required to determine the validity of a single apex or channel supplying the entire depositional system. Although current datasets support this, only a small number of localities are sampled (Applecross Peninsula- this study, Enard Bay- Rainbird, Hamilton and Young, 2001, Guinard Bay- Krabbendam *et al.*, 2017) see Figure 35, 4.1.
- 2. Further classification of palaeocurrents from the Applecross Formation as a whole is required to determine the validity of interpretation as a distributive feature. Comparative work on modern sedimentary flow indicators in the Okavango Delta may be beneficial in understanding the evidence seen in the limited (~40km X 200km) outcrop of the Applecross Formation.
- 3. reassessment of current detrital zircon U-Pb datasets using concordia ages following the methodology of Zimmermann *et al.* (2018) may improve the accuracy of analysis and subsequently provide further insight into potential source areas and sediment flux over the course of deposition.

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U-Pb analysis by LA-ICPMS: The use of core-rim ages and the single-analysis concordia age', *Sedimentary Geology*. Elsevier, 375, pp. 5-13. doi: 10.1016/J.SEDGEO.2017.12.020.

Chapter 6 Appendices

6.1 Appendix 1

6.1.1 Map of sample localities.

Holmes, Samuel, "Sample localities, Applecross" [PNG map], Scale 1:50000, DiGMapGB-50, [geospatial data], Updated: November 2018, Version 8, British Geological Survey (BGS), UK, Using: EDINA Geology Digimap Service, <http://digimap.edina.ac.uk/>, Created: November 2018 Sampling was undertaken on the Applecross Peninsula, Northwest Scotland (see Figure 35 section 4.1). Natural relief in the chosen study area allows collection of data and samples from a variety of stratigraphic levels. To achieve this a transect of the peninsula is sampled along the main road. Areas of alluvium displayed on the map contain bedrock outcrops and do not preclude sampling in the area, however additional care must be taken to ensure that sampled rocks are in situ where cover is abundant.



6.2 Appendix 2

6.2.1 LA-ICP-MS data tables

LA-ICP-MS U/Pb data table for detrital zircon containing, from left to right;

- Sample ID structured as <sample number><_grain number>_<spot number>.
- U/Pb, U/Th, and Pb/Pb isotope ratios corrected for background and gas blank. Ratios and errors for ²⁰⁶Pb/²³⁸U, ²⁰⁷Pb/²³⁵U, and ²⁰⁷Pb/²⁰⁶Pb are included.
- Calculated ages and deviation for ²⁰⁶Pb/²³⁸U, ²⁰⁷Pb/²³⁵U, and ²⁰⁷Pb/²⁰⁶Pb.
- U, Th, and Pb concentrations in PPM.
- U/Pb final ages.
- % Discordance between ²⁰⁶Pb/²³⁸U, and ²⁰⁷Pb/²⁰⁶Pb ages. In a closed system both ages should be the same- or concordant- discordance is a measure of similarity, the nearer discordance is to zero the more reliable the ages are likely to be. Percentage discordance alone is only an indicator of reliability and further investigations are made into highly discordant grains.
- Column 'X' contains information on the location of each analysed spot within either the core or rim of the grain. Spots marked 'C' are in the grain core, whilst spots marked 'R' are in the outer zones of the grain.
- The Notes column contains information on the quality of each grain or spot. Notes are brief and refer primarily to reasons for exclusion of a grain from further analysis or interpretation.

Spot name	206 /238	206 /238 2SE	207 /235	207 /235 2SE	207 /206	207 /206 2SE	U/Th Ratio	U/Th 2SE	206/204 Pb ratio	206 /204 2SE	U PPM	U PPM 2SE	Th PPM	Th PPM 2SE	Pb PPM	Pb PPM 2SE	206 /238 Age	206 /238 Age 2SE	207 /235 Age	207 /235 Age 2SE	207 /206 Age	207 /206 Age 2SE	% Discord- ance	х	Notes
SA2_0000_1	0.2928	0.0042	3.99	0.15	0.0956	0.0037	2.41	0.03	42000	25000	283.3	3.2	116.5	1.5	246.4	9.3	1654	21	1614	31	1476	76	-12.06	С	
SA2_0001_1	0.2187	0.0037	3.6	0.15	0.117	0.0049	0.913	0.011	106000	26000	276.6	3	297.5	3.7	399	10	1274	19	1532	34	1825	82	30.19		Cuts zones
SA2_0003_1	0.244	0.011	2.93	0.46	0.085	0.014	1.296	0.033	75000	19000	25.63	0.49	19.4	0.46	35.8	3.1	1395	57	960	160	430	340	-224.42	R	
SA2_0004_1	0.2816	0.0046	4.74	0.19	0.119	0.0049	1.209	0.015	261000	52000	224.9	2.8	180.5	2.6	383	13	1598	23	1753	33	1873	75	14.68		Cuts zones

Appendices

i																							1		
SA2_0004_2	0.282	0.0053	4.24	0.19	0.106	0.0048	0.97	0.013	153000	41000	163.2	3.4	164.1	4.1	300	13	1599	27	1660	38	1660	91	3.67	R	metamictiz
SA2_0005_1											0.253	0.074	0.058	0.082	405	21									ation
SA2_0006_1	0.191	0.011	1.66	0.58	0.067	0.026	1.323	0.035	12400	5800	24.79	0.68	19.26	0.57	43.4	5.2	1115	58	1230	150	-830	650	234.34	С	
SA2_0006_2	0.171	0.013	-0.1	1.2	0.014	0.092	1.09	0.049	-730	780	10.7	0.25	10.44	0.39	15.9	4.3	1002	69	1300	220	-5800	1800	117.28		Cuts resin
SA2_0008_1	0.304	0.005	4.41	0.18	0.1028	0.0044	3.722	0.057	-76000	26000	129.4	1.9	35.97	0.61	134.1	7	1709	25	1693	34	1584	85	-7.89	С	
SA2_0100_1	0.1931	0.0028	2.21	0.1	0.08	0.0036	2.083	0.023	30000	25000	239.8	2.6	119.6	1.6	239.8	9.1	1137	15	1165	32	1115	91	-1.97	R	Cuto
SA2_0100_2	0.1894	0.0039	2.46	0.16	0.0928	0.0062	0.597	0.008 3	-29000	16000	130.1	3.6	222.6	4.8	332	15	1117	21	1248	47	1350	130	17.26		zones Radiation
SA2_0105_1	0.2907	0.004	4.05	0.16	0.0983	0.0038	3.511	0.046	-105000	46000	224.8	5.4	65.6	1.9	225.5	9.6	1646	20	1624	32	1513	75	-8.79		damage
SA2_0106_2	0.2304	0.0045	2.94	0.16	0.0912	0.005	2.326	0.032	-54000	22000	135.3	1.7	58.41	0.91	149.9	7.2	1335	24	1362	43	1290	120	-3.49	R	
SA2_0107_1	0.2749	0.004	4.05	0.17	0.105	0.0045	1.821	0.021	460000	240000	203.7	2.1	110.5	1.3	296	11	1564	20	1624	34	1626	83	3.81		Cuts resin
SA2_0108_1	0.2823	0.0051	3.97	0.18	0.1002	0.0049	3.002	0.047	30000	22000	150.9	1.8	49.31	0.75	145.2	7.2	1601	26	1610	39	1529	92	-4.71	R	
SA2_0108_2	0.2882	0.005	4.26	0.19	0.1047	0.0046	1.75	0.019	30000	34000	169.4	2.5	93.7	1.4	308	12	1631	25	1656	37	1622	86	-0.55	R	Fractura
																									metamictiz
SA2_0201_1	0.2775	0.0047	3.94	0.22	0.1003	0.0057	1.998	0.033	-600000	220000	127.7	2.8	63	1.9	178.9	9	1577	24	1585	47	1490	120	-5.84		ation
SA2_0201_2	0.2821	0.0045	4.01	0.18	0.1012	0.0046	2.167 0.466	0.028 0.007	97000	57000	154.9	1.8	70.7	1	235.9	9.7	1600	23	1620	37	1550	92	-3.23	R	
SA2_0204_1	0.2216	0.0069	1.72	0.37	0.056	0.013	2	3	-80000	31000	34.31	0.53	73.49	0.84	208.5	9.2	1286	36	890	170	-260	390	594.62	R	Readings
																									too low to
SA2_0205_1											0.625	0.088	1.76	0.11	14	4.7									age
SA2_0206_1	0.1792	0.0026	3.314	0.06	0.1311	0.0026	1.191	0.012	640000	600000	865	10	755	12	1915	36	1062	14	1482	14	2094	35	49.28		Cuts zones
SA2_0206_2	0.249	0.0043	4.11	0.14	0.1166	0.0038	2.417	0.034	380000	160000	276.7	9	118.9	3.1	373	15	1432	22	1639	28	1858	61	22.93		Cuts resin
SA2_0207_1	0.2226	0.004	2.72	0.14	0.087	0.0047	1.258	0.013	216000	93000	196.7	3	165	2.8	354	13	1294	21	1305	42	1200	120	-7.83		damage
									- 131000																
SA2_0208_1	0.2693	0.0037	4.03	0.13	0.1053	0.0033	1.408	0.032	0	660000	471.3	5	364	10	531	15	1536	19	1625	26	1692	55	9.22		Cuts resin
SA2 0301 1	0 3075	0 0044	4 67	0 15	0 1068	0 0034	1 937	0.02	700000 0	220000 0	335.7	35	184	21	374	10	1727	21	1746	27	1703	64	-1 41	R	
SA2 0201 2	0 2106	0.0045	1 00	0.16	0 1100	0.0020	1 50	0.019	224000	-	214 6	2.2	202.0	24	27.		1740		1705	28	1776	62	1.01		Cuts zonos
SA2_0301_2	0.3208	0.0045	4.80	0.10	0.1109	0.0038	1.58	0.018	01000	50000	101	3.3	203.9	2.4	322	11 0 1	1742	22	1242	20	1190	220	1.91		Cuts zones
3AZ_0303_1	0.2208	0.0054	3.00	0.29	0.098	0.0095	1.202	0.017	91000	39000	1 101	1.5	19.8	1.1	122	0.1	1284	29	1342	00	1190	250	-0.01		cuts resin
SA2 0305 1	0.1266	0.002	2.683	0.086	0.1506	0.005	3.528	0.081	62000	87000	648	9.8	185.5	6.4	798	19	768	11	1314	24	2306	59	66.70	Cuts resin	
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 SA2 0306 1											- 0 315	0 076	- 0 178	0 089	-11	35								Cuts resin	
S/12_0300_1											-	0.070	0.170	0.005		5.5									
SA2_0306_2											0.083	0.08	-0.01	0.11	-4.3	4								Cuts resin	
SA2_0307_1	0.2379	0.0037	3.94	0.15	0.1174	0.0046	0.837	0.013	99000	95000	253.4	5.4	294.4	4.4	392	15	1374	19	1608	31	1860	72	26.13	Cuts resin	
SA2_0308_1	0.3228	0.0044	5.16	0.17	0.1131	0.0035	1.573	0.027	-250000	170000	288.8	3.2	183.3	2.9	491	12	1802	22	1829	28	1808	57	0.33	Cuts resin Metamicti	
SA2_0401_1	0.224	0.012	0.89	0.78	0.021	0.025	1.346	0.04	-18100	8800	21.33	0.43	16.23	0.42	30.8	4.9	1292	60	1510	150	-2480	820	152.10	zation	
																					- 1440				
SA2_0406_1	0.208	0.024	5.4	3.1	0.05	0.77	13.2	7.2	-38000	53000	7.24	0.29	1.52	0.19	20.6	5	1160	130	2430	240	0	9300	108.06	Cuts resin	
SA2_0406_2											0.029	0.09	-0.19	0.11	-4.5	4.2								Cuts resin	
SA2_0407_1	0.1889	0.0027	2.917	0.094	0.1094	0.0034	3.476	0.056	-380000	150000	531.2	5.5	157.7	3.3	437	14	1116	15	1376	24	1757	59	36.48	Cuts resin	
SA2_0408_1	0.2209	0.0049	2.66	0.17	0.0867	0.0055	1.291	0.02	-111000	47000	167.6	2	131	1.7	187.2	7.6	1284	26	1281	49	1150	130	-11.65	inclusion	
SA2_0409_2	0.5	0.12	15.2	9.6	0.49	0.58	0.87	0.11	-3600	3000	2.96	0.23	3.62	0.25	15.5	5.5	2320	490	3330	230	-4100	5300	156.59	Cuts resin	
SA2_0500_2	0.2908	0.0042	4.6	0.18	0.1127	0.0043	1.501	0.015	-123000	62000	238.5	2.7	153.7	1.8	340	13	1647	22	1727	32	1785	69	7.73	Cuts resin	
SA2_0500_3	0.2129	0.004	3.86	0.17	0.1275	0.0051	0.815	0.016	-80000	51000	262.9	9.9	310	13	443	20	1243	21	1590	35	2028	74	38.71	Cuts resin	
SA2_0501_1	0.2989	0.0055	4.63	0.21	0.1106	0.0051	2.825	0.043	220000	85000	152.3	1.7	52.23	0.79	161.8	7.9	1683	27	1728	38	1716	89	1.92	Cuts resin	
SA2_0503_1	0.2956	0.0055	4.26	0.21	0.1015	0.0051	1.395	0.018	-19000	29000	153.4	1.6	107.6	1.3	218.8	9.9	1667	27	1657	43	1583	98	-5.31	R	
SA2_0503_2	0.2839	0.0054	4.54	0.22	0.1141	0.0053	1.387	0.022	-700000	300000	144.6	2.2	104.2	2.1	175.8	8.5	1609	27	1710	41	1785	87	9.86	Cuts resin	
											- 0.069	0.001	0.088	0.000											
SA2_0505_1											6	7	49	6	6	1.3								Cuts resin	
SA2_0506_1	0.1842	0.004	2.09	0.14	0.0802	0.0052	2.007	0.033	103000	31000	157	2.3	80.6	1	115.6	6.2	1088	22	1098	47	990	150	-9.90	Cuts resin	
SA2_0506_3	0.1932	0.0033	2.137	0.097	0.0789	0.0035	2.253	0.031	163000	49000	280.6	2.9	130.5	1.9	208.4	7.9	1138	18	1146	33	1072	96	-6.16	Cuts zones	
SA2_0508_1	0.185	0.0037	4.06	0.16	0.1595	0.0067	1.019	0.019	78000	24000	187.4	5.2	190.1	3.7	320	13	1093	20	1635	34	2401	73	54.48	Cuts resin	
SA2_0509_1	0.2878	0.0047	4.07	0.15	0.1	0.0036	1.385	0.015	996000	230000	244.9	2.9	181.8	2.1	467	11	1629	24	1630	29	1565	68	-4.09	R	
SA2_0509_2	0.1426	0.002	3.7	0.088	0.1844	0.0045	0.613 6	0.005 4	196000	43000	683	9.3	1130	18	1328	29	859	11	1563	20	2671	41	67.84	Cuts resin	
SA2_0602_1	0.338	0.014	4.65	0.53	0.1	0.012	1.571	0.058	25500	7600	26.1	1.6	17.4	1.1	38.8	4	1865	65	1470	140	1050	270	-77.62	Cuts resin	
SA2 0604 1	0.2297	0.0036	4.71	0.16	0.1455	0.0051	0.981 9	0.009 7	162000	43000	287.2	4.2	290.5	3.9	547	14	1332	19	1750	29	2248	63	40.75	Cuts resin	
SA2 0605 1	0.2819	0.0052	43	0.15	0.11	0 0041	1 12	0.013	140000	40000	197.2	2.7	175 7	23	461	13	1598	26	1682	30	1736	69	7 95	C	
	0.2019	3.0052		5.15	0.11	5.00.1		5.010	1.0000				2, 5.7	2.0			2000		1002		2,00		, ,,,,,,	-	

											1												1		
SA2_0605_2	0.2058	0.0035	3.47	0.14	0.1194	0.0047	1.091	0.014	119000	27000	268.4	3.1	248.4	3.9	535	15	1205	19	1506	31	1896	72	36.45		Cuts resin
											0.018	0 000	-	0.000											
SA2_0606_1											6861	0079	691	071	2.1	1.2									Cuts resin
SA2_0608_1	0.3837	0.008	18.47	0.62	0.3404	0.0093	1.46	0.028	53000	13000	130.7	2.5	92.4	3	1420	63	2089	37	2995	33	3646	42	42.70		Cuts resin Radiation
SA2_0701_1	0.1483	0.0018	2.798	0.067	0.1338	0.0029	5.32	0.12	303000	71000	1685	19	344	10	1366	56	891	10	1348	18	2125	39	58.07		damage
SA2_0702_1	0.1824	0.0074	1.8	0.23	0.0735	0.0097	4.32	0.13	8100	3600	53.42	0.88	13.51	0.43	19	2.6	1074	40	882	90	430	260	-149.77		ation
SA2_0702_2	0.178	0.0061	1.55	0.2	0.0648	0.0089	1.765	0.038	17200	4900	54.93	0.88	33.82	0.71	46.1	3.9	1056	33	803	92	210	260	-402.86		Cuts resin
SA2_0704_1	0.1753	0.0085	1.94	0.29	0.085	0.014	0.919	0.021	6600	2200	38.22	0.82	45.4	1	44.5	3.9	1039	47	870	110	440	320	-136.14	С	
SA2_0704_2								I			0.055	0.023	0.004	0.016	-0.37	0.72	I								Cuts resin
SA2_0705_1	0.27	0.005	3.88	0.17	0.1027	0.0045	1.029	0.015	80000	22000	194.2	2.5	189.6	3.2	340	11	1539	25	1581	38	1570	92	1.97		Cuts resin
_1	0.325	0.0078	4.55	0.24	0.1044	0.006	0.933	0.013	34000	12000	81	1.7	86.8	1.8	206.7	8.5	1809	38	1716	47	1560	110	-15.96	С	
_1	0.2528	0.0035	4.386	0.092	0.1255	0.0025	1.101	0.02	222000	56000	600.1	6.3	548	12	1009	19	1452	18	1703	17	2016	36	27.98		Cuts zones
SA3_1_0008 _1	0.2016	0.0029	3.624	0.099	0.1307	0.0035	0.393 5	0.007 1	99000	26000	423	16	1046	26	942	36	1183	16	1545	21	2077	50	43.04		Cuts resin
CA2 1 0000							0.167	0.000																	Fracture,
SA3_1_0008 _2	0.1747	0.0039	3.82	0.18	0.1598	0.0075	0.167	0.003 3	27600	9000	163.4	7.1	943	27	425	16	1037	21	1573	38	2367	85	56.19		damage
SA3_1_0103 _1	0.3182	0.0061	4.55	0.18	0.1048	0.0041	0.757	0.007 8	49000	17000	159.6	2.5	206.4	3.2	603	14	1778	30	1723	34	1643	77	-8.22		zation
SA3_1_0103 _2	0.3461	0.0078	4.9	0.25	0.1031	0.0052	1.139	0.015	18700	9100	89.8	1.2	77.5	1.2	237.3	8.8	1911	37	1776	44	1580	100	-20.95	R	
SA3_1_0104 _1	0.296	0.0046	4.89	0.12	0.1202	0.0031	1.133	0.038	114000	35000	390.8	6.1	356	12	635	21	1670	23	1795	21	1942	46	14.01	с	
SA3_1_0105 1	0.1992	0.0039	2.07	0.12	0.0766	0.0047	1.056	0.012	34000	10000	157	2.4	147.4	2.2	289	9	1170	21	1100	44	910	140	-28.57	с	
	0 2777	0.005	4 11	0 13	0 1085	0 0039	0.683 7	0.006 9	65000	19000	184.4	3.6	269.9	59	440	12	1577	25	1647	27	1721	69	8 37	c	
SA3_1_0107	0.2102	0.0076	2.26	0.13	0.076	0.0035	1 701	0.022	12800	4200	E2 47	0.92	205.5	0.62	440 60 E	20	1077	20	1071	27	660	220	02.49	D	
_1 SA3_1_0107	0.2192	0.0076	2.20	0.25	0.078	0.0079	0.675	0.009	12800	4200	52.47	0.82	51.19	0.02	50.5	5.0	1277	59	10/1	01	000	220	-95.46	N	
_2 5A2 1 0201	0.2152	0.0043	2.25	0.12	0.0761	0.004	2	1	68000	17000	172.3	3.1	260.5	6.4	504	14	1255	23	1169	39	950	110	-32.11		Cuts zones
_1	0.296	0.0051	4.2	0.15	0.1038	0.004	1.045	0.012	74000	29000	195.9	3.5	191.6	4.1	484	13	1669	25	1664	31	1634	76	-2.14	R	
_1	0.298	0.005	4.05	0.14	0.0996	0.0034	2.613	0.029	93000	41000	277.7	4.3	108.2	1.8	274.5	9.1	1679	25	1641	27	1586	63	-5.86	R	
SA3_1_0203 _1	0.3095	0.0066	4.27	0.23	0.1005	0.0055	2.056	0.031	45000	15000	100.5	1.4	49.76	0.86	130.6	5.7	1735	33	1657	48	1520	120	-14.14	С	
SA3_1_0204 _1	0.203	0.014	1.78	0.42	0.089	0.028	1.233	0.047	2600	1100	12.01	0.34	10.28	0.35	16.7	2.1	1181	73	600	160	-390	400	402.82	С	

SA3_1_0205 1	0.1553	0.0026	2.189	0.089	0.1024	0.0039	1.139	0.013	69000	19000	325.3	4.7	287.6	4	363	11	930	15	1160	28	1598	73	41.80		Cuts resin
SA3_1_0206	0.3358	0.0076	4.59	0.24	0.101	0.0056	1.295	0.021	12800	7200	68.45	0.89	53.32	0.84	163	6.2	1862	37	1721	45	1510	110	-23.31	С	
	0 2463	0 0047	2 94	0 15	0 0859	0 0043	2 335	0.039	37000	11000	141.6	19	61 1	12	118 1	61	1417	24	1358	40	1220	110	-16 15		Cuts resin
_1 SA3_1_0208	0.2403	0.0047	2.54	0.15	0.0055	0.0045	2.555	0.035	57000	11000	141.0	1.5	01.1	1.2	110.1	0.1	1417	24	1550	40	1220	110	10.15		cuts resin
_1 SA3_1_0209	0.3131	0.0088	4.58	0.33	0.1068	0.0078	3.382	0.085	12400	4300	46.82	0.65	14.07	0.31	44.3	3.5	1749	43	1682	63	1530	150	-14.31	R	
_1 \$42,1,0200	0.2783	0.0053	3.49	0.15	0.092	0.004	1.486	0.019	28000	10000	122.4	2	82.4	1.5	230.5	8.3	1580	27	1502	35	1384	91	-14.16	С	
_2	0.2373	0.0042	2.74	0.14	0.085	0.0043	1.584	0.024	42000	12000	166.1	6	105.8	4.9	263	12	1373	22	1317	37	1180	110	-16.36		Cuts zones
SA3_1_0301																									radiation
_1 \$43_1_0302	0.2631	0.0044	3.26	0.13	0.0904	0.0035	2.359	0.027	23000	13000	182.5	2.7	76.7	1.1	190.7	7.2	1504	22	1454	30	1358	77	-10.75		damage
_1	0.5284	0.0091	16.25	0.37	0.2237	0.0041	1.334	0.027	157000	36000	222	3	167.5	3.8	383	20	2730	39	2883	22	2997	30	8.91	С	
_1	0.2114	0.0069	2.15	0.21	0.0762	0.0081	1.172	0.02	8500	3100	43.71	0.76	37.07	0.7	78.5	4.7	1232	36	1062	76	680	210	-81.18	С	
SA3_1_0305 _2	0.2502	0.0068	2.65	0.23	0.0792	0.0071	1.177	0.021	16700	5200	56.08	0.77	47.61	0.77	116.1	5.4	1439	36	1217	75	810	190	-77.65	с	
SA3_1_0306 1	0.5392	0.0072	13.87	0.26	0.1874	0.003	1.122	0.01	251000	74000	298.6	5.3	264.6	5.3	1300	26	2780	30	2734	18	2708	27	-2.66	R	
																									Cuts
_1 SA3_1_0307	0.3319	0.0053	5.13	0.2	0.1132	0.0046	2.994	0.066	55000	21000	132.1	1.9	44.32	0.76	129.1	5.9	1845	26	1815	35	1778	79	-3.77		inclusion
_2 SA3 1 0307	0.3469	0.0087	5.1	0.32	0.1087	0.0069	1.895	0.078	24800	8400	49.38	0.72	27.39	0.93	69.1	4.4	1914	42	1785	58	1590	140	-20.38	R	
_3 _3	0.2497	0.0035	4.493	0.094	0.1316	0.0027	1.201	0.011	322000	67000	620	12	513	11	920	19	1436	18	1723	17	2098	37	31.55		Cuts zones
_2	0.2486	0.0047	2.95	0.17	0.0862	0.0051	1.7	0.023	45000	15000	120	1.7	70.2	1.3	159.2	6.5	1429	25	1356	45	1170	130	-22.14	С	
SA3_1_0308 _3	0.2527	0.0066	3.06	0.22	0.0882	0.0063	1.662	0.027	30000	9900	86.1	1.3	51.71	0.87	108.5	5.8	1456	35	1375	56	1180	150	-23.39		Cuts zones
SA3_1_0400 _1	0.2277	0.0043	2.81	0.12	0.0913	0.0042	1.463	0.023	52000	20000	191.7	2.6	132.3	3.2	204.6	7.8	1321	22	1336	33	1346	90	1.86	R	
SA3_1_0400	0.245	0.0056	2 22	0.17	0 1005	0.0055	1 427	0.024	50000	15000	120.8	2.1	08.6	2.1	1577	7	1/10	20	1457	41	1/00	110	5 27	c	
_2 SA3_1_0401	0.245	0.0050	5.52	0.17	0.1005	0.0055	1.427	0.024	50000	15000	135.0	2.1	58.0	2.1	157.7	,	1410	23	1457	41	1490	110	5.57	C	
_1 SA3_1_0402	0.1973	0.0054	2.02	0.16	0.077	0.0061	1.331	0.019	15100	6900	81.6	1.3	61.41	0.94	89.8	4.4	1158	29	1069	58	830	170	-39.52	R	
_1 SA3_1_0402	0.3103	0.005	4.5	0.15	0.1061	0.0035	3.183	0.043	123000	32000	239	2.6	75.6	1.1	183.9	6.5	1740	25	1721	27	1696	63	-2.59	С	
_2 \$42.1.0404	0.2641	0.0034	4.43	0.11	0.1222	0.0027	1.234	0.012	259000	65000	631	10	519	11	628	14	1510	17	1709	21	1967	41	23.23	R	
_1	0.1887	0.0037	1.86	0.11	0.0726	0.0043	1.734	0.022	38000	14000	176.6	2.3	103.7	1.6	132.7	6	1113	20	1034	39	820	130	-35.73	R	
SA3_1_0405 _1	0.3087	0.0073	4.55	0.25	0.1085	0.0061	0.766 3	0.009 8	31000	11000	92.3	1.5	123	2	246.4	8.6	1730	36	1700	49	1640	110	-5.49	с	
SA3_1_0406	0 2106	0.0049	156	0.14	0 1076	0 0024	2 001	0 022	105000	42000	324.9	11	150 1	22	336.6	Q 1	17/2	24	1776	26	1716	56	-1 5 2	c	
- -	0.3100	0.0049	4.50	0.14	0.1070	0.0054	2.094	0.022	102000	42000	1 324.0	4.4	109.1	2.5	550.0	9.1	1/42	24	1/20	20	1/10	50	-1.52	C	

542 1 0407							0.051	0.000			1												1		
SA3_1_0407	0 1851	0.0033	2 24	01	0.0888	0 0042	0.951	0.009	61000	21000	264.6	3.6	286	4 1	272 1	79	1094	18	1180	32	1307	97	16 30	R	
SA3 1 0408	0.1001	0.0055	2.24	0.1	0.0000	0.0042	0.684	0.009	01000	21000	204.0	5.0	200	4.1	272.1	7.5	1004	10	1100	52	1307	57	10.50	i.	
_1	0.1895	0.0051	1.91	0.17	0.0745	0.0067	7	3	22300	7600	100.2	1.4	149.6	2.3	196	6.8	1116	28	1005	63	690	190	-61.74	С	
SA3_1_0500																									
_1	0.3206	0.0045	5.25	0.13	0.1202	0.0027	1.735	0.021	311000	77000	644.9	9.6	379.2	7.4	557	13	1791	22	1854	21	1935	40	7.44		Cuts zones
SA3_1_0501							0.658	0.008																	
_2	0.2382	0.0042	3.27	0.13	0.1015	0.0043	5	5	59000	21000	231	2.7	355.5	5.5	453	13	1376	22	1456	32	1569	83	12.30		Cuts zones
SA3_1_0502	0.0404	0.0054	4.50	0.40	0 4 0 5 0	0.000	2 007	0.001	400000	10000	240.0		152.6		270 4		4705	25		22	4.600	50	5.00	~	
_L \$A2_1_0E02	0.3194	0.0051	4.50	0.13	0.1052	0.003	2.087	0.024	108000	40000	319.9	4.4	153.6	2.4	378.4	9.9	1/85	25	1/41	23	1689	53	-5.68	C	Cuto
1	0 2509	0.0054	3 35	0.18	0 0981	0.0053	0 97/	0.012	29000	12000	129.2	3.6	131 7	33	253	10	1///1	28	1/157	11	1/160	110	1 30		inclusion
	0.2309	0.0034	5.55	0.18	0.0381	0.0055	0.974	0.012	29000	12000	129.2	3.0	131.7	5.5	255	10	1441	20	1457	44	1400	110	1.50		Inclusion
2	0.2787	0.006	3.52	0.2	0.0928	0.0053	1.544	0.023	24700	8600	93.8	1.3	59.49	0.87	151.1	6.1	1582	30	1486	46	1310	120	-20.76	R	
_1	0.2345	0.0053	2.61	0.17	0.0821	0.0056	2.501	0.039	18100	7100	96.4	1.2	37.6	0.66	83.1	4.7	1356	28	1253	50	1030	150	-31.65	R	
SA3_1_0505																									
_1	0.282	0.0044	4.25	0.15	0.1109	0.0039	0.556	0.008	63000	17000	194.1	2.9	340.8	8.2	918	17	1600	22	1668	29	1756	67	8.88	R	
SA3_1_0506									~~~~~			-													
_1	0.1892	0.003	2.074	0.078	0.081	0.0032	1.293	0.012	65000	17000	2/9./	5	208.6	4.1	3/1	11	1116	16	1125	26	1158	79	3.63		Cuts zones
SA3_1_0507	0 2160	0.0055	2 /1	0.16	0.001	0.0055	1 000	0.015	12600	E100	77 4	1 1	60 0	1	150.7	6 5	1260	20	1202	ED	1020	150	22.20		Cute rocin
	0.2109	0.0055	2.41	0.10	0.001	0.0055	1.000	0.015	12000	5100	//.4	1.1	08.8	1	150.7	0.5	1209	30	1202	52	1030	150	-23.20		Cuts resin
1	0.2459	0.0032	3.266	0.079	0.0974	0.0022	4.31	0.11	143000	49000	671	11	160.3	6.3	357	12	1416	16	1465	19	1548	43	8.53	R	
_2	0.2678	0.005	3.45	0.14	0.095	0.0039	2.683	0.055	63000	17000	193.9	2.3	74	1.9	84.9	4.8	1527	25	1495	33	1437	86	-6.26		Cuts zones
SA3_1_0509																									
_1	0.3177	0.0075	4.76	0.27	0.1102	0.0058	1.716	0.032	33300	9900	101.9	1.8	61.22	0.89	156	9.6	1774	36	1739	48	1670	100	-6.23	С	
SA3_1_0600	0.0047	0.0005	2.04	0.10	0.0050	0.005.4	0.044	0.012	25000	7400	02.0	1.2	04.4	1.0	475.4	67	1510	22	1270	50	1120	120	22.62		
_L \$A2_1_0601	0.2647	0.0065	3.04	0.19	0.0858	0.0054	0.944	0.012	25900	7400	83.9	1.3	94.1	1.6	1/5.1	6.7	1510	33	1378	50	1130	130	-33.03	к	
3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	0 2433	0.0057	3 22	0 19	0 0976	0.0056	0 946	0.015	38000	11000	118.2	3 9	135 3	3.6	154.4	76	1401	30	1434	45	1450	120	3 38		Cuts zones
SA3 1 0602	0.2455	0.0057	5.22	0.15	0.0570	0.0050	0.540	0.015	50000	11000	110.2	5.5	155.5	5.0	134.4	7.0	1401	50	1454	45	1450	120	5.50		cuto zoneo
_1	0.2487	0.0046	2.85	0.14	0.0848	0.0043	1.473	0.02	68000	17000	174.4	2.5	136.8	2.3	185.8	7.2	1430	24	1350	38	1200	100	-19.17	R	
SA3_1_0603							1.014	0.007																	
_1	0.1	0.0015	3.281	0.058	0.2417	0.0043	1	3	45000	6000	1714	27	1935	27	2638	44	614	8.5	1472	14	3121	28	80.33		Fracture
SA3_1_0604							0.773	0.009																	
_1	0.2846	0.0056	4.2	0.18	0.1093	0.005	4	2	55000	19000	143.4	3	210.3	5	277	10	1612	28	1651	36	1693	91	4.78	С	_
SA3_1_0604	0 0050	0.0076	4.50	0.00	0.4046	0.0057		0.017	24000	45000			00.0		466.4	6.5	4044	27	4746	42	4500				Cuts
_Z	0.3259	0.0076	4.58	0.23	0.1046	0.0057	1.1//	0.017	34000	15000	104.4	1.4	98.2	1.6	166.4	6.5	1814	37	1/16	43	1580	110	-14.81		inclusion
SA3_1_0005	0 208	0.0044	4.05	0.14	0 1006	0 0038	0 875	0.011	126000	36000	250.7	28	208.4	11	520	12	1690	22	1626	20	1562	75	-7.49	c	
SA3 1 0606	0.250	0.0044	4.05	0.14	0.1000	0.0050	0.075	0.011	120000	30000	250.7	2.0	500.4	4.1	520	12	1000	22	1020	50	1505	75	7.45	C	
1	0.192	0.007	2.24	0.27	0.085	0.01	1.063	0.022	16200	5100	53.18	0.86	50.39	0.85	34.2	3	1127	38	1026	92	730	250	-54.38	с	
_1	0.2743	0.0055	3.37	0.19	0.0913	0.0052	1.317	0.016	69000	21000	153	1.7	115.8	1.4	181.8	6.7	1563	28	1473	46	1340	110	-16.64	С	
SA3_1_0607																									
_2	0.257	0.011	3.43	0.41	0.104	0.014	0.994	0.067	6000	3500	32.3	0.73	38.4	2.6	22.1	2.4	1473	56	1310	110	990	270	-48.79	R	

SA3_1_0608																									
_1	0.511	0.016	11.39	0.69	0.168	0.011	0.648	0.014	34800	8200	35.24	0.6	53.95	0.9	151	5.8	2648	66	2499	61	2370	120	-11.73	С	
SA3_1_0608	0.534	0.015	40.70	0.05	0.470	0.040	0.644	0.010	20700	6000	20 72	0.57	46.5			6.2	2745	62	2504	60	2400	420	10.00		<u>.</u>
_2	0.534	0.015	12.78	0.85	0.178	0.012	0.614	0.013	20700	6800	28.73	0.57	46.5	1	141.5	6.3	2745	63	2584	68	2480	120	-10.69		Cuts zones
5A3_1_0009	0 2222	0.0048	2 5 7	0.15	0.0853	0.005	1 157	0.017	25000	12000	128.0	12	119 /	25	207.1	Q /	1207	25	1250	45	1120	120	-14 78	c	
	0.2252	0.0048	2.57	0.15	0.0855	0.005	1.157	0.017	33000	13000	130.5	4.5	110.4	5.5	207.1	0.4	1257	25	1250	43	1150	130	-14.70	C	
1	0.193	0.0028	2.052	0.072	0.0787	0.0027	1.574	0.013	115000	38000	471.8	8.2	295.5	5.3	460	12	1137	15	1126	24	1091	73	-4.22	R	
_2	0.1952	0.0037	2.03	0.098	0.0775	0.0038	1.45	0.015	28000	14000	192.2	2.8	130.9	1.9	215.3	7.1	1148	20	1112	34	1020	100	-12.55	С	
SA3_1_0702																									
_1	0.1885	0.0025	1.948	0.075	0.0756	0.0028	2.014	0.022	97000	24000	314.8	4.3	154.9	2.6	265.5	8.6	1112	14	1083	26	1037	78	-7.23	R	
SA3_1_0702	0.40000	0.00.47	2.45	0.46	0 0007	0.0000		0.000	224.00	6000	02.2		52.52	0.00	0F F		4427	25	4420	50	4000	4.60	40.70		Cuts
_2 5A2 1 0702	0.1933	0.0047	2.15	0.16	0.0827	0.0062	1.74	0.022	22100	6900	92.3	1.6	52.52	0.88	95.5	4.6	1137	25	1130	52	1000	160	-13.70		inclusion
SA3_1_0703	0 197/	0.0057	1 97	0.18	0.0745	0 0069	1 76	0.036	13800	1200	54.61	0.83	31.04	0.76	52.2	3.4	1158	30	1039	67	730	190	-58 63	R	
	0.1574	0.0057	1.57	0.10	0.0745	0.0005	1.70	0.050	13000	4200	54.01	0.05	51.04	0.70	52.2	5.4	1150	50	1055	07	/50	150	50.05	Ň	
3	0.1967	0.0056	1.98	0.19	0.0771	0.0076	0.917	0.014	17500	4100	52.67	0.93	56.79	0.86	102	5.4	1158	31	1030	73	750	210	-54.40	R	
_2	0.3072	0.0048	4.27	0.14	0.1025	0.0032	1.561	0.015	101000	29000	252.1	3	159.2	1.9	513	12	1725	24	1674	28	1631	58	-5.76	R	
SA3_1_0706																									
_1	0.3239	0.0079	4.29	0.29	0.0997	0.007	2.159	0.043	18100	5000	42.34	0.74	19.43	0.44	59.6	4.3	1804	39	1628	61	1370	150	-31.68	R	
SA3_1_0/0/	0 2022	0.000	4.44	0.17	0 1001	0.0042	1 (20)	0.021	47000	10000	120.0	2	70		255	0.1	1705	20	1024	24	1550	01	10.00		Cuts
_L \$A3 1 0708	0.3033	0.006	4.11	0.17	0.1001	0.0042	1.638	0.021	47000	16000	129.9	2	/8	1.4	255	8.1	1705	29	1634	34	1550	81	-10.00		Inclusion
3A3_1_0708 1	0 3247	0 0048	4 74	0.13	0 1087	0.003	2 186	0.03	129000	37000	315.9	32	142.8	2	311	10	1814	23	1768	23	1745	50	-3.95	c	
	0.3247	0.0040	4.74	0.15	0.1007	0.005	2.100	0.05	125000	57000	515.5	5.2	142.0	2	511	10	1014	25	1/00	25	1745	50	5.55	C	
_2	0.32	0.0052	4.68	0.16	0.1089	0.0041	3.266	0.045	65000	20000	177.1	2.1	53.53	0.79	165.4	6.3	1787	25	1751	30	1730	74	-3.29	R	
SA3_1_0708																									
_3	0.3187	0.0048	4.66	0.14	0.108	0.0034	3	0.042	114000	24000	226.6	2.6	75	1.2	215.1	8	1784	24	1745	27	1714	59	-4.08	R	
SA3_1_0804																							-		
_1	0.254	0.014	2.76	0.51	0.079	0.016	3.85	0.23	1730	730	9.94	0.26	2.83	0.15	5.3	1.2	1451	74	810	170	40	380	3527.50		Cuts zones
SA3_1_0804	0 2278	0.005	2 72	0.12	0 0802	0.004	0.900	0.009	27000	12000	171 1	10	101 2	2.2	287.0	00	1221	26	1217	25	121/	05	-0.52	D	
	0.2278	0.005	2.72	0.15	0.0092	0.004	0 562	0.005	37000	12000	1/1.1	1.5	191.5	2.2	207.5	0.0	1521	20	1317	33	1514	55	-0.55	N	
1	0.1663	0.0023	4.238	0.079	0.1884	0.0032	3	2	39900	5700	1080	15	1981	21	2530	31	991	13	1676	15	2715	28	63.50		Cuts zones
_2	0.228	0.0037	2.7	0.13	0.0872	0.0041	1.146	0.029	54000	16000	217	8.4	209	13	309	17	1323	19	1306	35	1260	100	-5.00	С	
SA3_1_0900																									
_1	0.3001	0.0047	4.01	0.14	0.0991	0.0036	1.07	0.011	72000	21000	210.6	3.2	206.3	3.4	378	11	1690	23	1628	29	1559	71	-8.40	R	
SA3_1_0900																									Cuts
_2	0.3097	0.005	4.22	0.17	0.1017	0.0042	1.271	0.018	65000	20000	196.7	2.4	162.8	2.9	208	7.3	1740	24	1659	33	1572	80	-10.69		inclusion
3	0.2444	0.0035	4 16	0.12	0 1262	0 0038	0.359	0.003	165000	40000	451 2	6.8	1310	22	1647	28	1/09	18	1650	24	2016	53	30.16		inclusion
_3 SA3 1 0903	0.2444	0.0035	4.10	0.12	0.1203	0.0000	J	0	103000	-0000	-31.5	0.0	1313	~~	1047	20	1400	10	1055	24	2010	55	50.10		menusion
1	0.2186	0.0036	2.92	0.11	0.0987	0.0035	1.878	0.038	178000	43000	401	6.5	227.1	7.5	273	12	1273	19	1372	30	1541	71	17.39	R	
											-														Radiation
_1	0.2209	0.0053	2.52	0.16	0.0849	0.0056	0.983	0.013	43000	16000	133.8	2.1	140.2	2	175.3	6.5	1284	28	1237	47	1120	140	-14.64		damage

SA3_1_0904	0 236	0.012	2 65	0 41	0 087	0 014	1 325	0 042	7600	2900	24 29	0 51	19 36	0.61	21.2	22	1361	65	990	130	490	320	-177 76	R	
	01200	01012	2100	0.11	0.007	0.01	1.020	0.012	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	2500	225	0.01	10.00	0.01		2.2	1001	00	550	100	150	020	1,,,,,,,		
_2 SA3_1_1000	0.507	0.0084	12.21	0.32	0.178	0.0045	0.924 0.759	0.013	185000	54000	186.2	5.3	206.3	7.7	602	22	2640	36	2611	24	2619	44	-0.80	R	
_1	0.2349	0.0041	2.97	0.12	0.0939	0.0041	6	9	119000	29000	211.8	3	280.5	4	414	10	1359	21	1378	33	1406	89	3.34	С	
SA3_1_1001	0.2568	0.0041	2 21	0.11	0 0028	0 0033	2 075	0.026	11/000	37000	202.7	12	140.8	28	222.6	74	1472	21	1446	28	1/29	67	-2.26	D	
_2 SA3_1_1002	0.2308	0.0041	5.21	0.11	0.0928	0.0033	2.075	0.020	114000	37000	233.7	4.5	140.8	2.0	232.0	7.4	1472	21	1440	20	1458	07	-2.30	ĸ	
_2 \$A2 1 1002	0.3302	0.0059	4.82	0.15	0.1092	0.0035	3.351	0.046	114000	37000	236.4	3.5	70.1	1.3	181.3	6.6	1836	29	1779	28	1738	61	-5.64	R	
_1	0.22	0.011	2.67	0.46	0.096	0.017	2.83	0.14	4600	1400	12.74	0.25	4.8	0.24	6.8	1.3	1271	59	940	150	410	370	-210.00	R	
SA3_1_1003	0 1022	0.0024	2.45	0.11	0.0020	0.0045	1 200	0.016	46000	14000	105.0	1.0	120.2	1.2	100 7	7	1125	10	1112	26	1110	110	0.44		Cute and in
_2	0.1923	0.0034	2.15	0.11	0.0839	0.0045	1.366	0.016	46000	14000	- 105.8	1.9	- 120.3	1.3	190.7	/	1135	18	1143	30	1140	110	0.44		Cuts resin
CA2 4 4004											0.001	0.000	0.001	0.000											<u>.</u>
SA3_1_1004 _1											1245	0.000	1616	0008 7	0.56	0.63									inclusion
SA3_1_1006							0.429	0.004							1700										
_2 SA3 1 1007	0.222	0.0031	3.989	0.095	0.1331	0.0031	/ 0.804	1 0.008	128000	29000	352.4	4.1	819	8.3	1729	25	1291	16	1626	19	2122	40	39.16		Cuts zones
_1	0.2983	0.0058	4.11	0.18	0.1023	0.0044	9	9	45000	12000	94.5	1.1	117.3	1.5	403	11	1680	29	1634	35	1577	82	-6.53	С	
SA3_1_1008 1	0.2255	0.0033	2.77	0.076	0.0916	0.0025	1.997	0.022	89000	28000	297.2	3.8	148.9	1.8	362.1	9.7	1310	17	1338	21	1424	53	8.01	R	
							0.612																		
_1 SA3 1 1103	0.3851	0.005	11	0.17	0.2119	0.0028	2	0.005	233000	50000	403.8	6.3	660.8	9.4	1653	23	2098	23	2518	14	2915	21	28.03	С	Cuts
_1	0.2481	0.0068	2.79	0.19	0.0859	0.0061	2.113	0.039	17500	4400	46.58	0.73	22.27	0.46	70.2	4.1	1424	35	1319	52	1120	150	-27.14		inclusion
SA3_1_1103 2	0.2428	0.005	2.89	0.17	0.0878	0.0049	2.07	0.031	18800	7000	74.8	2.3	36.5	1.1	107.2	5.3	1399	26	1344	47	1250	120	-11.92	с	
_ SA3_1_1104											_												_		
_1 SA3 1 1104	0.2793	0.004	4.43	0.13	0.118	0.0034	0.868	0.019	106000	26000	237.2	5	285	11	636	17	1586	20	1705	24	1890	52	16.08	R	
_2	0.2949	0.0048	5.55	0.26	0.1378	0.0055	1.043	0.021	135000	28000	264.6	6.3	254.7	7.7	954	40	1664	24	1872	41	2128	73	21.80		Cuts zones
SA3_1_1105	0 2918	0 0049	4 74	0.16	0 1077	0 0039	2 139	0 071	62000	17000	138.2	2	67 1	18	145 5	61	1649	24	1660	32	1695	72	2 71	R	
	0.2510	0.0045	4.24	0.10	0.1077	0.0035	2.135	0.071	02000	1,000	150.2	-	07.1	1.0	145.5	0.1	1045	24	1000	52	1055	, 2	2.71	i.	
_1 \$42.1.1106	0.2104	0.0075	2.39	0.23	0.087	0.0091	1.572	0.034	12200	3100	34.93	0.56	22.78	0.43	40.3	3.5	1230	40	1145	80	930	220	-32.26	R	Cute
_2	0.2097	0.0047	2.3	0.13	0.0823	0.0051	1.811	0.028	35000	10000	108.1	1.5	60.7	1	108.6	5.1	1225	25	1177	43	1070	130	-14.49		inclusion
SA3_1_1107	0 2008	0.0049	2 10	0.15	0.0775	0.0052	1 01	0.027	26500	8200	04.6	1 2	E2 91	0.79	00.6		1225	26	1124	50	020	140	21 72	D	
_2 SA3_1_1108	0.2098	0.0048	2.18	0.15	0.0775	0.0053	1.81	0.027	26500	8300	94.0	1.2	52.81	0.78	90.6	4.4	1225	20	1154	50	930	140	-31.72	к	Radiation
_1	0.1965	0.0038	2.17	0.13	0.0828	0.005	1.226	0.016	50000	11000	133.1	2.7	109.8	2.7	186.5	8	1155	21	1133	43	1070	130	-7.94		damage Boodings
																									too low to
											0.000	0.07	2 72	0.15	11.0	1 5									calculate
SA4_0005_1											U.838	0.07	2.73	0.15	11.6	1.5									age

SA4 0007 1 -2.78 0.2954 0.0056 4.03 0.18 0.1046 0.005 1.779 0.023 44000 10000 120.4 1.6 67.8 1.1 143.3 5.2 1666 28 1622 38 1621 96 С SA4 0008 3 0.0065 1549 1442 R 0.2974 3.73 0.19 0.0955 0.0048 1.434 0.02 43800 9500 106.2 1.3 74.2 1 159.6 5.6 1679 31 42 94 -16.44 SA4_0104_1 0.2845 0.0081 3.71 0.27 0.1015 0.0076 1.781 0.038 20800 4600 52.92 0.78 29.92 0.48 65.7 3.9 1608 41 1506 63 1370 170 -17.37 R SA4_0104_2 0.0076 0.1023 0.0075 0.034 1618 -10.82 0.2862 3.84 0.28 1.737 21500 4500 50.01 0.69 28.94 0.49 60.5 3.7 38 1547 62 1460 150 Cuts zones Not a SA4 0105 1 0.091 0.047 2.98 0.71 58.7 8.5 0.76 0.15 0.522 1510 480 1.477 0.091 0.13 45.4 3 3210 320 4130 140 3820 630 15.97 zircon SA4 0108 1 0.0066 0.1834 2.15 0.16 0.0924 0.0066 1.454 0.052 27300 6500 110.8 9.2 71.2 4.8 74.8 5.8 1081 36 1128 49 1260 150 14.21 Cuts resin SA4_0108_2 0.2276 0.005 0.17 0.0833 0.0055 0.029 8800 117.5 58.88 109.3 1319 51 1050 150 -25.62 С 2.5 2.027 41600 1.3 0.8 4.8 26 1218 SA4 0200 2 0.2798 0.004 3.92 0.12 0.1064 0.0034 2.147 0.049 67000 18000 213.7 2.7 101.7 2 134.6 5.5 1589 20 1607 25 1700 60 6.53 Cuts resin 0.002 0.000 0.000 -5115 0002 0.001 0000 SA4_0207_1 6 9 2723 58 -0.4 0.45 Cuts resin SA4_0300_1 0.2184 0.004 2.6 0.12 0.0908 0.0044 1.197 0.014 53000 12000 167.6 196.5 1272 21 1275 35 1333 97 4.58 С 2.3 144.4 2.7 6.6 20.07 SA4_0301_1 0.2281 0.0047 3.21 0.16 0.1072 0.0053 0.93 0.02 38900 9100 126.8 2.2 140.8 2.2 143.8 5.4 1322 24 1435 38 1654 98 Cuts resin SA4_0301_2 0.0061 1725 -3.60 R 0.3074 4.32 0.2 0.1066 0.0048 1.809 0.028 47900 9400 95.5 1.3 54.55 0.84 131.8 5.3 30 1675 41 1665 92 SA4_0302_1 0.274 0.004 3.9 0.12 0.1084 0.0033 1.818 0.032 128000 27000 314.4 3.6 179.3 2.9 232.3 6.8 1560 21 1602 26 1728 60 9.72 С SA4_0302_2 0.2156 0.0042 3.22 0.13 0.113 0.0044 3.16 0.044 88000 18000 269 4.4 87.5 1.8 155.2 5.5 1257 22 1446 31 1793 75 29.89 Cuts zones Cuts SA4_0303_1 0.0053 193.8 1313 1420 0.2257 2.89 0.18 0.098 0.0062 0.903 0.014 31600 6600 95.2 1.6 106.1 1.5 6.8 27 1340 49 130 7.54 inclusion SA4_0303_2 0.2303 0.0063 2.78 0.19 0.0923 0.0063 2.342 0.047 22400 5000 70.4 30.77 0.6 54.9 3.4 1332 33 1301 54 1250 150 -6.56 R 1.1 metamictiz SA4 0304 2 0.24 0.23 0.01 2.54 0.086 0.012 2.75 19.94 0.38 7.51 14.5 1.8 1326 53 1060 120 700 -89.43 0.34 0.1 6500 1500 290 ation metamictiz SA4_0305_1 0.293 0.01 4.16 0.35 0.114 0.01 2.009 0.047 11200 2900 33.55 0.59 16.96 0.38 39.7 2.5 1646 51 1605 69 1450 190 -13.52 ation SA4 0306 1 0.2916 0.0063 3.98 0.22 0.1045 0.006 0.861 0.011 39300 8200 96.1 1.3 111.5 1.5 253.2 7.6 1646 31 1588 47 1540 120 -6.88 С Cuts SA4_0307_2 0.1551 0.0026 1.776 0.077 0.0869 0.0039 1.317 0.016 60000 15000 360.7 3.8 274.3 4.1 251.4 7.7 929 15 1025 30 1270 93 26.85 inclusion SA4_0308_1 0.2702 0.0049 3.64 0.16 0.1026 0.0048 2.209 0.072 56000 12000 149.4 2.7 68.9 1.7 104.7 5.2 1540 25 1533 37 1569 87 1.85 Cuts resin Cuts SA4_0401_1 0.1975 0.0041 2.99 0.0038 2.135 0.028 101000 19000 334.2 4.3 156.9 2.5 218.2 7.2 1160 22 1389 26 1813 62 36.02 inclusion 0.1 0.1143 SA4_0401_2 0.3119 0.0051 4.33 0.15 0.1042 0.0034 3.858 0.054 79000 19000 213.5 3.4 55.6 1.1 133.9 5.3 1748 25 1684 28 1652 63 -5.81 R Cuts SA4_0402_1 0.2229 0.004 2.98 0.12 0.1011 0.0043 1.117 0.017 68000 15000 239 4.5 215.2 2.8 287 9 1296 21 1386 31 1573 82 17.61 inclusion SA4_0403_2 0.3191 0.0058 4.79 0.2 0.1143 0.005 2.669 0.037 61000 14000 158.1 1.7 60.41 0.89 147.7 5.6 1783 28 1762 37 1797 81 0.78 R

1											1												1		
SA4_0404_1	0.1823	0.0061	1.83	0.21	0.0786	0.0093	1.317	0.029	11300	2600	48.11	0.76	37.55	0.75	54.9	3.3	1076	33	927	86	620	240	-73.55	Cuts r	esin
SA4_0404_2	0.1841	0.0051	1.97	0.16	0.0823	0.0072	1.91	0.036	17400	4100	74.7	1.1	40.25	0.69	62.1	3.8	1087	27	1034	62	890	190	-22.13	R	
SA4_0405_1	0.2606	0.0069	3.88	0.25	0.1128	0.0074	1.345	0.029	23600	5200	66.6	1.2	52	1.6	69.6	4.4	1489	35	1555	54	1680	130	11.37	Cuts r	esin
SA4_0405_3	0.3071	0.0047	4.3	0.15	0.1057	0.0038	2.084	0.025	90000	19000	203.7	2.3	100.9	1.4	235.3	8.1	1724	23	1683	29	1674	69	-2.99	R	
SA4_0407_1											0.086	0.022	0.41	0.053	16.3	2								Cuts r	esin
SA4_0407_2	0.3085	0.0045	4.35	0.13	0.1054	0.0032	1.752	0.019	107000	23000	243.9	3.3	144.4	2.2	323.5	9.2	1732	22	1691	26	1691	58	-2.42	R	
SA4_0407_3	0.3137	0.0061	4.47	0.19	0.108	0.0047	2.263	0.037	26000	8400	96.7	1.4	44.38	0.73	115.1	5.1	1756	30	1700	37	1667	84	-5.34	R	
SA4_0408_3	0.1875	0.0043	2.03	0.14	0.0828	0.0058	2.162	0.03	21300	5400	103.6	1.4	49.64	0.7	73.9	4.2	1106	23	1083	49	1020	150	-8.43	Cuts r	esin
SA4_0500_1	0.2402	0.0087	3.58	0.24	0.1141	0.0078	0.804	0.018	23500	5400	73.3	2.1	95.6	4.2	139.8	5.8	1380	45	1488	58	1650	150	16.36	Cuts r	esin
SA4_0500_3	0.3176	0.0058	4.98	0.19	0.1176	0.0047	1.049	0.012	39000	10000	134.7	1.9	132.1	1.8	330	7.8	1775	28	1793	33	1850	73	4.05	Cuts z	ones
SA4_0501_2	0.301	0.0042	4.53	0.14	0.1129	0.0035	1.686	0.026	122000	27000	305.4	4	186	2	359	9.3	1695	21	1721	26	1802	58	5.94	Cuts r	esin
SA4_0503_1	0.1894	0.0078	1.99	0.23	0.085	0.011	3.21	0.22	10200	2100	36.1	1.4	12.47	0.62	11.8	2	1112	42	973	91	730	260	-52.33	Cuts r	esin
SA4_0503_2	0.2526	0.006	3.21	0.2	0.0952	0.006	1.437	0.021	24900	6200	86.7	1.1	61.44	0.91	126.9	5.4	1448	31	1406	51	1340	130	-8.06	R	
SA4_0504_1	0.2825	0.0055	3.85	0.21	0.1025	0.0056	0.727	0.009 8	33400	7100	88.2	1.2	122.8	1.4	274.5	8.6	1601	28	1575	44	1590	100	-0.69	R	
																								Cuts zones,	,
SA4 0505 2	0.1675	0.0026	2.108	0.066	0.0956	0.0032	1.397	0.013	96000	19000	426.5	4.1	303.8	3.1	338	9.7	998	14	1152	23	1496	62	33.29	fractu inclusi	re, ion
 SA4 0506 1	0.22	0.03	20	1 2	0 209	0.063	1 27	0 1 2	480	170	2.64	0.14	2 16	0.12	2 5 2	0 02	1270	150	220	520	-11/0	650	211.40	metar	nictiz
SA4_0500_1	0.23	0.03	10.04	0.20	0.203	0.003	2.046	0.12	97000	20000	177 1	2.2	2.10	1 5	2.55	0.95	2270	20	250	24	2756	20	17.56	Cuts a	ones
SA4_0000_1	0.4230	0.0030	1 907	0.25	0.1343	0.0045	2.040	0.023	97000	20000	656.5	6.5	204.8	2.9	209.5	11	770	14	1072	24	1750	55	55 71	Cuts z	ocin
SA4_0001_1	0.1285	0.0024	2 /1	0.000	0.1103	0.0038	1 1 2 7	0.024	15100	21000	51	1	J04.8	1.5	77 0	11	1/70	20	12072	76	1735	100	-19.27	Cuts n	esin
SA4_0604_1	0.2300	0.0070	2 698	0.25	0.0883	0.0005	2 311	0.020	100000	21000	364	19	152.7	2.8	234.6	79	1322	17	1317	27	1270	73	-0.08	Cuts r	ocin
SA4_0606_1	0.2276	0.0032	3 //5	0.050	0.0005	0.0032	2.511	0.041	6800	1600	21.26	0.42	7 35	0.23	17.5	23	1618	59	1230	130	800	290	-102.25	Not zi	ircon
SA4_0608_1	0.280	0.012	2.45	0.45	0.095	0.013	0.947	0.11	38800	8100	179 1	3.6	18/ 9	0.25	175.8	2.5	1018	21	1230	38	1180	120	102.25	Cuts r	ocin
SA4_0608_2	0.2272	0.0030	2.05	0.11	0.0873	0.0045	1 929	0.015	32700	7400	175.1	1.0	64.41	0.91	99.5	1.8	1318	25	1257	50	1120	140	-17.68	Cuts 7	ones
SA4_0700_1	0.183	0.0045	2.05	0.17	0.1209	0.0057	3 739	0.020	36700	8300	181 1	3.2	/8 7	1 1	73.2	4.0	1085	20	1381	40	1878	98	17.00	Cuts r	ocin
SA4 0700 2	0.103	0.0033	12 27	0.15	0.1203	0.000	1 /11/	0.00	140000	34000	249 /	2.9	176 9	2.2	667	13	27/2	34	2607	21	270/	34	-1 //	Cute 7	ones
5A4_0700_2	0.3313	0.0079	13.57	0.23	0.1072	0.0038	1.414	0.014	140000	1500	55.0-	2.5	170.3	2.2	54.0	1.5	2/43		2037	21	2704	54	-1.44	Cuts	
SA4_0702_1	0.2907	0.0088	3.88	0.27	0.1009	0.007	2.403	0.048	26600	4500	55.37	0.79	23.33	0.42	54.9	3./	1639	43	1569	58	1460	140	-12.26	inclusi	on

SA4_0702_2	0.2792	0.0078	3.48	0.26	0.0935	0.0074	1.816	0.041	17400	3600	49.49	0.73	27.99	0.54	44.2	3.3	1582	39	1457	61	1200	170	-31.83	Fra ra da	acture, diation amage
SA4_0705_1	0.58	0.72	35	60	-4.1	8.6	0.36	0.17	900	1500	0.885	0.07	3.11	0.17	14.1	1.9	2200	2100	4100	1400	1900 00	3800 00	101.16	Cu in	its clusion
SA4_0707_2	0.1952	0.0039	2.44	0.13	0.0925	0.0048	2.034	0.04	52000	11000	199.1	2.6	101.9	2.1	167.4	7.5	1148	21	1223	38	1360	110	15.59	Cu	uts resin
SA4_0707_3	0.2723	0.0054	3.66	0.15	0.1002	0.0042	1.271	0.019	60000	12000	162.6	1.8	131.5	2	278.6	7.8	1550	27	1543	33	1552	81	0.13	Cu	uts resin
SA4_0800_2	0.2562	0.0041	3.153	0.098	0.0925	0.003	2.207	0.023	89000	23000	337.8	4.5	156.6	2.3	322	10	1469	21	1438	25	1420	63	-3.45	R	
											0.001	0.000	0.000	0.000											
SA4_0806_1											3214	0002 3	8856 8	0001 1	1.75	0.88								Cı	uts resin
SA4_0808_1	0.2743	0.004	4.09	0.12	0.1108	0.0031	2.152	0.03	140000	28000	374.8	3.4	178	2.5	269.5	7.4	1561	20	1641	23	1778	52	12.20	Cı	uts resin
SA4_0808_2	0.3119	0.0063	4.44	0.24	0.1051	0.0053	2.813	0.051	40200	8800	103	1.6	37.25	0.83	92.7	4.7	1747	31	1682	45	1620	100	-7.84	R	
SA4_0900_1	0.1785	0.0052	1.95	0.16	0.0823	0.007	0.639 2	0.008 4	14000	3700	78	1.1	122.5	1.5	181.4	6.5	1056	28	1033	60	920	180	-14.78	Cı	uts zones
SA4_0900_2	0.1764	0.0062	1.72	0.19	0.0727	0.0081	0.946	0.015	13900	3000	57.54	0.87	61.3	1.1	91.1	5.1	1043	34	918	76	610	230	-70.98	R	
SA4_0902_1	0.2637	0.0055	3.85	0.17	0.1083	0.0046	2.177	0.052	69000	13000	171.1	6.3	78.2	3	93.2	5.1	1506	28	1574	37	1696	86	11.20	Cı	uts resin
																								Cu zo	uts ones,
SA4_0902_3	0.3015	0.0055	4.3	0.19	0.1063	0.0048	2.519	0.034	71000	15000	177.5	2.7	70.5	1.2	151.6	6.5	1696	27	1677	36	1671	83	-1.50	in	clusion
SA4_0903_1	0.2541	0.0044	3.47	0.14	0.1019	0.0044	1.573	0.02	52000	12000	179	4.7	113	2.9	172.3	6.8	1458	23	1503	33	1570	83	7.13	Cu	uts zones
SA4_0903_2	0.1999	0.0059	2.07	0.19	0.0756	0.007	1.59	0.03	15600	3500	62.65	0.94	39.24	0.62	63.1	4.2	1171	32	1049	69	750	200	-56.13	R	
SA4_0905_2	0.0944	0.0015	1.4	0.044	0.1095	0.0032	8	9	88000	21000	891	13	927	12	442	13	581	9.1	884	18	1766	53	67.10	Cu	uts zones
SA4_0906_1	0.316	0.0053	4.52	0.17	0.1056	0.004	2.522	0.035	69000	14000	161.5	2.2	64	1.2	170.2	6.8	1768	26	1718	33	1671	75	-5.80	Cu in [,]	its clusion
SA4_0908_1	0.209	0.0051	2.52	0.18	0.0907	0.0068	1.35	0.028	23400	4600	77.9	1.1	58.1	1.4	87	4.5	1221	27	1237	51	1230	150	0.73	Cı	uts resin
SA4_0908_2	0.231	0.0069	2.5	0.24	0.0803	0.0079	1.589	0.034	11800	2800	44.81	0.91	28.26	0.68	49.6	3.4	1335	36	1152	82	780	220	-71.15	Cu in	its clusion
SA5 0004 2	0.431	0.044	59.5	6.7	0.98	0.17	0.944	0.069	-1170	260	25	1.4	29	1.5	506	46	2230	200	3950	120	4800	1200	53.54	ZO CL	ne utter
SA5 0005 2	0 231	0.026	23	0.94	0 174	0.061	1 81	0.25	50600	5600	37 5	2	25.9	16	87	10	1310	140	170	220	-830	490	257.83	zo	ine
SA5_0005_2	0.231	0.020	2.5	0.54	0.174	0.001	1.01	0.25	57800	4600	9/.5	2	56.7	2.3	100	20	1299	83	570	180	-400	410	424 75	Cu	uts resin
SA5_0006_1	0.220	0.017	2.40	0.71	0.005	0.025	0.845	0.08	13300	1800	116	5 2 1	59.7	2.5	37	13	751	95	10	190	-400	520	287.75	си С	
SA5_0006_1	0.129	0.0002	2.06	0.71	0.174	0.040	1 601	0.00	104900	1000	107 1	5.2	110 1	4.7	37 20E	10	1101	50	050	120	-400	320	_424.20	Cu c.	ute zonoc
3A5_0000_2	0.10/9	0.0092	2.00	0.55	0.074	0.012	1.091	0.005	104000	0400	19/.1	5.2	110.1	4.4	205	25	1101	50	050	120	210	320	-424.29	Cu	113 201165

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| 0.2235 | 0.0087 | 3.26 | 0.33 | 0.107 | 0.012 | 1.548 | 0.048 | 126600

 | 5400

 | 300.5 | 7.9 | 188.1 | 5.4 | 365 | 35
 | 1293 | 46
 | 1300
 | 100 | 1200 | 260 | -7.75
 | Cuts | resin |
| 0.191 | 0.0066 | 3.51 | 0.29 | 0.139 | 0.013 | 1.246 | 0.027 | 112100

 | 7600

 | 453 | 13 | 340 | 12 | 649 | 48
 | 1126 | 36
 | 1412
 | 79 | 1740 | 210 | 35.29
 | Cuts | resin |
| 0.224 | 0.018 | 1.49 | 0.6 | 0.066 | 0.029 | 1.64 | 0.11 | 17300

 | 1400

 | 67 | 2.7 | 41.6 | 2.2 | 57 | 12
 | 1274 | 94
 | 120
 | 180 | -1410 | 410 | 190.35
 | Cuts | resin |
| | | | | | | | |

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 | 0.034 | 0.000 | 0.053 | 0.000 | 1 1 | 4
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 | Cutc | rocin |
| | | | | | | | |

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 | 5065 | 79 | 01 | 11 | 1.1 | 4
 | |
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 | | | |
 | Radia | tion |
| 0.263 | 0.016 | 2.76 | 0.66 | 0.082 | 0.02 | 1.424 | 0.066 | 150600

 | 9800

 | 97.2 | 3 | 64.1 | 2.6 | 105 | 14
 | 1490 | 84
 | 670
 | 190 | -270 | 410 | 651.85
 | dama | ge |
| 0.209 | 0.019 | 2.26 | 0.66 | 0.153 | 0.051 | 2.79 | 0.24 | 23100

 | 2300

 | 62.9 | 2.9 | 24.2 | 1.7 | 29.5 | 8.5
 | 1220 | 110
 | 510
 | 180 | -530 | 470 | 330.19
 | Cuts 2 | zones |
| 0.218 | 0.013 | 2.82 | 0.42 | 0.122 | 0.021 | 1.889 | 0.085 | 35600

 | 2500

 | 144.5 | 4.4 | 72.7 | 2.9 | 92 | 15
 | 1256 | 69
 | 1060
 | 140 | 780 | 360 | -61.03
 | Cuts 2 | zones |
| | | | | | | | |

 |

 | 0.030 | 0.000 | 0.087 | 0.000 | |
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 | 047 | 013 | 4 | 68 | 0.2 | 4.1
 | |
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 | | | |
 | Cuts i | resin |
| 0.263 | 0.025 | 2.49 | 0.71 | 0.117 | 0.039 | 2.2 | 0.2 | 14600

 | 1400

 | 53 | 2.5 | 26.1 | 1.6 | 40 | 10
 | 1470 | 130
 | 470
 | 190 | -540 | 470 | 372.22
 | R | |
| | | | | | | | |

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 | | | | | 8.716 | 0.006
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 | 0.78 | 0.25 | 1.03 | 0.31 | 6 | 3
 | |
 |
 | | | |
 | Cuts | resin |
| 0.338 | 0.024 | 2.91 | 0.64 | 0.076 | 0.019 | 1.146 | 0.062 | 21600

 | 1500

 | 64.2 | 2.5 | 57.9 | 2.6 | 96 | 13
 | 1830 | 110
 | 710
 | 190 | -240 | 410 | 862.50
 | Cuts i
zone | resin |
| 0.075 | 0.009 | 0.2 | 0.23 | 0.187 | 0.063 | 0.752 | 0.031 | 7190

 | 940

 | 71.2 | 2.9 | 95 | 3.8 | 54 | 11
 | 456 | 53
 | -115
 | 90 | -1350 | 550 | 133.78
 | cutte | r |
| 0.34 | 0.017 | 4.1 | 0.65 | 0.1 | 0.017 | 2.44 | 0.13 | 68400

 | 5000

 | 95.8 | 4 | 41.6 | 2.2 | 82 | 12
 | 1863 | 82
 | 1210
 | 160 | 620 | 340 | -200.48
 | R | |
| 0.1887 | 0.0086 | 2.36 | 0.34 | 0.101 | 0.015 | 1.274 | 0.051 | 87400

 | 5800

 | 226.8 | 9.5 | 184.6 | 9.7 | 218 | 21
 | 1107 | 46
 | 1000
 | 120 | 810 | 320 | -36.67
 | Cuts 2 | zones |
| 0.245 | 0.01 | 2.98 | 0.33 | 0.102 | 0.012 | 1.991 | 0.07 | 133700

 | 5400

 | 200.2 | 5 | 101.8 | 3.4 | 142 | 15
 | 1401 | 53
 | 1220
 | 100 | 1050 | 260 | -33.43
 | Cuts | resin |
| | | | | | | | |

 |

 | 2.27 | 0.41 | 2.97 | 0.62 | 5 | 4.1
 | |
 |
 | | | |
 | Cuts | resin |
| 0.191 | 0.01 | 1.78 | 0.29 | 0.081 | 0.013 | 1.812 | 0.063 | 53600

 | 3000

 | 159.4 | 6.8 | 88.7 | 4.4 | 97 | 14
 | 1115 | 55
 | 820
 | 120 | 310 | 330 | -259.68
 | Cuts | resin |
| 0.292 | 0.019 | 3.58 | 0.7 | 0.123 | 0.03 | 1.88 | 0.11 | 37800

 | 2500

 | 71.4 | 2.4 | 40.5 | 2.1 | 54 | 11
 | 1619 | 95
 | 900
 | 190 | 180 | 410 | -799.44
 | Cuts | resin |
| 0.1037 | 0.0059 | 1.5 | 0.23 | 0.12 | 0.02 | 0.757 | 0.031 | 46300

 | 3200

 | 266.7 | 9.3 | 351 | 15 | 137 | 16
 | 632 | 34
 | 765
 | 99 | 900 | 360 | 29.78
 | Cuts | resin |
| 0.149 | 0.029 | 0.79 | 0.85 | 0.313 | 0.069 | 0.902 | 0.08 | 3090

 | 570

 | 19.1 | 1.2 | 23.4 | 1.3 | 26.4 | 7.1
 | 830 | 150
 | -310
 | 250 | 510 | 660 | -62.75
 | Cuts | resin |
| 0.223 | 0.026 | 1.55 | 0.78 | 0.196 | 0.066 | 1.23 | 0.12 | 23600

 | 2600

 | 25.7 | 1.3 | 23.5 | 1.6 | 29.9 | 7.2
 | 1240 | 130
 | -250
 | 250 | -950 | 540 | 230.53
 | Cuts | resin |
| 0.368 | 0.016 | 6.22 | 0.71 | 0.122 | 0.014 | 5.61 | 0.34 | 91800

 | 4200

 | 137.1 | 3.9 | 25.9 | 1.5 | 64 | 11
 | 2000 | 73
 | 1720
 | 140 | 1350 | 270 | -48.15
 | Cuts | resin |
| 0.339 | 0.018 | 4.6 | 0.65 | 0.099 | 0.014 | 1.81 | 0.08 | 54900

 | 3600

 | 125.1 | 5 | 67.4 | 3.1 | 153 | 17
 | 1860 | 83
 | 1360
 | 160 | 790 | 310 | -135.44
 | R | |
| 0.316 | 0.014 | 4.35 | 0.58 | 0.096 | 0.013 | 1.916 | 0.081 | 68600

 | 3700

 | 140.6 | 4.4 | 71.5 | 3.1 | 169 | 18
 | 1763 | 68
 | 1360
 | 140 | 810 | 300 | -117.65
 | Cuts 2 | zones |
| 0.2 | 0.011 | 2.71 | 0.42 | 0.094 | 0.015 | 2.46 | 0.11 | 49800

 | 3300

 | 155.8 | 5 | 60.8 | 2.8 | 72 | 12
 | 1161 | 59
 | 1000
 | 140 | 590 | 340 | -96.78
 | Cuts | resin |
| | 0.2235
0.191
0.224
0.263
0.209
0.218
0.263
0.338
0.075
0.34
0.338
0.375
0.191
0.292
0.1037
0.149
0.223
0.368
0.339
0.316
0.2 | 0.22350.00870.1910.00660.2240.0180.2630.0190.2180.0130.2630.0250.3380.0240.0750.0090.340.0170.18870.00860.2450.010.1910.010.2450.010.1920.0190.1930.0160.1940.0290.10370.00590.1490.0290.2330.0260.3680.0160.3390.0180.3160.0140.20.014 | 0.2235 0.0087 3.26 0.191 0.0066 3.51 0.224 0.018 1.49 0.263 0.016 2.76 0.209 0.019 2.26 0.218 0.013 2.82 0.263 0.025 2.49 0.338 0.024 2.91 0.338 0.024 2.91 0.34 0.017 4.1 0.1887 0.0086 2.36 0.245 0.01 2.98 0.191 0.01 1.78 0.292 0.019 3.58 0.1037 0.0059 1.5 0.149 0.029 0.79 0.223 0.026 1.55 0.368 0.016 6.22 0.339 0.018 4.6 0.316 0.014 4.35 | 0.22350.00873.260.330.1910.00663.510.290.2240.0181.490.60.2630.0162.760.660.2090.0192.260.660.2180.0132.820.420.2630.0252.490.710.3380.0242.910.640.0750.0090.20.230.340.0174.10.650.18870.00862.360.340.2450.011.780.290.1910.011.780.290.10370.00591.50.230.1490.0290.790.850.2330.0166.220.710.3390.0184.60.650.3160.0144.350.580.20.0112.710.42 | 0.2235 0.0087 3.26 0.33 0.107 0.191 0.0066 3.51 0.29 0.139 0.224 0.018 1.49 0.6 0.066 0.263 0.016 2.76 0.66 0.082 0.209 0.019 2.26 0.66 0.153 0.218 0.013 2.82 0.42 0.122 0.338 0.025 2.49 0.71 0.117 0.338 0.024 2.91 0.64 0.076 0.075 0.009 0.2 0.23 0.187 0.34 0.017 4.1 0.65 0.1 0.1887 0.0086 2.36 0.34 0.101 0.245 0.01 2.98 0.33 0.102 0.191 0.01 1.78 0.29 0.081 0.292 0.019 3.58 0.7 0.123 0.1037 0.029 0.79 0.85 0.313 0.223 0.026 1.55 0.78 0.194 0.368 0.016 6.22 0.71 | 0.2235 0.0087 3.26 0.33 0.107 0.012 0.191 0.0066 3.51 0.29 0.139 0.013 0.224 0.018 1.49 0.6 0.066 0.029 0.263 0.016 2.76 0.66 0.082 0.02 0.209 0.019 2.26 0.66 0.153 0.051 0.218 0.013 2.82 0.42 0.122 0.021 0.263 0.025 2.49 0.71 0.117 0.039 0.338 0.024 2.91 0.64 0.076 0.019 0.338 0.025 2.49 0.71 0.117 0.039 0.338 0.024 2.91 0.64 0.076 0.019 0.34 0.017 4.1 0.65 0.1 0.017 0.1887 0.0086 2.36 0.34 0.101 0.015 0.245 0.01 2.98 0.33 0.102 0.012 0.191 0.01 1.78 0.29 0.85 0.313 0.069 | 0.2235 0.0087 3.26 0.33 0.107 0.012 1.548 0.191 0.0066 3.51 0.29 0.139 0.013 1.246 0.224 0.018 1.49 0.6 0.066 0.029 1.64 0.263 0.016 2.76 0.66 0.082 0.02 1.424 0.209 0.019 2.26 0.66 0.153 0.051 2.79 0.218 0.013 2.82 0.42 0.122 0.021 1.889 0.263 0.025 2.49 0.71 0.117 0.039 2.2 0.338 0.024 2.91 0.64 0.076 0.019 1.146 0.075 0.009 0.2 0.23 0.187 0.063 0.752 0.34 0.017 4.1 0.65 0.1 0.017 2.44 0.1887 0.0086 2.36 0.34 0.101 0.015 1.274 0.184 0.01 1.78 0.29 0.081 0.013 1.812 0.192 0.01 2.98 | 0.2235 0.0087 3.26 0.33 0.107 0.012 1.548 0.043 0.191 0.0066 3.51 0.29 0.139 0.013 1.246 0.027 0.224 0.018 1.49 0.6 0.066 0.029 1.64 0.11 0.263 0.016 2.76 0.66 0.082 0.02 1.424 0.066 0.209 0.019 2.26 0.66 0.153 0.051 2.79 0.24 0.218 0.013 2.82 0.42 0.122 0.021 1.889 0.085 0.263 0.025 2.49 0.71 0.117 0.039 2.2 0.2 0.338 0.024 2.91 0.64 0.076 0.019 1.146 0.052 0.035 0.09 0.2 0.23 0.187 0.063 0.752 0.031 0.187 0.009 0.2 0.23 0.187 0.013 1.812 0.051 0.1887 0.0086 2.36 0.31 0.013 1.812 0.051 0.187 <td>0.2235 0.0087 3.26 0.33 0.107 0.012 1.548 0.048 126600 0.191 0.0066 3.51 0.29 0.139 0.013 1.246 0.027 112100 0.224 0.018 1.49 0.6 0.066 0.029 1.64 0.11 17300 0.263 0.016 2.76 0.66 0.082 0.02 1.424 0.066 150600 0.209 0.019 2.26 0.66 0.153 0.051 2.79 0.24 23100 0.218 0.025 2.49 0.71 0.117 0.039 2.2 0.2 14600 0.038 0.024 2.91 0.64 0.076 0.019 1.146 0.062 21600 0.075 0.009 0.2 0.23 0.187 0.063 0.752 0.031 7190 0.34 0.017 4.1 0.65 0.1 0.017 2.44 0.3 68400 0.1887 0.0086 2.36 0.34 0.101 0.015 1.274 0.51 87400<!--</td--><td>0.2235 0.0087 3.26 0.33 0.107 0.012 1.548 0.048 126600 5400 0.191 0.0066 3.51 0.29 0.139 0.013 1.246 0.027 112100 7600 0.224 0.018 1.49 0.6 0.066 0.029 1.64 0.11 17300 1400 0.263 0.016 2.76 0.66 0.082 0.02 1.424 0.066 150600 9800 0.209 0.019 2.26 0.66 0.153 0.051 2.79 0.24 23100 2300 0.218 0.013 2.82 0.42 0.122 0.021 1.889 0.085 35600 2500 0.263 0.025 2.49 0.71 0.117 0.039 2.2 0.2 14600 1400 0.338 0.024 2.91 0.64 0.076 0.019 1.146 0.62 21600 1500 0.434 0.017 4.1 0.65 0.1 0.177 2.44 0.13 68400 5000</td><td>0.2235 0.0087 3.26 0.33 0.107 0.012 1.548 0.048 12600 5400 430 0.191 0.0066 3.51 0.29 0.139 0.013 1.246 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<</td><td>0.22350.00873.260.330.1070.0121.5480.0481266005400540130.57.90.1910.00663.510.290.1390.0131.2460.0271121007600453130.2240.0181.490.60.0660.0291.640.11173001400672.700.3470000.2630.0162.760.660.0820.021.4240.066150600980097.230.2090.0192.260.660.1530.0512.790.2423100230062.92.900.2180.0132.820.420.120.0211.8890.85356002500144.54.400.2630.0252.490.710.1170.392.20.2146001400532.50.2630.0252.490.710.1170.392.20.214600150060.92.160.2630.0252.490.710.1170.391.240.21460015064.22.50.2630.0252.490.710.1170.391.240.21460015064.22.50.2630.0290.020.20.20.50.3171009407122.50.3380.0242.910.640.0172.440.1368400500095.840.364</td><td>0.2225 0.0087 3.26 0.33 0.107 0.012 1.548 0.048 126600 5400 450 453 43 0.191 0.0066 3.51 0.29 0.139 0.013 1.246 0.07 112100 7600 453 13 3005 0.224 0.018 1.49 0.6 0.066 0.029 1.64 0.11 17300 1400
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Cuts resin		283.91	890	-870	550	0 !	190	270	1600	4.1	3.7	1.3	7.9	1.9	11	1200	6800	11	-5	0.12	0.2	2.8	4.1	0.058	0.301	SA5_0501_2
Cuts	R	467.50	490	-400	260	0 2	480	130	1470	10	41	1.6	21.4	2.5	44.7	970	10050	0.31	2.38	0.04	0.149	1.1	3.8	0.026	0.267	SA5_0508_2
inclusion		323.44	530	-640	270	0 2	250	160	1430	10	57	1.3	17.1	1.2	27	870	7900	0.17	1.67	0.051	0.174	1.2	3.4	0.031	0.26	SA5_0508_3
	R	400.47	480	-430	190	0 3	540	94	1292	8.8	39.4	1.8	28.9	3.2	74.3	1200	14700	0.17	2.5	0.04	0.114	0.74	2.84	0.018	0.228	SA5_0509_1
cutter		394.87	740	-390	400	0 4	-200	170	1150	5.5	13.7	1.1	11.1	1.4	19.7	850	5500	2.3	0.9	0.079	0.249	1.3	2.1	0.032	0.206	SA5_0600_2
zone cutter		106.76	4000 0	2100 0	730	D	-780	320	1420	8.4	31.9	1.1	16.3	1.1	13.8	960	3640	0.16	0.94	0.92	-0.2	1.8	0.6	0.067	0.27	SA5_0601_1
	С	-72.27	330	1280	180	0 :	1740	94	2205	18	140	2.1	39.2	4	85.5	1800	24400	0.11	2.11	0.019	0.135	1	7.7	0.02	0.412	SA5_0603_1
Cuts resin		425.33	560	-150	79	0	-230	84	488	7.9	26.7	3.8	60.9	2.3	36.2	500	2820	0.037	0.586	0.038	0.166	0.47	0.51	0.014	0.078	SA5_0608_1
Cuts resin		111.08	1800 0	- 1200 0	240	0 2	1220	130	1330	16	125	2.3	35.7	2.5	39.9	960	8240	0.081	1.163	0.41	-0.02	1.3	6.3	0.025	0.234	SA5_0700_2
Cuts resin		346.44	470	-450	180	0 3	560	85	1109	7.7	30	1.9	33.9	2.5	60	930	11290	0.13	1.92	0.054	0.147	0.64	2.42	0.016	0.192	SA5_0703_1
Cuts resin Cuts inclusion, radiation		503.85	430	-260	160	D :	620	66	1050	10	55	1.8	42.8	2.5	78.9	870	11270	0.1	1.89	0.052	0.132	0.51	2.07	0.012	0.18	SA5_0704_1
damage		-283.59	330	390	150	0 3	1020	64	1496	14	104	2.2	48.6	4.3	119.5	2300	36900	0.1	2.46	0.015	0.085	0.47	2.95	0.013	0.264	SA5_0704_2
Cuts resin		1740.00	560	50	220	0 2	320	110	920	8.8	50.5	1.4	25	1.3	30.5	610	4480	0.1	1.32	0.064	0.265	0.94	2.97	0.02	0.162	SA5_0706_1
	С	-65.10	280	980	120	0 3	1350	61	1618	13	89	1.9	37.1	4.6	145.2	2500	43300	0.19	3.98	0.013	0.1	0.47	3.91	0.012	0.288	SA5_0706_2
Cuts resin		-20.80	240	2260	120	0 :	2570	130	2730	11	67	0.86	9.5	3.4	74.1	2700	42300	130	-150	0.02	0.199	1.4	13.8	0.031	0.538	SA5_0707_1
	R	-8.67	40	2826	24	8 2	2928	36	3071	15	109	1.2	20.2	27	1024	19000	743000	3.5	54.3	0.0048	0.2025	0.43	17.1	0.0089	0.6103	SA5_0707_2
Cuts resin										2.8	0.6	0.37	0.94	0.17	0.38											SA5_0708_1
Cuts resin										3.1	2.5	0.000 054	0.012 341	0.000 0026	0.011 8672											SA5_0800_1
Cuts resin		450.00	570	-80	53	8 !	-98	45	280	6.1	26.5	6.5	78.8	5.3	64.9	650	4040	0.041	0.807	0.053	0.214	0.14	0.03	0.0075	0.0454	SA5_0800_2
Cuts resin		-39.33	350	1190	160	0 3	1440	88	1658	16	115	2.9	46.2	3.9	83.9	2600	33400	0.1	1.84	0.022	0.142	0.7	5.1	0.017	0.297	SA5_0801_1
Cuts resin		-41.28	290	1480	150	0 3	1770	94	2091	13	109	2.5	68.8 -	2.9	88.5	3400	54500	0.055	1.252	0.017	0.14	0.82	6.93	0.021	0.39	SA5_0802_1
Cuts resin										0.004 2	3.693 6	0.000 02	0.009 57	0.000 0023	0.010 4846											SA5_0804_1
	R	-293.88	370	490	180	0 3	1130	100	1930	9.2	65.7	1.5	24.2	3.3	70.6	2200	29700	0.19	2.98	0.019	0.102	0.74	4.4	0.022	0.356	SA5_0804_2

Appendices

Cuts zones		-61.64	280	1100	130	1450	75	1778	10	79	1.7	37.2	2.6	101.6	3300	56600	0.15	2.79	0.013	0.108	0.52	4.49	0.015	0.319	SA5_0804_3
Cuts resin		67.69	650	1040	58	-613	70	336	5.9	16.5	1.6	36.5	1.2	25.3	580	3020	0.042	0.672	0.067	0.435	0.24	-0.18	0.012	0.056	SA5_0805_1
Cuts resin		64.34	770	1220	150	-950	79	435	3.1	2.7	1.4	19.2	1.3	22.7	590	3270	0.18	1.45	0.11	0.67	0.3	-0.37	0.014	0.073	SA5_0806_1
Cuts inclusion		103.28	3800 0	- 4000 0	320	-120	170	1310	5.7	18.6	0.85	10.63	1.1	15.8	1000	8200	0.19	1.73	0.86	-0.68	1.4	2.5	0.031	0.224	SA5_0808_1
Cuts zones Cuts inclusions and		20.57	150	2640	77	2346	92	2097	22	277	5	107.6	5.6	114.8	4400	62500	0.037	1.065	0.018	0.198	0.84	9.58	0.02	0.388	SA5_0810_1
fractures		-8.86	180	2450	85	2538	98	2667	19	223	2.1	64.5	2.2	83.1	3600	69200	0.051	1.332	0.018	0.189	1.1	12.4	0.023	0.52	SA5_0810_2
Cuts resin		693.10	440	-290	220	770	130	1720	11	59	2.9	40.6	2.3	36.1	1800	20100	0.081	1.009	0.029	0.105	1	3.9	0.027	0.317	SA5_0900_1
inclusion		-469.44	410	360	210	1040	130	2050	12	88	1.8	32.8	1.9	42.5	2500	34600	0.1	1.59	0.025	0.116	0.89	4.72	0.028	0.385	SA5_0900_2
Cuts resin		1933.33	560	-60	220	-100	140	1100	8.1	32	1.8	29.7	0.97	18.34	750	5610	0.071	0.838	0.061	0.255	0.9	1.69	0.028	0.2	SA5_0901_1
2020	R	5.56	230	1350	93	1338	48	1275	24	257	9	168	14	296	7400	112600	0.069	2.146	0.011	0.112	0.33	3.28	0.0093	0.2201	SA5_0905_1
cutter		232.00	640	-1000	290	-340	190	1320	8.5	32.3	1.6	27	1.3	19.9	1500	11100	0.095	0.995	0.074	0.192	0.79	0.94	0.038	0.243	SA5_0910_1
Cuts zones		222.72	460	-810	180	400	83	994	8.1	34.7	2.1	33.9	2.7	51.8	1500	16500	0.14	1.95	0.05	0.136	0.61	1.82	0.015	0.171	SA5_0910_2
Cut zones,	С	10.94	130	1280	45	1208	29	1140	8.8	261.1	5.2	207.3	4.8	162.5	18000	26000	0.013	0.793	0.006	0.0931	0.15	2.4	0.0054	0.1941	SA7_0001_2
damage		30.12	52	1494	20	1202	12	1044	17	731	9	681.9	9.2	834.7	84000	245000	0.012	1.24	0.0025	0.095	0.064	2.274	0.0022	0.176	SA7_0003_1
	R	2.37	55	1391	22	1363	15	1358	13	491	3.7	276.2	7.5	571.1	74000	97000	0.021	2.082	0.0026	0.0899	0.081	2.868	0.0029	0.2346	SA7_0003_2
Inclusion	R	3.68	86	1276	32	1249	18	1229	8.5	221.7	3.4	181.3	4.2	278.8	31000	67000	0.018	1.545	0.0035	0.0865	0.11	2.49	0.0033	0.2102	SA7_0005_1
cutter		38.34	79	1458	26	1081	15	899	14	383	14	603	11	470	36000	73000	0.012	0.778	0.0038	0.0954	0.076	1.944	0.0026	0.1498	SA7_0005_2
Cuts zones		-8.79	140	1070	47	1155	24	1164	6.7	120.7	1.2	70.5	1.9	143.3	14000	29000	0.035	2.027	0.0055	0.0833	0.14	2.23	0.0043	0.1977	SA7_0101_1
	R	-3.01	140	1130	46	1182	24	1164	6.1	101.4	0.99	58.46	1.8	136.4	14000	18000	0.036	2.312	0.0055	0.0866	0.14	2.32	0.0044	0.1983	SA7_0101_2
Cuts zones		-16.83	140	1010	46	1154	23	1180	4.8	75	0.85	41.61	2.4	133.2	13000	16000	0.057	3.181	0.0051	0.0804	0.14	2.24	0.0043	0.2011	SA7_0101_3
Cuts zones		0.51	64	1382	25	1397	18	1375	11	340	2.3	161.7	4.7	419.1	50000	110000	0.028	2.567	0.0029	0.0903	0.093	2.976	0.0034	0.2379	SA7_0104_1
inclusion		1.66	79	1387	29	1401	20	1364	13	412	3.5	215.6	7.6	342.5	41000	47000	0.02	1.554	0.0036	0.0919	0.12	3.03	0.0038	0.2359	SA7_0104_2
Cuts resin		4.58	19	2907	12	2886	25	2774	120	1330	28	289	41	963	280000	590000	0.22	4.15	0.0026	0.211	0.21	16.18	0.006	0.5384	SA7_0105_1
Cuts zones		1.74	30	2867	19	2880	29	2817	13	426	1.5	88	3.3	291.5	87000	125000	0.054	3.31	0.0038	0.207	0.32	16.18	0.007	0.5488	SA7_0106_1

Cuts zones		58.90	43	2304	18	1481	14	947	26	1357	9.3	855.4	7.4	702.3	46000	174000	0.008 5	0.813	0.0037	0.1484	0.075	3.329	0.0024	0.1584	SA7_0202_2
	R	-6.79	70	1238	27	1323	16	1322	12	431	3.4	214.1	5.1	448.8	56000	103000	0.023	2.076	0.003	0.0847	0.097	2.726	0.0031	0.2278	SA7_0203_1
Cuts resin									2.7	13	0.026	0.09	0.015	0.037											SA7_0204_1
Cuts inclusion		49.94	55	1780	27	1193	23	891	20	734	60	1188	28	628	49000	89000	0.009 4	0.533	0.0033	0.1108	0.084	2.266	0.004	0.1481	SA7_0205_1
	R	19.98	55	1702	23	1504	18	1362	16	601	3.8	361.5	8.5	538.8	73000	166000	0.02	1.467	0.003	0.1065	0.1	3.44	0.0035	0.2354	SA7_0208_1
Radiation damage		-9.58	120	1440	45	1533	30	1578	7	169.7	1.2	68.5	1.4	100.9	18000	26000	0.021	1.456	0.0061	0.0992	0.21	3.66	0.0061	0.278	SA7 0301 2
Radiation		28.42		1407	27	1120	22	1007	17	720	11	65.0	7.0	E27.4	55000	120000	0.008	0.788	0.0022	0.0016	0.091	2 070	0.004	0.1605	SA7 0202 1
Radiation		20.45	00	1407	27	1129	22	1007	17	750	11	030	7.9	527.4	33000	129000	9	5	0.0032	0.0910	0.081	2.079	0.004	0.1095	3A7_0305_1
damage		71.28	38	2188	14	1072	8.3	628.3	24	1517	15	1116	18	1665	94000	437000	0.013	1.46	0.003	0.1384	0.041	1.883	0.0014	0.1024	SA7_0304_1
	R	3.80	51	1711	23	1641	18	1646	7.3	162.7	3.6	172.5	7.1	510.5	100000	220000	0.038	2.906	0.0029	0.1071	0.11	4.09	0.0035	0.2911	SA7_0304_2
	С	-0.96	79	1670	33	1645	29	1686	12	407	2.7	149.7	2.5	160.8	35000	91000	0.011	1.05	0.0045	0.1067	0.16	4.15	0.0058	0.2994	SA7_0306_1
	R	1.35	120	1630	47	1594	32	1608	8.7	220.1	1.2	84	1.3	86.6	17000	22000	0.014	1.008	0.0063	0.1077	0.22	3.98	0.0064	0.284	SA7_0401_1
Cuts zones		-7.99	120	1490	46	1550	29	1609	9.5	307.9	1.7	119.6	1.8	122.1	26000	56000	0.012	0.999	0.0055	0.101	0.2	3.78	0.0058	0.2842	SA7_0401_2
Cuts zones		17.54	69	1613	30	1410	19	1330	12	461	3.2	233.9	3.5	262.2	43000	71000	0.011	1.095	0.0039	0.1017	0.12	3.08	0.0036	0.2294	SA7_0401_3
	С	7.81	48	1639	21	1555	17	1511	15	579	3.9	279.8	6.3	554.8	110000	260000	0.018	1.94	0.0028	0.1024	0.097	3.67	0.0034	0.2644	SA7_0402_1
Cuts zones		42.49	51	1744	21	1264	14	1003	24	1032	21	693	12	677	86000	189000	0.018	0.976	0.0031	0.1088	0.072	2.506	0.0026	0.1685	SA7_0403_1
	R	-3.44	75	1570	29	1613	23	1624	12	389	2.6	183.8	3.6	226.7	49000	121000	0.013	1.207	0.0039	0.1009	0.14	3.95	0.0046	0.287	SA7_0404_1
Cuts zones		-2.77	57	1586	24	1625	21	1630	15	686	5.3	295.2	5	400.2	87000	130000	0.016	1.331	0.003	0.0995	0.12	3.99	0.0042	0.2879	SA7_0404_2
Cuts resin		75.14	46	1843	14	789	5.6	458.2	17	957	13	839	21	1687	67000	329000	0.016	1.97	0.0029	0.1147	0.03	1.184	0.00094	0.07368	SA7_0405_1
Cuto	R	-4.25	46	1716	21	1786	21	1789	8.7	270.1	1.3	101.1	4.6	423.9	90000	166000	0.049	4.115	0.0026	0.1069	0.12	4.85	0.0042	0.3203	SA7_0504_1
inclusion		10.14	58	1430	22	1369	16	1285	13	545	7.8	547.6	4	441.8	64000	137000	8	6	0.0027	0.092	0.085	2.883	0.003	0.2207	SA7_0505_1
Cuts inclusion		4.23	52	1324	20	1311	16	1268	12	556	4.6	306.6	7.4	558.4	78000	145000	0.017	1.793	0.0023	0.0869	0.072	2.668	0.0029	0.2176	SA7_0506_1
Cuts inclusion		20.28	54	1524	21	1355	14	1215	20	535	4.4	346.5	7.7	640.8	77000	212000	0.023	1.822	0.0028	0.0964	0.082	2.826	0.0027	0.2075	SA7_0506_2
Cuts resin		-18.18	120	990	39	1144	20	1170	8.3	264.8	4.8	193.1	1.9	160.5	18000	34000	0.022	0.842	0.0042	0.0778	0.11	2.18	0.0036	0.1988	 SA7 0701 1
	R	3.80	64	1709	27	1693	22	1644	9.6	289.4	2.1	192.7	2.8	257.8	43000	92000	0.013	1.33	0.0036	0.1073	0.14	4.37	0.0045	0.2909	 SA7 0804 1
Cuts resin		-684.71	380	170	160	810	71	1334	2.8	27.3	0.36	13.57	0.31	13.6	5600	3300	0.035	1.029	0.017	0.084	0.47	2.46	0.013	0.23	 SA8 0000 1
	С	5.38	73	1505	28	1454	22	1424	15	459	6.6	276.7	5	262.9	110000	110000	0.01	0.953	0.0037	0.0977	0.12	3.26	0.0042	0.2471	 SA8_0001_ 1
Cuts zones		-8.02	170	1160	56	1273	31	1253	6.6	123.7	1.2	82.2	1.2	71.7	28000	-20000	0.016	0.873	0.0072	0.0923	0.21	2.65	0.0059	0.2152	_ SA8_0003_2
														-											_

C	4.94	89	1356	33	1319	21	1289	11	305	3.9	205	5	279.6	120000	500000	0.016	1.365	0.0038	0.0912	0.12	2.75	0.0039	0.2217	SA8_0004_1
damage	-10.44	76	1284	28	1362	24	1418	10	297	1.9	142.9	3.2	262.9	130000	-300000	0.02	1.839	0.0034	0.0862	0.11	2.86	0.0047	0.2465	SA8_0004_2
R	-14.38	120	1440	47	1572	33	1647	6.5	127.7	0.96	51.4	1.7	102.8	70000	24000	0.035	2.002	0.0061	0.0995	0.22	3.83	0.0066	0.2918	SA8_0005_1
R	-3.77	77	1592	31	1626	28	1652	8.2	227.1	1.5	95.7	3.9	243.2	180000	100000	0.034	2.534	0.0041	0.1029	0.15	4.06	0.0055	0.2926	SA8_0009_1
С	-14.46	110	1010	37	1111	21	1156	7.8	179.9	1.4	108.3	2.6	216.1	110000	120000	0.027	1.991	0.0041	0.0781	0.11	2.06	0.0039	0.1966	SA8_0013_1
Cuts zones	26.31	59	1410	21	1163	15	1039	22	827	14	650	13	648	300000	610000	0.009 3	0.993	0.0027	0.091	0.063	2.164	0.0027	0.175	SA8_0015_1
Cuts resin	-0.55	120	1640	48	1660	32	1649	15	327	2.6	123.5	1.4	118.1	100000	150000	0.018	0.958	0.0064	0.11	0.25	4.3	0.0064	0.2922	SA8_0100_1
Cuts resin	-10.36	160	1400	60	1512	35	1545	11	290	1.8	128.4	1.6	85.9	84000	64000	0.009 5	0.661 4	0.0073	0.102	0.26	3.73	0.007	0.2716	SA8_0100_2
С	-7.69	83	1352	32	1422	20	1456	19	513	6.3	235.7	6.2	349.2	360000	350000	0.02	1.476	0.0035	0.0896	0.13	3.13	0.004	0.2533	SA8_0101_1
Cuts inclusion	-52.80	230	1000	94	1334	51	1528	6.8	105.5	0.92	47.35	1.5	45.2	51000	20000	0.03	0.948	0.0093	0.0921	0.31	3.17	0.0099	0.268	SA8_0103_1
Cuts zones	17.51	58	1690	23	1516	20	1394	17	582	4.6	338.2	6.4	569.6	610000	310000	0.022	1.672	0.0033	0.1064	0.1	3.5	0.0038	0.2416	SA8_0104_1
R	-14.47	100	1500	43	1623	31	1717	12	256	1.8	98.6	2.8	177.7	250000	600000	0.028	1.785	0.005	0.0993	0.21	4.11	0.0063	0.3059	SA8_0104_2
Cuts resin	7.83	71	1469	28	1405	24	1354	28	557	14	274	26	495	680000	560000	0.021	1.78	0.0036	0.0957	0.12	3.06	0.0046	0.2341	SA8_0105_1
С	9.29	59	1431	24	1352	19	1298	18	564	4.8	346.2	15	803	110000 0	110000 0	0.056	2.314	0.0027	0.0924	0.087	2.82	0.0036	0.2234	SA8_0105_2
С	-22.30	98	906	31	1056	19	1108	17	533	4.1	320.8	4.4	349	420000	480000	0.012	1.081	0.0033	0.0723	0.09	1.88	0.0035	0.1877	SA8_0109_2
С	-6.39	82	1331	31	1397	21	1416	13	377	2.5	173.5	4.4	349	590000	780000	0.023	2.004	0.0034	0.0886	0.12	3.01	0.004	0.2458	SA8_0112_1
R	-11.78	180	1010	63	1123	25	1129	8.7	151.9	1.4	87.8	1.8	131.3	170000	270000	0.026	1.488	0.0067	0.0856	0.18	2.26	0.0046	0.1917	SA8_0113_1
С	1.47	51	1697	24	1689	23	1672	20	860	6.3	450.1	7.2	569	110000 0	130000 0	0.013	1.262	0.0029	0.1059	0.13	4.33	0.0046	0.2965	SA8_0115_1
Cuts resin	-21.77	120	1240	46	1430	29	1510	13	374	2.3	161.7	2.4	162.7	290000	600000	0.013	1.004	0.0052	0.0891	0.18	3.2	0.0057	0.2646	SA8_0200_1
С	-42.84	180	1020	62	1342	36	1457	12	332	2.5	152.4	1.1	79.3	130000	800000	0.008 7	0.522 5	0.0071	0.0864	0.24	2.96	0.0071	0.2544	SA8_0200_2
R	-54.71	210	700	70	989	29	1083	7.7	133.3	1.4	76.8	1.9	117.7	130000	0	0.026	1.534	0.0074	0.0764	0.18	1.89	0.0052	0.1835	SA8_0201_1
R	7.02	65	2776	41	2688	61	2581	12	333	1.9	91.1	1	58	170000	-200000	0.013	0.642	0.0079	0.199	0.59	13.51	0.014	0.494	SA8_0203_2
С	10.20	81	2520	45	2409	49	2263	18	394	2.5	125.1	1.7	106.9	230000	220000	0.015	0.857	0.0084	0.1756	0.48	10.09	0.011	0.422	SA8_0204_1
Fracture, radiation																								
damage	-5.97	84	1575	34	1645	28	1669	18	648	4.2	263.7	3.1	224.8	320000	240000	0.01	0.852	0.0042	0.1021	0.17	4.17	0.0056	0.296	SA8_0205_1
Cuts resin	-2.20	54	1591	26	1618	23	1626	15	473	6.6	252.3	9.9	605.1	770000	-390000	0.038	2.422	0.0028	0.1003	0.13	3.99	0.0045	0.2867	SA8_0209_2
С	36.34	58	1599	23	1231	14	1018	20	651	19	699	19	933	650000	920000	0.019	1.348	0.003	0.1012	0.074	2.388	0.0026	0.1711	SA8_0212_1

SA8_0215_2	0.2052	0.0053	2.4	0.16	0.0855	0.0058	1.079	0.016	150000	130000	153.5	1.9	142.6	1.9	205.4	9.9	1200	29	1198	50	1110	140	-8.11	R	Radiation damage
SA8_0301_1	0.2322	0.005	2.81	0.15	0.0877	0.0048	1.511	0.021	110000	160000	189.3	3.2	125	2.2	256	11	1347	27	1325	42	1230	120	-9.51		inclusion
SA8_0302_1	0.2196	0.0028	3.44	0.082	0.1132	0.0025	1.228	0.01	140000 0	710000	1075	11	870.6	8.6	1582	33	1279	15	1508	19	1831	39	30.15		Cuts resin
SA8_0302_2	0.2919	0.0046	4.09	0.12	0.101	0.0028	1.072	0.011	530000	490000	541.5	6.9	502.9	7.5	1082	26	1649	23	1643	24	1617	55	-1.98	R	
SA8_0303_1	0.3037	0.0049	4.68	0.15	0.1118	0.0036	1.387	0.015	270000	380000	420.2	7.3	301.6	5.8	698	18	1708	24	1747	28	1772	65	3.61	R	
SA8_0303_2	0.3164	0.0052	4.62	0.14	0.1055	0.0033	2.501	0.027	110000	390000	443.4	5.3	176.1	2.4	455	14	1770	26	1739	26	1692	60	-4.61	R	C .
SA8_0304_1	0.1918	0.0052	2.04	0.16	0.0767	0.0064	1.011	0.016	23000	54000	108.1	1.8	106	2.1	164.7	7.6	1128	28	1053	61	800	180	-41.00		inclusion
SA8_0304_2	0.1548	0.0026	1.753	0.063	0.0816	0.0031	3	1	350000	270000	744	11	1160	21	1532	30	927	14	1019	24	1174	80	21.04	R	
SA8_0305_1	0.2447	0.0039	3.22	0.13	0.0948	0.0038	1.229	0.014	260000	200000	351.3	4.6	280.7	3.5	544	16	1410	20	1441	32	1433	81	1.61	R	Fracture
SA8_0309_1	0.1251	0.0023	2.004	0.058	0.1154	0.0032	1.699	0.021	104000 0	320000	1255	27	725	12	996	24	761	13	1108	20	1859	50	59.06		radiation damage
SA8_0311_1	0.2536	0.004	3.5	0.14	0.0994	0.0038	0.82	0.012	190000	140000	244.1	6.3	298	11	551	24	1456	21	1505	32	1550	73	6.06		Cuts resin Fracture,
SA8_0311_2	0.2548	0.0053	3.49	0.12	0.0992	0.0033	0.891	0.019	330000	240000	451	14	520	28	1003	37	1461	27	1512	26	1564	64	6.59		radiation damage
SA8_0312_1	0.565	0.021	16.6	1.1	0.216	0.014	2.82	0.12	23000	21000	18.05	0.44	6.67	0.28	29.2	3.1	2863	86	2846	67	2800	130	-2.25	R	
SA8_0315_1	0.2609	0.0077	3.78	0.29	0.1076	0.0087	1.116	0.021	24000	30000	57.9	1.1	51.6	1.1	73.8	5.1	1489	39	1529	64	1480	170	-0.61	С	
SA8_0402_1	0.2899	0.007	4.04	0.23	0.1024	0.006	1.852	0.03	85000	58000	96.5	1.5	52.03	0.96	125.7	5.7	1637	35	1598	49	1500	120	-9.13	R	
SA8_0402_2	0.2977	0.0078	4.12	0.26	0.1012	0.0062	2.166	0.039	43000	43000	75.1	1.3	34.84	0.69	83.4	4.6	1675	38	1610	52	1450	130	-15.52	R	
SA8_0404_1	0.205	0.0052	2.42	0.15	0.0866	0.0055	1.294	0.021	27000	41000	112.5	2.1	89.1	2.1	156.6	7.1	1199	28	1208	48	1130	140	-6.11		Cuts resin
SA8_0405_1	0.2546	0.0041	3.68	0.12	0.1041	0.0033	8	2	230000	160000	329.6	5.1	401	7.1	730	17	1463	21	1559	25	1664	57	12.08	R	Cuts
							0.605	0.007																	radiation,
SA8_0405_2	0.2509	0.0041	3.66	0.1	0.1051	0.0028	1	2	140000	180000	390.9	9.7	679	22	1297	35	1442	21	1556	23	1702	49	15.28		damage
SA8_0409_1	0.2235	0.0038	2.784	0.083	0.0901	0.0027	1.598	0.016	140000	150000	373.5	6.3	245.8	4.1	439	12	1299	20	1340	23	1380	61	5.87	_	Cuts zones
SA8_0409_2	0.2284	0.0035	2.844	0.088	0.0902	0.0029	1.532	0.015	170000	150000	385.3	4.1	266.1	2.8	449	11	1325	18	1360	24	1379	64	3.92	R	Radiation
SA8_0409_3	0.0892	0.0013	1.4	0.037	0.1131	0.0029	0.638	0.011	890000	180000	1603	17	2678	51	1246	21	550.4	7.9	884	15	1816	47	69.69		Cuts
SA8_0411_1	0.2731	0.0054	3.86	0.16	0.1029	0.0045	1.052	0.01	98000	73000	176.6	2.4	175.8	2.4	401	12	1554	27	1586	35	1582	87	1.77		inclusion
SA8_0412_1	0.2283	0.0044	2.71	0.13	0.0865	0.0042	1.475	0.017	75000	58000	179.9	3.6	127	3.1	242.2	9.1	1324	23	1307	38	1220	100	-8.52	R	

Cuts zones		-18.17	110	1150	41	1303	25	1359	7.5	163.5	2.5	84.2	3.6	134.3	42000	62000	0.022	1.645	0.0045	0.084	0.14	2.71	0.0048	0.235	SA8_0412_2
Cuts	C	-10.92	110	1200	40	1310	23	1331	8.1	193.7	1.6	106.6	2.6	196.4	55000	11000	0.023 0.007	1.867 0.785	0.0046	0.0865	0.14	2.73	0.0044	0.2296	SA8_0414_1
inclusion		-8.05	98	1031	33	1104	17	1114	14	547	3.6	336.5	2.9	267.1	56000	80000	5	2	0.0037	0.0766	0.094	1.999	0.0031	0.1888	SA8_0415_1
R	R	-5.33	91	1089	31	1142	18	1147	10	248	2.5	153.6	3.3	318	66000	72000	0.031	2.057	0.0034	0.0789	0.094	2.134	0.0034	0.1946	SA8_0415_2
Cuts zones		5.04	140	1270	49	1263	30	1206	15	454	9.6	284.9	3.2	126.3	27000	32000	0.006 7	0.442	0.0065	0.0942	0.17	2.63	0.0055	0.2062	SA8_0501_1
Cuts resin		33.68	44	1805	19	1442	16	1197	9.9	257.8	3.3	191.5	12	826	160000	440000	0.052	4.264	0.0026	0.1115	0.077	3.17	0.003	0.2042	SA8_0502_1
C	С	15.44	36	2668	21	2489	30	2256	43	1568	9.4	506	4.2	306.4	130000	140000	2	0.601	0.0039	0.183	0.24	10.69	0.0066	0.4196	SA8_0502_2
C	С	50.78	60	1662	22	1094	14	818	29	1513	7.9	668.2	8.8	696.4	86000	147000	0.015	1.037	0.0034	0.1038	0.065	1.97	0.0024	0.1354	SA8_0505_1
C	С	-0.38	47	1831	23	1844	25	1838	27	1314	5.1	469.3	5.3	469.9	140000	200000	0.009 1	0.997	0.003	0.1137	0.13	5.2	0.0051	0.3303	SA8_0509_2
Cuts resin		19.09	95	1519	33	1357	22	1229	18	339	5.6	156.5	7.3	315.1	58000	113000	0.044	2.06	0.0046	0.1003	0.12	2.89	0.0042	0.2104	SA8_0511_1
inclusion		-28.07	150	880	48	1084	24	1127	15	485	4.4	286.5	2.1	168.5	29000	40000	0.009 7	0.589	0.0054	0.0766	0.14	2.03	0.0044	0.1913	SA8_0513_1
R	R	-8.67	150	1050	51	1147	26	1141	7.2	135.8	1.5	94.2	1.9	144.7	25000	41000	0.024	1.539	0.0056	0.0834	0.15	2.26	0.0049	0.1941	SA8_0515_2
R	R	-6.67	130	1080	44	1163	24	1152	7.4	118.8	1.3	66.9	2.4	158.9	24000	-10000	0.041	2.387	0.0052	0.0836	0.14	2.27	0.0044	0.1959	SA8_0515_3
0	С	-8.24	120	1190	42	1283	26	1288	10	264	1.6	129.3	2	169.8	31000	50000	0.018	1.313	0.0049	0.0865	0.15	2.67	0.0049	0.2216	SA8_0600_1
Cuts resin		-26.12	120	1030	43	1229	25	1299	8.9	210.1	1.9	108.7	2.5	161.8	31000	50000	0.021	1.49	0.0044	0.0785	0.14	2.43	0.0047	0.2237	SA8_0600_2
Cuts zones		3.42	90	1227	31	1214	20	1185	11	210	2.2	169.6	4.2	333	55000	74000	0.026	1.958	0.0038	0.0841	0.1	2.35	0.0037	0.202	SA8_0602_1
R	R	-13.82	120	1100	41	1229	22	1252	9.6	232.4	1.7	132.4	2.9	215.4	38000	69000	0.023	1.619	0.0048	0.0821	0.14	2.45	0.0041	0.2148	SA8_0602_2
Cuts resin		-8.34	72	1547	30	1631	26	1676	20	717	3.3	286.5	3.6	277.7	69000	111000	0.011	0.958	0.0038	0.0987	0.15	4.06	0.0053	0.2975	SA8_0603_1
Miss		-22.10	210	810	68	977	27	989	7.2	123.8	2.2	92.5	2.4	104	14000	17000	0.022	1.117	0.0076	0.0802	0.17	1.87	0.0048	0.1663	SA8_0609_1
		22.83	72	1139	22	969	11	879	26	1322	14	1242	9.4	906.8	110000	320000	5	8	0.0028	0.08	0.056	1.625	0.0019	0.1462	SA8_0609_2
Cuts resin		0.38	290	800	91	858	32	797	6.3	101.3	4.5	103.3	2.2	62.9	6900	8300	0.014	0.619	0.012	0.094	0.22	1.71	0.0057	0.1322	SA8_0611_1
ג	R	-14.85	130	970	44	1100	23	1114	11	295	2.5	186.7	2.5	184.1	30000	47000	0.012	0.976	0.0048	0.079	0.12	2.06	0.0043	0.189	SA8_0613_2
R	R	28.37	96	1519	39	1263	20	1088	18	730	11	414	5.6	277.1	45000	112000	9	0.672	0.0049	0.0998	0.13	2.58	0.0036	0.1841	SA8_0614_1
Cuts zones		-0.97	100	1030	33	1056	17	1040	19	793	8.5	517	4.6	294.1	47000	107000	0.005 3	0.569	0.0036	0.0775	0.092	1.897	0.0031	0.1752	SA8_0614_2
C	С	-13.98	89	987	29	1102	18	1125	12	280	4	166.1	3.9	265.1	46000	55000	0.026	1.622	0.0033	0.0759	0.086	2.013	0.0033	0.1909	SA8_0615_2
0	С	-7.57	90	1520	37	1609	27	1635	13	469	2.7	179.2	2.4	172.7	48000	48000	0.011	0.973	0.0045	0.0994	0.18	3.98	0.0054	0.2892	SA8_0700_2
C	С	1.49	92	1680	39	1691	29	1655	8.4	200	1.3	72.1	2	130.7	38000	67000	0.028	1.844	0.0054	0.1089	0.22	4.42	0.0059	0.2932	SA8_0702_1

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SASD 01 OL32 OL32 OL42	SA8_0703_1	0.2238	0.0064	2.68	0.2	0.0872	0.0065	1.231	0.02	13000	16000	72	1.2	59.8	1.1	124.5	6.6	1302	34	1285	57	1150	150	-13.22	С	Cuts
6.48.0704 0.708 0.604 0.709 0.005 0.700 1.600	SA8_0703_2	0.2292	0.0046	2.7	0.15	0.0842	0.0047	1.941	0.029	24000	40000	168.8	2.9	89	2	186.8	8.3	1329	24	1295	42	1150	120	-15.57		inclusion
SA20701 O170 O170 O170 O170	SA8_0704_1	0.2185	0.0045	2.64	0.13	0.088	0.0046	1.909	0.026	46000	34000	152.8	2.3	81.7	1.7	146.2	6.7	1272	24	1284	39	1230	110	-3.41	R	
SAQ.071.1 0.07	SA8_0709_1	0.2172	0.0036	2.825	0.076	0.0937	0.0025	1.879	0.042	300000	140000	652.2	9.9	361	11	358	13	1266	19	1356	20	1462	52	13.41	С	
SAR_0712 0.11 0.007 0.20 0.007 0.007 0.000 0.007 0.000 <t< td=""><td>SA8_0711_1</td><td>0.179</td><td>0.0027</td><td>1.905</td><td>0.079</td><td>0.0766</td><td>0.0031</td><td>3.717</td><td>0.042</td><td>113000</td><td>83000</td><td>458.8</td><td>8</td><td>124.8</td><td>2</td><td>166.4</td><td>7.3</td><td>1061</td><td>15</td><td>1066</td><td>28</td><td>1011</td><td>88</td><td>-4.95</td><td>С</td><td>C. t.</td></t<>	SA8_0711_1	0.179	0.0027	1.905	0.079	0.0766	0.0031	3.717	0.042	113000	83000	458.8	8	124.8	2	166.4	7.3	1061	15	1066	28	1011	88	-4.95	С	C. t.
SAG,0712 0.23 0.044 3.71 0.14 0.003 0.045 0.004 1000 0.005 0.000 0.005 0.000	SA8_0711_2	0.181	0.0037	1.82	0.11	0.0724	0.0045	6.67	0.13	77000	38000	210	2.6	32.04	0.71	55.4	4.5	1071	20	1021	42	820	130	-30.61		inclusion
SA2.0712 0.279 0.044 4.07 0.3 0.034 0.03 0.034 0.034 0.14 <th0.134< th=""> 0.144 0.</th0.134<>	SA8_0712_2	0.253	0.0044	3.71	0.14	0.1055	0.0038	5	4	191000	76000	295.3	3.8	733	11	1634	30	1452	22	1555	30	1662	72	12.64		Cuts zones
SA2.0711 0.183 0.083 1.95 0.08 0.076 0.035 $\overline{11}$ 7 8200 500 24 45 500 52 53 6 108 18 108 31 97 90 96 90 96 90 96 90 96 90 96 90 96 90 96 90 96 90 96 90 96 90 96 90 96 90 96 90 96 90 96 90 90 <td>SA8_0712_3</td> <td>0.2797</td> <td>0.0044</td> <td>4.07</td> <td>0.13</td> <td>0.1046</td> <td>0.0031</td> <td>0.493 4 0.893</td> <td>6 0.008</td> <td>130000</td> <td>100000</td> <td>381.9</td> <td>4.8</td> <td>768</td> <td>11</td> <td>1892</td> <td>33</td> <td>1588</td> <td>22</td> <td>1638</td> <td>25</td> <td>1660</td> <td>57</td> <td>4.34</td> <td></td> <td>Cuts zones</td>	SA8_0712_3	0.2797	0.0044	4.07	0.13	0.1046	0.0031	0.493 4 0.893	6 0.008	130000	100000	381.9	4.8	768	11	1892	33	1588	22	1638	25	1660	57	4.34		Cuts zones
SA8_07132 0.1872 0.076 2.09 0.25 0.084 0.11 0.695 0.10 1.00 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.000 0.000 0.10 0.000 0.10 0.	SA8_0713_1	0.1838	0.0033	1.952	0.088	0.0766	0.0035	3	7	82000	58000	324.6	4.5	360.1	5.2	593	16	1087	18	1082	31	997	96	-9.03	R	cuts
SA8_07141 0.2288 0.004 2.78 0.11 0.099 0.023 1.90 0.000 2.10 0.038 2.10 0.038 2.27 0.11 0.079 0.001 1.33 0.017 0.023 0.003 0.038 2.27 0.01 0.017 0.004 1.33 0.017 0.000 0.016 0.013 0.017 0.001 0.010	SA8_0713_2	0.1872	0.0076	2.09	0.25	0.084	0.011	0.658	0.011	12900	6600	35.22	0.57	53.06	0.85	94.8	5.8	1101	41	977	98	710	270	-55.07		inclusion Radiation
SA2_08001 0.204 0.003 2.27 0.10 0.004 1.34 0.017 9.000 4900 2.27 2.9 1.66 2.4 3.58 1.01 0.10 1.00 1.01 0.12 0.12 0.13 0.03 0.03 0.033 0.033 0.033 0.033 0.033 0.033 0.033 0.037 0.033 0.277 0.03 0.277 0.03 0.277 0.03 0.077 0.033 0.277 0.03 0.077 0.033 0.277 0.03 0.077 0.033 0.077 0.033 0.277 0.04 0.00 0.00 0.13 0.1 0.1 0.10 0.11 </td <td>SA8_0714_1</td> <td>0.2288</td> <td>0.004</td> <td>2.78</td> <td>0.11</td> <td>0.0869</td> <td>0.0035</td> <td>1.995</td> <td>0.023</td> <td>87000</td> <td>71000</td> <td>331.3</td> <td>5</td> <td>164</td> <td>3.2</td> <td>321</td> <td>13</td> <td>1327</td> <td>21</td> <td>1335</td> <td>31</td> <td>1293</td> <td>83</td> <td>-2.63</td> <td></td> <td>damage</td>	SA8_0714_1	0.2288	0.004	2.78	0.11	0.0869	0.0035	1.995	0.023	87000	71000	331.3	5	164	3.2	321	13	1327	21	1335	31	1293	83	-2.63		damage
SA8_0802 0.215 0.004 2.45 0.14 0.002 0.004 1.50 0.20 0.170 1.170 1.18 2.31 0.125 2.3 1.35 2.3 1.35 2.3	SA8_0800_1	0.2084	0.0038	2.27	0.11	0.0791	0.004	1.334	0.017	93000	49000	252.7	2.9	186.9	2.4	358	15	1219	20	1181	36	1040	110	-17.21		Cuts zones
SA8_0801_1 0.038 2.18 0.088 0.0787 0.038 2.277 0.024 3000 6100 358.9 4.7 155.9 2.2 2.92 12 1147 21 1135 33 1000 100 9.924 R Mark SA8_0801_2 0.1928 0.044 2.52 0.17 0.09 0.006 2.379 0.02 5600 2500 151.3 2 63.3 1.1 158.7 8.9 135.8 2.4 136.3 1.1 136.3 1.1 158.7 1.1 1.58.7 1.1 1.58.7 1.1 1.58.7 1.1 1.58.7 1.6 1.21 0.30 0.007 0.0	SA8_0800_2	0.2153	0.0043	2.45	0.13	0.0823	0.0046	1.632	0.02	65000	37000	193.5	2.7	117.2	1.8	233.2	9.7	1255	23	1226	41	1090	120	-15.14		Cuts zones
SA8_0801_2 0.1928 0.0044 2.52 0.17 0.096 0.2379 0.42 56000 25000 1513 2 633 1.1 158.7 8.9 1135 24 1236 51 1300 140 12.69 inclusion SA8_0801_2 0.2393 0.077 4.27 0.29 0.015 0.074 0.764 0.013 2000 1700 67.3 1.6 88 2.6 2.35 12 1656 38 1631 61 1490 150 11.8 2 63.3 1.1 158.7 8.9 135 24 153 161 130 140 12.69 11.8 2 163 11 130 140 150 130 140 150 140 150 <	SA8_0801_1	0.195	0.0038	2.118	0.098	0.0787	0.0038	2.277	0.024	30000	61000	358.9	4.7	155.9	2.2	292	12	1147	21	1135	33	1050	100	-9.24	R	Cuts
SA8_0803_1 0.293 0.007 4.27 0.29 0.015 0.007 0.013 0.200 0.700 1.200 1.700 0.700 1.700 0.700 0.700 1.217 0.005 1.000 0.000 0.700	SA8_0801_2	0.1928	0.0044	2.52	0.17	0.096	0.0066	2.379	0.042	56000	25000	151.3	2	63.3	1.1	158.7	8.9	1135	24	1236	51	1300	140	12.69		inclusion
SA8_0803_2 0.020 0.012 3.58 0.38 0.0907 0.008 1.217 0.03 1.010 0.07 0.07 0.002 0.000 0.000 0.008 1.017 0.000 1000 9	SA8_0803_1	0.2939	0.0077	4.27	0.29	0.105	0.0074	0.764	0.013	22000	17000	67.3	1.6	88	2.6	235	12	1656	38	1631	61	1480	150	-11.89		Cuts zones Cuts
5A8_0804_1 0.17 0.002 2.629 0.069 0.1109 0.0028 1 7 45000 13000 952 16 1619 30 1070 25 1011 12 1301 19 1791 48 43.55 Cuts respectively SA8_0804_2 0.2942 0.0043 4.14 0.15 0.1015 0.0037 1.627 0.019 178000 78000 303.4 4.6 185.4 3.1 460 15 1661 22 1647 29 1592 67 4.33 R Radiat SA8_0805_1 0.1895 0.0059 2.15 0.19 0.0818 0.0073 1.715 0.36 15000 13000 80.8 1.3 47.4 0.95 81.1 5.3 1115 32 1085 69 910 90 22.53 14014 48 SA8_0805_1 0.196 0.0061 2.17 0.22 0.086 2.69 1000 160 1700 500 151.6 1.6 161 1.5 1.6 1.6 1.6 1.6 1.6	SA8_0803_2	0.296	0.012	3.58	0.38	0.0907	0.0098	1.217	0.03	11000	9200	37.93	0.87	31.21	0.73	85.8	5.9	1662	57	1380	100	930	230	-78.71		inclusion, cuts zones
SA8_0804_2 0.043 4.14 0.15 0.015 0.0037 1.627 0.019 17800 7800 303.4 4.6 185.4 3.1 480 15 1661 22 1647 29 1592 67 4.33 A <td>SA8_0804_1</td> <td>0.17</td> <td>0.0022</td> <td>2.629</td> <td>0.069</td> <td>0.1109</td> <td>0.0028</td> <td>0.587 1</td> <td>0.005 7</td> <td>450000</td> <td>130000</td> <td>952</td> <td>16</td> <td>1619</td> <td>30</td> <td>1070</td> <td>25</td> <td>1011</td> <td>12</td> <td>1301</td> <td>19</td> <td>1791</td> <td>48</td> <td>43.55</td> <td></td> <td>Cuts resin</td>	SA8_0804_1	0.17	0.0022	2.629	0.069	0.1109	0.0028	0.587 1	0.005 7	450000	130000	952	16	1619	30	1070	25	1011	12	1301	19	1791	48	43.55		Cuts resin
SA8_0805_1 0.189 0.0059 2.15 0.19 0.0818 0.0073 1.715 0.036 1500 13000 80.8 1.3 47.14 0.95 81.1 5.3 1115 32 1085 69 910 190 -22.53 damage SA8_0805_2 0.1964 0.0061 2.17 0.22 0.0806 0.086 2.697 0.068 2100 11000 67 1 25.02 0.55 48.6 4.4 1152 33 1060 79 760 200 -51.58 R SA8_0809_1 0.025 0.0062 6.09 0.25 0.1349 0.0059 1.231 0.016 17700 58000 215.4 2.4 142 2.4 142 34 1382 83 -5.50 C - SA8_0900_1 0.0254 0.0047 3.210 0.141 0.033 1.017 0.034 98 0.018 7500 25000 261 4.4 154.8 33 330 12 145.8 24 145.8 24 145.8 210.9 145 <td>SA8_0804_2</td> <td>0.2942</td> <td>0.0043</td> <td>4.14</td> <td>0.15</td> <td>0.1015</td> <td>0.0037</td> <td>1.627</td> <td>0.019</td> <td>178000</td> <td>78000</td> <td>303.4</td> <td>4.6</td> <td>185.4</td> <td>3.1</td> <td>480</td> <td>15</td> <td>1661</td> <td>22</td> <td>1647</td> <td>29</td> <td>1592</td> <td>67</td> <td>-4.33</td> <td>R</td> <td></td>	SA8_0804_2	0.2942	0.0043	4.14	0.15	0.1015	0.0037	1.627	0.019	178000	78000	303.4	4.6	185.4	3.1	480	15	1661	22	1647	29	1592	67	-4.33	R	
SA8_0805_2 0.1964 0.0061 2.17 0.22 0.0806 0.086 2.697 0.068 2100 11000 67 1 25.02 0.55 48.6 4.4 1152 33 1060 79 760 220 -51.58 R SA8_080_1 0.325 0.0062 6.09 0.25 0.1349 0.0055 1.231 0.016 17700 58000 2154 2.8 174.2 2.2 659 26 1815 31 1971 38 2099 75 13.53 C SA8_0900_1 0.2542 0.0047 3.21 0.14 0.033 1.587 0.018 7500 52000 246.1 4.4 154.8 33 12 1458 24 1442 34 1382 83 -5.50 C	SA8_0805_1	0.1895	0.0059	2.15	0.19	0.0818	0.0073	1.715	0.036	15000	13000	80.8	1.3	47.14	0.95	81.1	5.3	1115	32	1085	69	910	190	-22.53		Radiation damage
SA8_0809_1 0.325 0.0062 6.09 0.25 0.1349 0.0055 1.231 0.016 177000 58000 215.4 2.8 174.2 2.2 659 26 1815 31 1971 38 2099 75<	SA8_0805_2	0.1964	0.0061	2.17	0.22	0.0806	0.0086	2.697	0.068	21000	11000	67	1	25.02	0.55	48.6	4.4	1152	33	1060	79	760	220	-51.58	R	
SA8_0900_1 0.2542 0.0047 3.21 0.14 0.0913 0.0039 1.587 0.018 7500 52000 246.1 4.4 154.8 3 330 12 1458 24 1442 34 1382 83 -5.50 C SA8_0900_2 0.2199 0.0038 3.092 0.094 0.1017 0.0034 9 8 16600 82000 435.2 7.7 401.6 7.1 745 19 1280 20 1419 23 1596 63 19.80 Cuts ze Fractur SA8_0901_1 0.0803 0.0016 1.366 0.035 0.1227 0.0029 9 3 53000 11000 2153 42 7570 190 3276 51 497.8 9.5 871 15 1967 44 74.69 cuts ze cuts ze	SA8_0809_1	0.325	0.0062	6.09	0.25	0.1349	0.0055	1.231	0.016	177000	58000	215.4	2.8	174.2	2.2	659	26	1815	31	1971	38	2099	75	13.53	С	
SA8_0900_2 0.2199 0.0038 3.092 0.094 0.1017 0.0034 9 8 166000 82000 435.2 7.7 401.6 7.1 745 19 1280 20 1419 23 1596 63 19.80 Cuts ze SA8_0901_1 0.0803 0.0016 1.366 0.035 0.1227 0.0029 9 3 530000 110000 2153 42 7570 190 3276 51 497.8 9.5 871 15 1967 44 74.69 cuts re	SA8_0900_1	0.2542	0.0047	3.21	0.14	0.0913	0.0039	1.587	0.018	75000	52000	246.1	4.4	154.8	3	330	12	1458	24	1442	34	1382	83	-5.50	С	
SA8_0901_1 0.0803 0.0016 1.366 0.035 0.1227 0.0029 9 3 530000 110000 2153 42 7570 190 3276 51 497.8 9.5 871 15 1967 44 74.69 cuts re	SA8_0900_2	0.2199	0.0038	3.092	0.094	0.1017	0.0034	1.082 9 0.284	8 0.003	166000	82000	435.2	7.7	401.6	7.1	745	19	1280	20	1419	23	1596	63	19.80		Cuts zones
	SA8_0901_1	0.0803	0.0016	1.366	0.035	0.1227	0.0029	0.284 9	3	530000	110000	2153	42	7570	190	3276	51	497.8	9.5	871	15	1967	44	74.69		cuts resin

								0.003																	
SA8_0901_2	0.097	0.0015	1.42	0.048	0.1051	0.0037	0.245	1	178000	65000	858	10	3510	43	795	19	596.7	9	888	20	1658	67	64.01		Cuts zones
SA8_0902_1	0.1792	0.0039	1.97	0.12	0.0797	0.0054	1.312	0.02	27000	23000	169.3	3.1	129	2.2	186.5	8.4	1061	21	1078	44	1010	140	-5.05		Cuts resin
SA8_0902_2	0.1858	0.0053	1.97	0.15	0.078	0.0063	1.639	0.028	31000	16000	111.8	1.8	68.3	1.2	114.9	6.1	1096	29	1051	56	860	170	-27.44	R	
SA8_0903_1	0.1101	0.0019	1.701	0.058	0.1105	0.0036	0.756	0.016	200000	64000	812	15	1084	29	494	14	673	11	998	22	1764	63	61.85		Cuts resin
SA8_0903_2	0.2309	0.0082	2.7	0.27	0.0863	0.0088	1.218	0.027	7300	8400	49.1	0.88	40.02	0.76	79.2	6.1	1333	42	1197	91	900	220	-48.11	С	
SA8_0904_1	0.2798	0.0053	3.95	0.2	0.1023	0.0053	0.97	0.011	31000	34000	174.7	2.3	177.3	2.7	373	12	1591	27	1598	41	1550	100	-2.65	R	
SA8_0904_2	0.2813	0.0073	3.98	0.17	0.1029	0.0044	0.815	0.016	114000	53000	264.2	8.1	330	16	736	26	1593	37	1611	37	1600	80	0.44		Cuts inclusion
SA8_0909_1	0.2645	0.0046	3.8	0.16	0.1036	0.0044	2.014	0.029	94000	47000	246.8	3	121.1	2	160.4	8.2	1511	24	1575	34	1628	76	7.19	R	
SA8_0911_2	0.1521	0.0028	1.936	0.094	0.0912	0.0042	0.732 1	0.008 8	93000	41000	382.9	5.5	514.8	7.1	625	15	912	15	1075	31	1351	89	32.49		Cuts inclusion
SA8_0911_4	0.1931	0.0045	2.1	0.14	0.0781	0.0054	1.143	0.014	49000	21000	147.4	2.1	127.3	2.1	196.6	8.2	1136	24	1096	50	910	150	-24.84	R	
SA8_0915_2	0.2348	0.0047	2.83	0.14	0.0872	0.0044	1.019	0.012	72000	36000	214.2	5.9	208.8	6.3	419	17	1358	25	1341	38	1270	100	-6.93	с	
SA8_0915_3	0.2281	0.0045	2.86	0.16	0.0915	0.0052	1.023	0.014	70000	28000	166.6	3	161.9	2.7	289	11	1323	24	1344	42	1290	120	-2.56		Cuts resin
SA10_0000_ 1	0.2975	0.0015	4.261	0.045	0.1073	0.0012	1.806 4	0.007 8			453.2	4.6	253.5	2.4	459.4	4.7	1678. 7	7.5	1683	8.8	1740	20	3.52		Cuts resin
SA10_0000_ 2	0.32	0.0023	4.534	0.08	0.1062	0.0019	2.7	0.023			161	3.1	61	1.5	144.2	3.3	1789	11	1729	15	1712	34	-4.50		Cuts inclusion
SA10_0001_	0 2205	0.0014	2 705	0.042	0.0995	0.0015	1 0 7	0.01			202.2	4.2	160	2.2	24E 4	4.2	1331.	7 2	1226	12	1270	21	2 80	р	
SA10_0002_	0.2295	0.0014	2.705	0.042	0.0885	0.0015	1.02	0.01			292.2	4.2	102	2.5	243.4	4.2	,	7.5	1320	12	1370	51	2.80	ĸ	
1 SA10_0002_	0.1931	0.0023	2.012	0.085	0.0787	0.0034	2.708	0.026			62.62	0.4	23.43	0.22	33.5	1.2	1137	12	1084	30	947	96	-20.06	С	
2 SA10_0003	0.198	0.0015	2.063	0.045	0.0781	0.0018	2.621 0.971	0.015 0.008			175.3	1.7	67.39	0.75	104.7	2.2	1164 1739.	8.1	1126	15	1083	48	-7.48	С	
2	0.3099	0.0018	4.582	0.057	0.1105	0.0014	8	4			262.8	2.7	272.2	4.1	346.3	4.6	7	9	1743	10	1794	24	3.03	R	Fracture
SA10_0004_																									metamictiz
2 SA10_0006_	0.13128	0.00078	1.578	0.016	0.08988	0.00091	1.948	0.013			1229	10	632	6.1	623	6.8	795 1342.	4.4	960.1	6.4	1413	19	43.74		ation
1	0.2317	0.0018	2.828	0.048	0.0911	0.0015	2.043	0.021			257.4	1.2	127.4	1.4	210.2	3.3	6	9.4	1355	13	1422	32	5.58	С	Cuts
6410,0000																									inclusion,
1 1	0.182	0.0018	2.321	0.092	0.0951	0.0036	1.276	0.019			91.4	1.2	73	1.4	132.1	4.6	1077	10	1199	29	1396	78	22.85		damage
SA10_0011_ 2	0.5344	0.0034	13.66	0.14	0.1902	0.0019	1.837	0.011			181.8	2.9	98.7	1.4	395.4	4.8	2758	14	2722. 7	9.6	2734	17	-0.88	R	
SA10_0012_ 1	0.1801	0.0011	2.726	0.032	0.1127	0.0012	1.466 5	0.006 9			687.6	7.4	469.5	5.8	553.9	5.3	1067	6.1	1333. 4	8.6	1831	20	41.73	R	
SA10_0012_	0 2224	0.0021	4 662	0.069	0 1072	0.0015	2 026	0.018			199 7	27	62.2	1	161 4	2 9	1901	10	1755	12	1725	27	-3 80	c	
2	0.3224	0.0021	4.002	0.009	0.1072	0.0013	3.030	0.010			100.7	2.1	02.5	T	101.4	2.0	1001	10	1/33	12	1/33	21	-3.00	C	

CA10, 0012									1		107.0				1051						1		
SA10_0013_	0 21 4 4	0.0017	2 5 0	0.050	0.0000	0.0001	1 4 4 0	0.017	154.0		107.0	0.70	120.1	2.4	1251.		1204	17	1255	40	7.62		
	0.2144	0.0017	2.58	0.058	0.0892	0.0021	1.448	0.017	154.8	1.1	9	0.79	128.1	2.4	1201	8.9	1284	17	1355	48	7.62	к	
SA10_0013_	0 2201	0.0015	2 9 4 0	0.049	0.0000	0.001	1 0 2 1	0.012	252	2.1	121 7	2.2	244.1	2 7	1361.		1202	12	1272	24	0.64		Cuto sense
2	0.2391	0.0015	2.849	0.048	0.0888	0.0015	1.931	0.012	255	5.1	131.7	2.2	244.1	3.7	0	0	1303	15	13/3	54	-0.64		Cuts zones
SA10_0014_	0 2512	0.0024	2.67	0.047	0 1000	0.0011	1.707	0.000	C21 F	2.0	200.0	2.4	COC 4	6.2	1445	12	1501	10	1767	10	10.22		
	0.2513	0.0024	3.67	0.047	0.1086	0.0011	4	0.008	631.5	3.0	369.6	2.4	696.4	6.2	1445	13	1561	10	1/6/	18	18.22	к	
SA10_0014_	0 2052	0.004.0	4 35 9	0.054	0 4 0 7 0	0.004.0	2 4 0 0	0.010	202.0	<i></i>	476.0		204.0		1666.	~	4600	40	4747	22	4.50		<u>.</u>
2	0.2952	0.0018	4.258	0.051	0.1078	0.0013	2.189	0.013	383.9	6.1	1/6.3	3.4	391.8	5.8	8	9	1682	10	1/4/	23	4.59		Cuts resin
SA10_0015_	0 2070	0.0000	2 057	0.005	0.0000	0 0000	0.711	0.003					246		4.630	40	4500	40	4570		2.42	~	
1	0.2879	0.0023	3.857	0.085	0.0996	0.0022	5	/	104.4	1.2	146.4	1.7	346	4.5	1630	12	1592	18	1576	44	-3.43	C	
SA10_0015_							0.775	0.005														_	
2	0.2931	0.0022	4.039	0.072	0.1026	0.0019	5	9	146.1	2.8	190.5	4.8	455.8	9.8	1656	11	1632	15	1645	35	-0.67	С	
SA10_0016_							1.747	0.007							1400.								
1	0.2427	0.0015	2.839	0.047	0.0875	0.0015	3	9	262.1	3.5	149.2	2	299.9	4.4	3	7.6	1358	12	1339	34	-4.58	С	
SA10_0017_							0.897	0.003							1623.								
1	0.2865	0.0019	4.025	0.066	0.1057	0.0018	3	8	195.8	3	216.9	3.4	513.9	6.4	4	9.5	1634	13	1699	31	4.45		Cuts resin
SA10_0100_																							
1	0.1997	0.0036	2.25	0.13	0.086	0.0052	2.41	0.04	25.91	0.56	11.05	0.36	21.5	1.3	1174	20	1157	42	990	130	-18.59	С	
SA10_0100_																							
2	0.2004	0.0036	2.24	0.12	0.085	0.0048	3.418	0.049	26.6	0.43	7.84	0.16	14.22	0.86	1175	19	1147	40	990	130	-18.69	С	
SA10 0101							1.252	0.004							1455.								
2 – –	0.2534	0.0017	3.642	0.048	0.108	0.0014	9	9	360.9	3.4	285.1	2.7	548.5	5.2	3	8.9	1555	10	1752	23	16.93	R	
SA10 0101															1380.		1473.						
3	0.2389	0.0017	3.28	0.039	0.1034	0.0012	1.251	0.01	499.7	6.9	400.6	8.3	741.5	8.7	5	8.7	1	9	1673	21	17.48		Cuts zones
SA10_0103								0.004							1541								
2	0 2701	0.0015	3 813	0.056	0 1062	0.0015	0 814	5	344.6	39	418 1	44	869 1	6.8	3	75	1590	12	1716	25	10.18	C	
SA10_0104	0.2701	0.0015	5.015	0.050	0.1002	0.0015	1 0/6	0.004	344.0	5.5	410.1	7.7	005.1	0.0	1515	7.5	1550	12	1/10	25	10.10	C	Cuts
1	0 265	0.0017	3 72/	0.06	0 1053	0.0016	1.040	9	220.3	3 /	208.1	3 /	129.8	6.6	1313.	87	1570	13	1702	30	10.95		inclusion
1 SA10_0104	0.205	0.0017	5.724	0.00	0.1055	0.0010	5	5	220.5	5.4	200.1	5.4	425.0	0.0	1010	0.7	1210	15	1702	50	10.55		Motamicti
3A10_0104_	0 1609	0.0014	2 206	0 020	0 1022	0.001	1 /15	0.022	020	27	606	21	020	20	1010.	7.0	1210. C	0 E	1657	10	20.02		ration
2	0.1098	0.0014	2.500	0.028	0.1025	0.001	1.415	0.022	939	27	090	51	820	29	1124	7.9	0	0.5	1057	10	39.05		2011011
SA10_0105_	0 1025	0.0012	2 225	0.024	0.0007	0.001.4	1.099	0.000	425.0	C A	200.0	4.0	500.0	F 4	1134.	<i>с</i> 7	1015	10	1422	20	20.22		
	0.1925	0.0012	2.325	0.034	0.0907	0.0014	3	0.006	425.8	6.4	380.9	4.8	506.9	5.4	5	6.7	1215	10	1422	29	20.22	к	
SA10_0105_	0 2024	0.0017	2.264		0.000	0.0016	4 245	0.010	264.6	2.4	400.4	2.4	267.7		1187.		422.4	40	42.40	26	11.00		<u>.</u>
2	0.2024	0.0017	2.364	0.044	0.088	0.0016	1.315	0.018	261.6	2.1	198.1	3.1	267.7	3.7	8	9.1	1224	13	1348	36	11.88		Cuts resin
SA10_0106_							0.963								1426.								
1	0.2477	0.0016	3.102	0.051	0.0946	0.0016	5	0.004	224.9	1.1	229.1	1.2	466.8	5.1	3	8.2	1428	12	1490	32	4.28		Cuts zones
SA10_0106_															1370.								
2	0.237	0.0018	3.02	0.055	0.0963	0.0018	1.325	0.011	179.9	1.3	133.9	1.6	239.2	4.4	5	9.2	1408	14	1522	36	9.95		Cuts zones
SA10_0108_															1762.								
1	0.3143	0.002	4.465	0.068	0.107	0.0016	2.6	0.015	194.7	2.2	73.7	1	200.6	3.1	1	9.7	1718	13	1729	28	-1.91	R	
SA10_0109_							0.750	0.007															
2	0.3607	0.0056	6.21	0.27	0.1307	0.0054	3	1	26.24	0.3	34.46	0.46	110.2	3	1980	26	1951	34	1977	74	-0.15	С	
SA10_0110_							1.542								1683.								
1	0.2984	0.0019	4.049	0.059	0.1022	0.0015	8	0.009	207.3	3	131.3	1.5	336.8	4.4	5	9.4	1639	12	1644	27	-2.40	С	
																							Fracture,
SA10 0111																							radiation
1	0.5043	0.004	14	0.16	0.2086	0.0019	1.567	0.023	195.7	2.8	127.6	3.9	429.7	5.6	2630	17	2746	10	2888	15	8,93		damage
SA10 0112										-					1168			-		-			Radiation
1	0 1987	0.001	3 007	0.028	0 1135	0 0011	0 878	0.014	637 5	51	721 4	7	731 7	58		55	1407	72	1852	17	36.93		damage
- 1	0.1307	0.001	5.007	5.020	0.1100	5.0011	0.070	0.014	057.5	5.1	121.4	,	, 51.7	5.0	1	5.5	1407	,. <u> </u>	1002	1,	50.55		aamage

6440 0442	1								I						1207		1071				1		
SA10_0112_ 2	0 2061	0.0011	2 873	0.032	0 10/17	0.0012	3 09	0.018	503.7	35	160 5	13	356.6	4.4	1207. Q	5.6	1371.	8 /	1693	21	28.65	R	
2 SA10 0113	0.2001	0.0011	2.075	0.032	0.1047	0.0012	1 759	0.018	503.7	3.5	100.5	1.5	350.0	4.4	5	5.0	1729	0.4	1095	21	20.05	ĸ	
1	0.3148	0.0017	4.508	0.049	0.1074	0.0011	1	3	381.7	5	213.4	3.1	572	6.3	1764	8.2	3	9.1	1749	20	-0.86	R	
SA10_0115_							0.823	0.005							1678.								
1	0.2976	0.002	4.055	0.058	0.102	0.0015	6	8	210.8	4.3	255.1	6.4	647	14	7	9.9	1640	12	1642	28	-2.24		Cuts zones
SA10_0115_							1.399																
2	0.3057	0.0023	4.255	0.086	0.1041	0.0022	4	0.009	100.3	1.3	70.9	1	187.6	3.1	1719	12	1673	17	1664	39	-3.31	R	
SAIU_UII6_	0.2512	0.0017	2 2/	0.052	0 0006	0.0015	1 691	0.011	201.2	2.2	119 7	12	255 7	2.4	1445. o	80	1486	12	150/	20	0.20		Cuts resin
SA10 0116	0.2313	0.0017	5.54	0.052	0.0990	0.0015	1.081	0.006	201.5	2.2	110.7	1.5	255.7	5.4	0	8.9	1480	12	1334	25	9.50		Cuts resin
2	0.2425	0.0023	3.201	0.066	0.099	0.0019	0.634	1	168.5	3.4	263.3	5.4	518	14	1398	12	1446	16	1568	37	10.84	С	
SA10_0117_																							
2	0.193	0.0039	2.2	0.12	0.0865	0.0051	0.935	0.029	26.12	0.27	29.85	0.88	40.1	1.4	1136	21	1137	40	1000	130	-13.60		Cuts resin
SA10_0200_											108.4												Cuts
1	0.1952	0.0013	2.062	0.041	0.0791	0.0016	2.057	0.011	224.4	2.1	8	0.84	1/2.1	2.9	1149	6.9	1130	14	1139	40	-0.88		inclusion
SA10_0201_ 1	0 12929	0 0008	1 672	0.023	0.0966	0.0013	1 321	0.017	703 1	84	532 7	47	408.4	53	783 7	45	994.8	89	1542	27	49 18		Cuts zones
SA10 0201	0.12525	0.0000	1.072	0.025	0.0500	0.0015	1.521	0.017	/05.1	0.4	552.7	4.7	400.4	5.5	1021.	4.5	554.0	0.5	1542	27	45.10		cuts zones
2	0.1718	0.0011	1.866	0.039	0.0809	0.0017	0.759	0.011	318.3	5	433	11	607	13	7	6.1	1060	14	1168	42	12.53		Cuts zones
SA10_0202_							1.247	0.008							1730.								
1	0.308	0.0018	4.338	0.062	0.1051	0.0015	6	7	220.6	2.4	176.1	1.3	415	4.7	2	8.7	1694	12	1693	26	-2.20		Cuts zones
SA10_0205_	0.4040	0.0040	4 07	0.40	0.0700	0.0001	4 070	0.014	12.5	0.40		0.40	40.07	0.00	4000	26				24.0	117 50		Metamicti
2	0.1849	0.0048	1.87	0.18	0.0792	0.0081	1.078	0.014	12.5	0.18	11.7	0.18	18.07	0.93	1089	26	832	83	440	210	-147.50		zation
2	0 2649	0.002	3 689	0.069	0 1033	0.002	1 438	0.015	2	0.81	113.8	13	227.4	3 3	1514	10	1558	15	1643	36	7 85	R	
SA10 0207	0.2045	0.002	5.005	0.005	0.1055	0.002	1.450	0.015	-	0.01	115.0	1.5	227.4	5.5	1914	10	1550	15	1045	50	7.05	i.	Cuts
1	0.2634	0.0024	3.603	0.051	0.101	0.0012	1.551	0.014	399.6	6.2	262.9	5.6	520	4.9	1506	12	1545	11	1631	22	7.66		inclusion
SA10_0207_							1.438	0.006															
2	0.2959	0.002	4.091	0.061	0.1019	0.0016	8	8	210.9	3.4	148.2	2.6	359	5.5	1670	10	1645	12	1635	29	-2.14	R	
SA10_0209_	0.25.21	0.000	2 107	0.072	0.0025	0.0022	1 5 1 2	0.009	115 1	1 2	77	1	166 5	2 7	1452	10	1447	10	1422	40	1.40	c	
I SA10 0209	0.2551	0.002	3.197	0.073	0.0925	0.0022	1.512	5	115.1	1.5	//	T	100.5	3.7	1455	10	1447	19	1455	48	-1.40	C	
2	0.2356	0.0013	2.933	0.039	0.0913	0.0013	2.663	0.016	406.7	3.6	154.7	1.9	306.9	4.3	5	6.8	1387	10	1434	27	4.92	R	
SA10_0210_							0.631	0.005							1655.								Cuts
2	0.2928	0.0016	4.15	0.059	0.1032	0.0015	4	7	261.2	5.3	426	12	1012	23	8	8	1660	12	1669	26	0.79		inclusion
SA10_0211_																							
2	0.2864	0.0032	4.07	0.12	0.104	0.0031	1.223	0.011	56.25	0.91	46.71	0.87	100.4	2.7	1622	16	1621	25	1597	60	-1.57		Cuts resin
SA10_0213_ 1	0.2828	0.0017	2 017	0.05	0 1006	0.0014	1 1 2 1	0.029	260.1	24	65 76	0.42	150.2	25	1605.	8.1	1614	10	1614	26	0.55		Cuts resin
SA10 0214	0.2020	0.0017	5.917	0.05	0.1000	0.0014	1 925	0.029	205.1	2.4	109.1	0.45	150.2	2.5	1778	0.4	1014	10	1014	20	0.55		Cuts resin
1	0.3178	0.0019	4.683	0.071	0.1069	0.0017	5	7	208.6	1.6	7	0.75	281.8	3.5	3	9.1	1757	13	1726	29	-3.03	R	
SA10_0214_															1649.		1690.						
2	0.2916	0.0015	4.299	0.041	0.10653	0.00099	2.46	0.011	547.3	5.7	224.5	2.8	458.9	4.6	7	7.4	8	8	1733	18	4.81		Cuts resin
																							Cuts
\$410 0215																							inclusion,
3A10_0213_ 1	0 2288	0.0026	2 744	0.051	0.087	0.0014	1 641	0.028	302	12	201	11	327	13	1327	14	1336	14	1331	33	0.30		damage
-	0.2200	3.0020	_ .,	5.051	0.007	5.002.	1.0.1		1 002		201		527		1017		2000		1001	55	1 0.00		

SA10_0217_ 1	0.1977	0.0031	2.5	0.12	0.0926	0.0042	1.282	0.019	56.5	1	44.44	0.85	65.6	2.5	1161	17	1247	29	1316	84	11.78		Cuts resin
SA10_0217_ 3	0.2234	0.0024	2.609	0.086	0.0846	0.0029	1.646	0.013	69.36	0.79	42.3	0.43	78.2	1.8	1299	13	1285	24	1208	69	-7.53	R	
SA10_0300_ 2	0.2699	0.002	3.809	0.077	0.1022	0.0022	1.149 7	0.006	126.7	2.4	110.5	2.1	227.7	4.9	1540	10	1584	16	1624	40	5.17		Cuts resin
SA10 0301																							inclusion, radiation
1 SA10_0301	0.1952	0.0023	2.801	0.041	0.1038	0.0011	0.884	0.008	743	19	864	29	1129	19	1148	13	1350	11	1683	19	31.79		damage
2 SA10_0302	0.269	0.0028	3.783	0.077	0.1022	0.002	1.231	0.02	149.5	2.6	127.6	4.3	214.8	3.3	1534	14	1577	17	1638	36	6.35	R	
1	0.2062	0.0025	2.308	0.085	0.0826	0.0032	1.924	0.017	55.79	0.83	28.97	0.4	51.7	1.5	1207	13	1187	27	1078	85	-11.97	R	Cuts
SA10_0303																							zones, nearby
1 SA10_0303	0.1113	0.0014	1.472	0.022	0.0965	0.0011	3.801	0.021	1351	22	354.1	5.3	583.9	6.2	680.1	7.9	915	8.9	1542	22	55.89		fractures
2 SA10_0304	0.2667	0.0027	3.327	0.09	0.0916	0.0025	1.443	0.013	78.25	0.88	54.12	0.44	116.9	2.6	1524	14	1477	22	1404	56	-8.55	С	
1 SA10_0305	0.2157	0.0022	2.478	0.068	0.0843	0.0023	1.477	0.012	101.6	2	69.3 123.8	1.7	124.9	3.2	1259 1608	12	1250	20	1229	55	-2.44	С	
1 SA10_0305	0.2835	0.0017	3.862	0.051	0.1014	0.0014	2.389	0.014	298.8	1.2	5	0.64	228.6	3	1500. 1593	8.3	1602	11	1633	25	1.50	R	
2	0.2806	0.0017	3.857	0.06	0.1026	0.0016	1.653	0.01	210.7	2.6	126.2	1.5	255.8	4.5	1333. 9	8.7	1598	13	1649	29	3.34		Cuts resin
1 5A10_0309_	0.2301	0.0014	2.647	0.039	0.0865	0.0013	1.480 4 2.240	1	321.5	4.8	213.3	3	370.9	5.2	1334. 4 1332	7.4	1309	11	1322	30	-0.94	С	
2	0.2297	0.0014	2.62	0.039	0.0857	0.0013	7	7	395.5	4.3	174	2	314.5	4.4	6	7.3	1302	11	1310	30	-1.73		Cuts resin
1 5A10_0313_	0.2615	0.0029	3.699	0.052	0.1069	0.0011	2.096	0.035	610	10	298	8.4	556	16	1496	15	1567	11	1738	19	13.92	С	
1	0.2229	0.0017	2.434	0.053	0.083	0.0018	1.92	0.011	173.1	2.2	88.8	1.3	152.4	2.9	7	9.1	1246	16	1230	44	-5.42	R	Fracture,
\$410.0315							1 /06	0.009							1525								cuts zones,
1	0.267	0.0016	3.635	0.045	0.1034	0.0013	1.400	1	357	2.8	250.5	2.9	258.1	3.3	3	8.2	1553	10	1670	24	8.66		inclusion
2	0.2592	0.0028	3.671	0.095	0.1079	0.0028	0.997	6	84.02	0.81	82.19	0.8	144.2	3.2	1484	14	1550	21	1705	52	12.96	С	Cuto
2 \$\\\10_0217	0.302	0.0027	4.419	0.071	0.1119	0.0015	1.873	0.03	353	12	194.8	8.6	393	12	1700	13	1712	13	1811	24	6.13		inclusion
1 5A10_0317_	0.2232	0.0027	2.411	0.088	0.0831	0.0031	1.919	0.016	66.8	0.81	34.29	0.49	58	1.6	1297	14	1221	26	1126	78	-15.19	R	
2 5A10_0317_ 2	0.2202	0.0038	2.94	0.2	0.1005	0.0057	1.284	0.015	49.81	0.55	38.64	0.73	78.2	5.8	1282	20	1306	43	1400	110	8.43		Cuts resin
1	0.2467	0.0019	3.011	0.062	0.0926	0.0019	2.384	0.014	167.7	1.5	69.19	0.64	128.2	2.3	4	9.8	1400	16	1434	40	0.88	R	

\$410.0402											1												1		
1 SA10_0402_ SA10_0403	0.2835	0.0053	4.02	0.2	0.1099	0.0058	2.554 0.676	0.043			20.67	0.17	8.11	0.12	16.49	0.9	1604	27	1575	42	1530	110	-4.84		Cuts resin
2 SA10 0405	0.2741	0.0029	3.76	0.11	0.1033	0.003	2	4			72.78	0.69	106.7	1.1	215	3.4	1560	14	1565	23	1603	56	2.68	R	
2 SA10 0406	0.5339	0.0049	14.53	0.23	0.203	0.0033	1.68	0.014			60.65	0.87	35.72	0.5	129.8	2.4	2755	21	2775	15	2829	28	2.62	R	
1 SA10_0407_	0.2951	0.003	4.29 10.74	0.11	0.1084	0.0029	2.775	0.034			75.6	1.5	27.51	0.71	64.3	2.3	1665	15	1675 2500.	22	1720	51	3.20	С	
1 SA10_0408_	0.4184	0.0023	9	0.082	0.1891	0.0014	1.371	0.012			495	6.4	362.9	7.2	644	16	2252	11	3	7.2	2729	12	17.48	С	
1	0.2469	0.002	3.499	0.071	0.1042	0.0022	0.767	0.018			163.9	2.3	232.1	8.9	329.5	5	1422	10	1518	16	1666	39	14.65		Cuts zones Cuts inclusion,
SA10_0410_ 1 SA10_0411	0.2285	0.0044	3.317	0.072	0.1067	0.0019	0.841 4	0.006 4			242.4	4.5	285.8	4	535.5	8.1	1322	24	1471	17	1719	33	23.09		damage
1 SA10_0412_	0.1551	0.0015	1.615	0.036	0.0756	0.0018	2.578	0.066			254.1	2.9	105.1	2.3	121.4	2.8	929.1	8.1	970 1626.	14	1009	52	7.92		Cuts resin
1 SA10_0415_	0.2648	0.002	3.981	0.047	0.1062	0.001	1.615	0.016			629	16	399	14	733	13	1514	10	7	9.5	1725	18	12.23	С	
1	0.3677	0.0032	9.3	0.11	0.1771	0.0014	2.215	0.02			428.9	2	197	2.4	460.4	4.7	2017	15	2363	10	2619	13	22.99	R	Cuts inclusion,
SA10_0415_																	1747.		2237.						radiation
2 SA10_0417_	0.3114	0.0018	8.082	0.065	0.1808	0.0013	1.098 0.502	0.022 0.002			798	11	794	29	690.4	6	3	8.7	7	7.2	2655	12	34.19		damage Cuts
1 SA10_0501_	0.1416	0.001	1.557	0.037	0.0765	0.0019	6	6			250	3.2	510.1	7.8	553.7	7.5	853.2 1381.	5.7	946	15	1038	51	17.80		incllusion
1 SA10_0501_	0.2392	0.0017	3.541	0.063	0.1021	0.0019	1.976	0.011			214.7	1.8	111.5	1.1	196	2.9	8 1375.	8.8	1528	14	1625	35	14.97	R	
2 SA10_0502_	0.238	0.0015	3.545	0.053	0.1022	0.0016	2.187 1.834	0.011 0.009			297.8	3.3	140.2	1.6	247	3.4	7 1396.	7.8	1533	12	1650	29	16.62	R	
1	0.2419	0.0015	3.695	0.05	0.1042	0.0014	4	4			346.2	4.4	194.5	2.2	346.4	4.1	3	1.1	1566	11	1684	25	17.08	L	Fracture,
1	0.1228	0.0017	1.595	0.063	0.0886	0.0036	1.434	0.012			105.9	1.1	77	1.2	59	1.6	745.9	9.8	941	25	1211	86	38.41		damage Fracture.
SA10_0503_																									radiation
2 SA21C_0002	0.156	0.0013	2.036	0.049	0.0887	0.0022	1.72	0.011			202.2	1	122.4	1	114.5	2.3	933.9	7.5	1116	16	1334	49	29.99		damage
_1 SA21C_0003	0.3152	0.0044	4.36	0.12	0.1008	0.0025	3.005	0.028	121000	42000	188.4	2.6	58.67	0.87	199.6	5.9	1764	22	1696	22	1612	48	-9.43	С	
_1 SA21C_0004	0.1943	0.0034	2.005	0.083	0.0754	0.0031	1.551	0.015	32000	14000	113.3	1.7	67.2	1	158.4	4.7	1143	18	1100	29	973	92	-17.47	R	
_1 SA21C_0005	0.2086	0.0033	2.269	0.079	0.0797	0.0028	1.477	0.018	43000	20000	166.5	2.3	103.3	1.4	196.8	5	1220	18	1192	25	1122	72	-8.73	С	
_1	0.58	0.01	19.76	0.49	0.2487	0.0059	1.734	0.056	31000	15000	47.72	0.86	25.76	0.88	153.6	5	2942	42	3068	24	3155	38	6.75	С	

SA21C_0007	0.2506	0.006	9.01	0.19	0 1662	0.0020	1 525	0.019	100000	40000	202.6	2.1	171.0	2	240 E	0 0	1024	20	2222	20	2504	20	22.76	в	
_1 SA21C_0008	0.5500	0.000	8.01	0.18	0.1002	0.0029	1.555	0.016	109000	40000	202.0	5.1	121.0	2	549.5	0.5	1954	29	2225	20	2504	50	22.70	n	
_1 \$421C_0100	0.1914	0.0045	1.99	0.13	0.0777	0.0054	1.466	0.019	9900	4100	52.19	0.81	33.92	0.56	74.6	3	1127	24	1076	48	880	150	-28.07	R	
_1	0.2192	0.0049	2.44	0.16	0.0828	0.0056	1.078	0.014	10500	3700	42.52	0.72	38.2	0.7	88.5	3.4	1275	26	1217	48	1030	140	-23.79	С	
SA21C_0101 1	0 1849	0.0026	1 818	0 044	0 0714	0 0017	2 248	0.016	84000	38000	554 3	8.8	241 1	4 1	442.6	95	1093	14	1048	16	936	49	-16 77	C	
SA21C_0101																								-	Cuts
_2 SA21C 0102	0.178	0.0039	2.23	0.15	0.0918	0.0059	1.666 0.733	0.038 0.007	15400	6200	91.2	1.3	55.2	1.7	110	10	1054	22	1148	47	1220	140	13.61		inclusion
_1	0.1857	0.0043	1.86	0.12	0.074	0.005	1	8	16100	4900	61.73	0.97	84.8	1.3	137.8	4.6	1096	24	1040	45	790	150	-38.73	R	
SA21C_0104 _1	0.2657	0.0037	3.719	0.081	0.1017	0.0021	1.192	0.009 6	157000	47000	466.3	6.6	405.4	5.2	696	13	1518	19	1570	18	1630	40	6.87	R	
SA21C_0105	0 5 2 2 5	0.0085	12.46	0.2	0 1825	0.0041	1 220	0.014	50000	15000	70	1 2	66.6	1	7727	5.6	2751	36	2702	21	2650	27	-2.46	D	
_1	0.5555	0.0085	13.40	0.5	0.1825	0.0041	1.239	0.014	30000	15000	75	1.2	00.0	I	223.7	5.0	2751	30	2702	21	2033	57	-3.40	N	Fracture,
SA21C_0106 1	0.2896	0.004	3.882	0.099	0.0966	0.0023	0.980 2	0.008 3	89000	34000	335.1	4.9	357.9	5.8	680	13	1640	20	1600	20	1532	44	-7.05		cuts inclusion
SA21C_0107																								_	
_1 SA21C 0108	0.1819	0.0046	1.76	0.15	0.0698	0.0059	0.994	0.014	10400	4100	60.1	1	63.1	1.2	78	3.4	1075	25	954	57	590	180	-82.20	R	
_1	0.3194	0.0044	4.71	0.1	0.1069	0.0023	2.569	0.024	152000	51000	384.5	7.9	155.1	3.2	320.3	8.3	1785	22	1765	18	1719	41	-3.84	R	
_1	0.5295	0.0074	13.49	0.27	0.1839	0.0033	1.613	0.014	98000	42000	203.3	2.8	128.3	1.9	402.5	8.8	2736	31	2705	19	2672	30	-2.40	R	
SA21C_0200	0 2211	0.0062	2 44	0.21	0 0814	0 0071	0.635	0.008 5	9500	3600	37 35	0.67	59.2	1	84 9	3.2	1284	33	1147	73	850	200	-51.06	C	
SA21C_0201	0.2211	0.0002	2.44	0.21	0.0014	0.0071	Ū	5	5500	3000	57.55	0.07	55.2	-	04.5	5.2	1204	33	1147	,5	050	200	51.00	C	
_1 SA21C 0202	0.2878	0.0047	3.79	0.14	0.0954	0.0035	2.297	0.026	56000	20000	159.9	2.2	70.1	1.2	124.2	4.5	1628	23	1576	30	1488	68	-9.41	С	
_1	0.681	0.011	29.76	0.57	0.3148	0.0047	1.015	0.011	202000	54000	155	2.8	152.6	3	466.3	9.9	3346	43	3472	19	3535	23	5.35	R	C .
SA21C_0203 _1	0.2248	0.0043	2.44	0.11	0.0792	0.0037	1.498	0.016	69000	18000	149.2	2.2	99.3	1.5	142.2	5	1305	23	1239	33	1065	99	-22.54		Cuts inclusion
SA21C_0205	0 2247	0.0061	2 82	0.21	0.0936	0.0072	1 275	0.021	12600	5100	52.68	0.95	11 16	0.0	62.6	2 7	1202	22	1220	55	1170	170	-11 27		Cuts rosin
	0.2247	0.0001	2.02	0.21	0.0550	0.0072	1.275	0.021	13000	5100	52.00	0.55	41.40	0.5	02.0	5.2	1505	52	1525	55	11/0	170	11.57		cuts resin
_1 SA21C 0207	0.5248	0.0066	13.06	0.18	0.1788	0.0019	3.456	0.028	360000	130000	608.7	9.8	176.5	2.8	535	11	2716	28	2681	13	2638	18	-2.96	С	
_1	0.2669	0.0038	3.613	0.075	0.0977	0.0016	1.503	0.013	158000	92000	876	16	588	14	853	15	1524	19	1546	16	1564	32	2.56	С	
SA21C_0208 _1	0.1776	0.0026	1.702	0.055	0.0692	0.0022	1.358	0.01	84000	32000	433.8	6.2	322.5	4.4	367.2	7.6	1053	14	1004	20	862	65	-22.16	R	
SA21C_0209	0 1896	0.0043	1 02	0.12	0.0728	0.0052	1 001	0.012	25200	7200	85.6	1 /	70.7	1 2	02.2	2.1	1110	22	1059	11	780	150	-13.16	D	
	0.1090	0.0045	1.92	0.13	0.0730	0.0052	0.630	0.015	23300	7200	05.0	1.4	13.1	1.3	52.2	5.4	1119	20	1028		760	130	-43.40	IX.	
_1 SA21C_0301	0.522	0.0075	13.01	0.31	0.1803	0.0044	8	5	67000	23000	112.6	1.6	180.9	2.6	548	11	2704	32	2671	23	2627	40	-2.93	R	
_1	0.1914	0.0034	2.119	0.081	0.08	0.0031	1.309	0.014	48000	18000	249.1	4.5	193.2	4	199.3	5.8	1128	19	1141	26	1114	81	-1.26	R	
SA21C_0302 _1	0.2155	0.0031	2.498	0.06	0.0835	0.0018	1.611	0.013	154000	57000	726	16	452.3	9.7	510	11	1257	16	1268	17	1259	42	0.16		Cuts inclusion,

																									radiation damage
SA21C_0303 _1	0.3211	0.0043	4.68	0.099	0.1051	0.0022	1.253	0.009 4	173000	62000	451.9	6.9	361.5	5.6	689	12	1794	21	1758	17	1690	39	-6.15	С	
_1	0.1888	0.0026	1.967	0.051	0.0751	0.002	0.941 9	5	184000	51000	555.8	8.2	589.9	8.9	700	12	1114	14	1100	17	1039	51	-7.22	R	
SA21C_0305	0.2221	0.0051	2.43	0.15	0.079	0.0048	1.812	0.025	15900	6400	83.4	1.2	46.64	0.78	66	3.2	1290	27	1212	46	980	130	-31.63	С	
_1	0.2261	0.004	2.64	0.1	0.0849	0.0032	1.528	0.019	28000	13000	153.4	2.6	102.9	1.9	143.6	4.6	1313	21	1300	30	1233	78	-6.49	R	
_1 \$421C_0308	0.3174	0.0039	4.704	0.084	0.1066	0.0016	2	9	155000	68000	528.4	7.4	521.1	7.1	1037	18	1776	19	1762	15	1727	29	-2.84	С	
_1	0.2263	0.0056	2.49	0.16	0.0815	0.0054	0.964	0.013	20200	7000	65.3	1	70.9	1.1	103.3	4.2	1312	29	1235	48	1020	140	-28.63	R	Fracture
SA21C_0309	0.0933	0.0044	1.061	0.092	0.0839	0.0067	1.079	0.033	15300	5100	98	4.2	97.9	4.8	49.4	3	573	26	698	47	970	180	40.93		cuts
SA21C_0400	0 2931	0.0052	4 04	0.16	0.0996	0.0039	0.828	0.007	55000	32000	131 7	23	163.3	2.9	326	7.6	1654	26	1620	32	1540	76	-7 40		Cuts zones
SA21C_0401	0.1803	0.0052	2.26	0.22	0.0977	0.0000	1 962	0.027	-12800	6900	20.48	0.58	16 5 8	0.28	24.2	1.0	1114	21	1020	92	870	220	-28.05	D	cuts zones
- ¹	0.1895	0.0058	2.20	0.22	0.0877	0.0092	1.805	0.037	-12800 -	0900	50.48	0.58	10.58	0.58	24.2	1.5	1114	51	1007	05	870	220	-28.05	ĸ	Padiation
_1	0.1219	0.0015	2.564	0.039	0.1509	0.002	3.373	0.026	0	290000	1694	25	495.6	7.2	1348	20	741.2	8.4	1287	11	2349	23	68.45		damage
_1	0.3072	0.0041	4.499	0.097	0.1052	0.0021	3.491	0.03	440000	0	359.1	6.3	99.5	2	184.8	5.8	1725	20	1723	18	1699	36	-1.53	С	Fractures
SA21C_0404	0 2106	0.0040	2.08	0.12	0 1015	0.004	1 094	0.012	280000	100000	120.0	26	122 6	Λ	177	E /	1000	26	1270	24	1501	75	22.07		radiation
_1 SA21C_0405	0.2100	0.0049	2.90	0.15	0.1015	0.004	1.004	0.015	450000	100000	159.9	5.0	125.0	4	200.0	5.4	1252	20	1579	54	1501	22	22.07		Cute reasin
_1 SA21C_0406	0.2707	0.0033	3.806	0.068	0.1014	0.0019	1.156	0.065	450000	120000	495.7	6.4	452	21	300.8	8.4	1543	17	1291	14	1039	33	5.80		Cuts resin
_1 SA21C_0407	0.227	0.0033	2.6	0.085	0.0822	0.0027	1.882	0.018	86000	35000	243.2	4.1	122.6	2.2	211.1	6.4	1318	17	1286	24	1200	67	-9.83	к	
_1 SA21C_0408	0.2131	0.0058	2.38	0.23	0.0825	0.0084	1.597	0.029	2600	4600	38.21	0.74	23.44	0.52	38.8	2.4	1242	31	1115	76	750	210	-65.60	C	
_1 SA21C_0409	0.1921	0.0058	1.93	0.21	0.0735	0.0078	2.572	0.052	2100	4000	36.54	0.55	14.3	0.32	18.6	1.6	1129	31	959	79	550	220	-105.27	R	Hit existing
_1 SA21C_0500	0.1618	0.0038	2.595	0.063	0.1158	0.0017	0.966	0.025	205000	99000	1307	23	1410	22	2004	30	965	21	1291	18	1883	27	48.75		spot Radiation
_1 SA21C_0503	0.1891	0.0042	2.79	0.15	0.1075	0.0072	1.174	0.023	22000	20000	124.4	4.7	113.6	6.2	186	13	1115	23	1325	41	1620	120	31.17		damage Radiation
_1 SA21C_0504	0.2391	0.0042	3.276	0.098	0.0988	0.0029	1.423	0.019	35000	73000	235.7	5.1	182.4	4.9	176.3	6.3	1380	22	1462	24	1567	56	11.93		damage
_1	0.2245	0.0037	2.512	0.086	0.081	0.0027	1.567	0.013	14000	87000	203.6	3.1	141.7	2.3	273.6	7.2	1304	19	1269	25	1162	68	-12.22	R	Fracture,
SA21C_0505 _1	0.1912	0.0034	2.233	0.095	0.0847	0.0034	1.103	0.011	175000	78000	119.8	1.8	117.3	1.9	191.6	6	1127	18	1172	31	1212	82	7.01		radiation damage

SA21C_0506							0.617	0.005																
_1	0.2235	0.0038	2.71	0.12	0.0878	0.0039	3	5	220000	150000	78.8	1.3	135.5	2	311.5	7.7	1299	20	1312	32	1265	96	-2.69	R
SA21C_0507																								
_1	0.1967	0.006	2.03	0.2	0.0772	0.0079	1.149	0.021	15000	11000	18.66	0.41	16.14	0.45	40.7	2.6	1153	32	1026	76	710	210	-62.39	С
SA21C_0508																								
_1	0.2816	0.0092	3.9	0.41	0.103	0.011	0.614	0.013	7000	6300	9.5	0.18	15.08	0.29	58.5	3.1	1591	46	1380	110	1060	240	-50.09	Cuts res
SA21C_0509																								
_1	0.2079	0.003	2.315	0.068	0.0803	0.0023	1.679	0.013	144000	85000	184	2.7	103.9	1.5	305.7	7.2	1218	16	1208	21	1169	58	-4.19	С

Plesovice Standards

Stanuarus																							
												Appro		Appro		Appro							
											Appro	х	Appro	х	Appro	х							
	206	206	207	207	207	207	U/Th	U/Th			х	U	х	Th	х	Pb	206	206	207	207	207	207	%
	/238	/238	/235	/235	/206	/206	Ratio	Ratio			U	PPM	Th	PPM	Pb	PPM	/238	/238	/235	/235	/206	/206	Discord
Standards A	Ratio	2SE	Ratio	2SE	Ratio	2SE		2SE			PPM	2SE	PPM	2SE	PPM	2SE	Age	2SE	Age	2SE	Age	2SE	ance
Z_Plesovice_			0.391	0.009																			
1	0.05367	0.00039	5	7	0.0538	0.0014	9.679	0.051			755.8	8	78.09	0.96	39	1.5	337	2.4	333.7	7	308	53	-9.42
Z_Plesovice_																							
2	0.0537	0.00037	0.394	0.01	0.0536	0.0015	9.682	0.051			/53.8	8.3	//.91	0.93	39	1.4	337.2	2.2	334.6	7.5	291	57	-15.88
Z_Plesovice_	0.05262	0.00025	0 402	0.01	0.05.46	0.0015	0 (77	0.040			750.0	0.1	70.4		20	1.2	226.0	2.2	240.0	7.0	226	F7	0.24
3 7 Discovice	0.05363	0.00035	0.402	0.01	0.0546	0.0015	9.677	0.049			/58.8	9.1	78.4	1.1	39	1.3	330.8	2.2	340.9	7.6	330	57	-0.24
Z_Plesovice_	0.05275	0 00025	0.389	0.009	0.0525	0.001.2	0 696	0.05			753 0	7 5	77 70	0 97	20 0	1 2	227 E	2.1	222	67	262	FO	20 22
4 7 Plesovice	0.05575	0.00055	0 203	2	0.0525	0.0012	9.000	0.05			/52.0	7.5	//./9	0.87	30.9	1.5	557.5	2.1	552	0.7	205	50	-20.55
2_Flesovice_	0.05369	0.00036	0.333	6	0.053	0.0013	9 667	0.048			760 3	87	78.6	1	39.2	14	337 1	22	335.4	7	287	51	-17 46
7 Plesovice	0.05505	0.00050	0 396	0 008	0.055	0.0015	5.007	0.040			700.5	0.7	70.0	-	55.2	1.4	557.1	2.2	555.4	,	207	51	17.40
6	0.05363	0 00035	6.556	8	0.0539	0.0013	9 693	0.048			751 2	81	77 55	0.92	38.8	14	336.8	21	337 3	64	321	50	-4 92
Z Plesovice	0.000000	0.00000	0.394	0.009	0100000	0.0010	5.050	01010			/01/2	0.1	///00	0.52	50.0		00010		00710	0	021	50	
7	0.05364	0.00036	7	2	0.0537	0.0013	9.679	0.047			754.4	9.4	78	1.1	39.1	1.3	336.8	2.2	335.6	6.7	308	50	-9.35
Z Plesovice			0.384	0.008																			
8	0.05371	0.00033	8	9	0.0523	0.0013	9.672	0.044			757	8.2	78.33	0.97	38.8	1.2	337.2	2	329	6.6	254	51	-32.76
Z_Plesovice_			0.405	0.009																			
9	0.05372	0.00035	5	5	0.0549	0.0013	9.678	0.05			757.3	6.6	78.14	0.75	39.4	1.2	337.3	2.2	343.4	6.8	357	50	5.52
Z_Plesovice_			0.389	0.009																			
10	0.05365	0.00037	8	5	0.0532	0.0013	9.682	0.05			751.7	5.7	77.67	0.64	38.7	1.4	336.8	2.3	333	7.1	289	54	-16.54
								Final_				Appro		Appro		Appro		FinalA		FinalA		FinalA	
				Final2			Final_	U_Th				x_U_		x_Th_		x_Pb_		ge206		ge207		ge207	
		Final206	Final2	07_2		Final207	U_Th	_Rati		Final206	Appro	PPM_	Appro	PPM_	Appro	PPM_	FinalA	_238	FinalA	_235	FinalA	_206	
	Final206	_238_In	07_2	35_In	Final207	_206_In	_Rati	o_Int	Final206	_204_In	x_U_	Int2S	x_Th_	Int2S	x_Pb_	Int2S	ge206	_Int2	ge207	_Int2	ge207	_Int2	
Standards B	_238	t2SE	35	t2SE	_206	t2SE	0	2SE	_204	t2SE	PPM	E	PPM	E	PPM	E	_238	SE	_235	SE	_206	SE	
Output 1 1	0.05245	0.00086	0 284	0.021	0.0522	0 0020	0 608	0 090	120000	420000	751	11	77.6	12	27.0	20	225.6	5.2	224	16	100	110	-76.63
Output_1_1	0.05545	0.00080	0.304	0.021	0.0522	0.0029	9.008	0.089	130000	430000	/51	11	77.0	1.5	57.5	2.9	555.0	5.5	524	10	190	110	-70.03
Output_1_2	0.05471	0.00085	0.469	0.027	0.0619	0.0035	9.793	0.093	3000	110000	697	10	71.1	1.2	69.8	6.6	343.3	5.2	385	18	560	120	38.70
Output 1 3	0.05482	0 00085	0 415	0.019	0 0552	0.0025	9 662	0 096	252000	91000	709	11	73 7	13	43 4	32	344	52	350	14	328	94	-4 88
Sachar_7_2	0.00402	5.00005	0.415	5.015	0.0332	5.0025	5.002	5.050	232000	31000	,05	**	, 5.7	1.5	-3.4	5.2	344	3.2	555	T -4	520	34	4.00

									-														
Output 1 4	0.05405	0.00079	0.405	0.018	0.0541	0.0024	9.728	0.085	5.00E+0 6	1.80E+0 6	772	13	79.9	1.4	41.5	3	339.3	4.8	343	13	299	92	-13.48
Output_1_5	0.05339	0.00081	0.403	0.018	0.0546	0.0024	9.157	0.083	-174000	59000	736	11	81.1	1.3	41.6	3	335.2	5	340	13	321	92	-4.42
Output_1_6	0.05322	0.0008	0.389	0.019	0.0536	0.0026	9.491	0.084	-230000	480000	765.9	9.9	81.5	1.1	43.5	3.2	334.2	4.9	331	14	270	100	-23.78
Output_1_7	0.05348	0.00083	0.393	0.019	0.0538	0.0026	9.8	0.097	55000	25000	743	11	76.6	1.3	38	2.9	335.7	5.1	332	13	266	96	-26.20
Output_1_8	0.05361	0.00082	0.386	0.02	0.0521	0.0026	10.07	0.11	26000	16000	698.7	9.6	69.7	1.1	33.4	2.6	336.6	5	326	15	210	100	-60.29
Output_1_9	0.05356	0.00083	0.385	0.018	0.0529	0.0025	9.96	0.089	14000	14000	734	11	73.3	1.1	37.5	2.5	336.2	5.1	328	13	238	97	-41.26
Output_1_10	0.05367	0.00082	0.391	0.017	0.0527	0.0024	9.613	0.08 Final	-140000	210000	758	11 Appro	78.4	1.2 Appro	38.9	2.8 Appro	336.9	5 Einal A	332	13 Final A	260	95 EinalA	-29.58
542	Final206	Final206 _238_In t2SE	Final2 07_2 35	Final2 07_2 35_In t2SE	Final207 206	Final207 _206_In t2SE	Final_ U_Th _Rati 0	Final_ U_Th _Rati o_Int 2SF	Final206 204	Final206 _204_In t2SE	Appro x_U_ PPM	Appro x_U_ PPM_ Int2S F	Appro x_Th_ PPM	Appro x_Th_ PPM_ Int2S F	Appro x_Pb_ PPM	Appro x_Pb_ PPM_ Int2S F	FinalA ge206 238	FinalA ge206 _238 _Int2 SF	FinalA ge207 235	FinalA ge207 _235 _Int2 SF	FinalA ge207 206	FinalA ge207 _206 _Int2 SF	
Z_Plesovice_	0.0526	0.001	0 277	0.027	_200	0.0024	0 72	0.12		25000	760.1	76	79.6	-	21.6	2	2250	6 1	216	20	_200	120	290 57
Z_Plesovice_	0.0530	0.001	0.377	0.027	0.0489	0.0034	9.72	0.13	116000	23000 2.80E+0	760.1	7.0	/8.0	1.1	31.0	3	330.4	0.1	310	20	70	130	-380.57
2 Z_Plesovice_	0.05378	0.00097	0.398	0.025	0.0533	0.0036	9.51	0.12	50000	6	731.4	8.3	75.5	1.1	37.5	3.4	337.6	5.9	335	18	190	130	-77.68
3 Z_Plesovice_	0.05419	0.00071	0.379	0.025	0.0495	0.0034	10.06	0.11	-800000	150000	833.1	9	86.3	1.2	51.5	5.9	340.2	4.3	319	19	70	130	-386.00
4 Z Plesovice	0.0526	0.001	0.389	0.029	0.0524	0.004	9.59	0.12	270000	170000	704.7	7.6	71.2	1.1	33.8	4.7	330.3	6.2	324	21	150	140	-120.20
5 7 Plesovice	0.05306	0.00078	0.428	0.024	0.057	0.0034	9.59	0.1	-13000	54000	875	10	92.8	1.3	68.8	6	333.2	4.8	355	17	360	120	7.44
6 7 Discovice_	0.0552	0.0012	0.453	0.06	0.0579	0.0074	10.64	0.14	55000	52000	716.9	7.6	71.9	1.1	40.3	6.6	346.5	7.4	339	31	170	190	-103.82
Z_Plesovice_ 7	0.05337	0.0009	0.398	0.03	0.0526	0.004	8.81	0.11	340000	200000	796.1	9.4	86.7	1.3	49.6	6.3	335.1	5.5	330	22	160	150	-109.44
Z_Plesovice_ 8	0.0547	0.00092	0.411	0.033	0.0537	0.0044	10.29	0.12	-54000	45000	737.1	8.4	74.6	1.1	39.1	5.3	343.2	5.6	337	24	170	160	-101.88
Z_Plesovice_ 9	0.05264	0.00088	0.347	0.034	0.0471	0.0046	8.982	0.095	44000	43000	766	8.5	81.3	1.1	40.8	5.8	330.6	5.4	291	26	-70	180	572.29
Z_Plesovice_ 10	0.0541	0.0011	0.404	0.027	0.0527	0.0036	10.24	0.13	520000	140000	751.2	8.3	76.6	1	38.1	3.7	339.7	6.5	338	20	220	140	-54.41
Z_Plesovice_	0.05349	0 0009	0 384	0.025	0.0516	0 0034	9 64	0 12	92000	28000	747 8	91	77 8	12	40 5	3.6	335.8	55	327	19	160	130	-109 88
Z_Plesovice_	0.05433	0.0000	0.304	0.025	0.0510	0.0034	0.00	0.12	00000	20000	700.7	0.7	01.1	1.2	40.5	3.0	241.0	5.5	327	10	170	130	100.04
12 Z_Plesovice_	0.05432	0.00094	0.389	0.025	0.0518	0.0034	9.98	0.11	98000	23000	/80./	8.7	81.1	1.1	43.3	3.6	341.6	5.6	329	19	170	130	-100.94
13 Z_Plesovice_	0.05348	0.00099	0.419	0.031	0.056	0.0043	10.57	0.15	46000	12000	729.7	7.4	73.4	1.1	29.4	3.1	335.8	6.1	344	22	260	150	-29.15
14	0.05349	0.00095	0.383	0.024	0.0506	0.0031	9.23	0.11	300000	120000	783.5	9.1	83.1	1.3	43	3.9	335.8	5.8	322	18	150	120	-123.87

	1							Final_				Appro		Appro		Appro		FinalA		FinalA		FinalA	
	Final206	Final206 238 In	Final2 07 2	Final2 07_2 35 In	Final207	Final207 206 In	Final_ U_Th Rati	U_Th _Rati o Int	Final206	Final206 204 In	Appro x U	x_U_ PPM_ Int2S	Appro x Th	x_Th_ PPM_ Int2S	Appro x Pb	x_Pb_ PPM_ Int2S	FinalA ge206	ge206 _238 Int2	FinalA ge207	ge207 _235 Int2	FinalA ge207	ge207 _206 Int2	
SA3_1	_238	t2SE	35	t2SE	206	t2SE	0	2SE	204	t2SE	PPM	E	PPM	E	PPM	E	_238	SE	_235	SE	_206	SE	
Z_Plesovice_					_				_								_		_		_		
1	0.0554	0.0012	0.397	0.026	0.052	0.0036	9.88	0.13	52000	23000	745.3	9.3	76.8	1.2	33.2	3	347.3	7.2	331	19	170	130	-104.29
Z_Plesovice_																							
2	0.0524	0.00096	0.416	0.023	0.0582	0.0032	9.4	0.1	54000	14000	787	9.7	82.2	1.2	61.8	3.9	329.1	5.9	351	17	410	120	19.73
Z_Plesovice_																							
3	0.0528	0.00095	0.384	0.022	0.0531	0.0031	9.92	0.12	51000	18000	745.7	8.8	76.4	1.2	39.5	3.2	331.5	5.8	326	16	230	120	-44.13
Z_Plesovice_																							
4	0.0555	0.0011	0.395	0.026	0.0522	0.0034	9.79	0.13	51000	17000	732	10	76	1.2	39.2	2.9	348.2	6.7	331	19	190	130	-83.26
Z_Plesovice_	0.05305	0.00000	0.004	0.00	0.05.40	0.0000	0.50	0.44	54000	42000	770	40	00 F		40.4	2.0	222.4		222		200		1100
5	0.05305	0.00089	0.394	0.02	0.0542	0.0028	9.58	0.11	54000	12000	//3	10	80.5	1.4	48.1	3.8	333.1	5.4	332	14	290	110	-14.86
Z_Plesovice_	0.05200	0.00000	0 207	0.021	0.0551	0.0020	0.64	0.1	50000	10000	770.0		70 5		40.5	2.5	222.2	F 4	226	45	210	110	7.52
D 7 Discovise	0.05308	0.00083	0.397	0.021	0.0551	0.0029	9.64	0.1	50000	19000	//0.8	8.8	79.5	1.1	48.5	3.5	333.3	5.1	330	15	310	110	-7.52
Z_Plesovice_	0.05202	0.00005	0 200	0.024	0.0522	0 0022	0.66	0.12	E2000	20000	720	10	75 /	1 2	41 E	2 0	222.1	6	226	17	220	120	11 02
7 Plesovice	0.05295	0.00095	0.566	0.024	0.0555	0.0055	9.00	0.12	52000	20000	720	10	75.4	1.5	41.5	5.0	555.1	0	520	17	250	120	-44.05
2_FIESOVICE_	0.05288	0 00097	0.406	0.025	0.0554	0.0035	0 72	0 11	52000	18000	772 /	Q 1	80	1 1	25.2	20	228.0	6	2/1	10	200	120	-12.07
	0.05588	0.00037	0.400	0.025	0.0554	0.0035	5.72	0.11	55000	18000	//2.4	0.1	80	1.1	55.2	2.9	330.9	0	341	10	300	130	-12.57
Q_FIESOVICE_	0.0549	0.001	0 409	0.027	0.0546	0.0036	10.07	0 14	51000	17000	722 4	9.6	74 1	13	28.3	27	344 7	63	342	20	260	130	-32 58
7 Plesovice	0.0345	0.001	0.405	0.027	0.0340	0.0050	10.07	0.14	51000	17000	/22.4	5.0	/4.1	1.5	20.5	2.7	544.7	0.5	342	20	200	150	52.50
10	0.05392	0 00091	0 386	0.021	0.0526	0 0027	9 61	0 11	52000	15000	766	10	78 4	13	40	31	338.4	56	327	15	230	110	-47 13
Z Plesovice	0.00002	0.00051	0.000	0.021	0.0520	0.0027	5101	0.11	52000	10000	,		,	1.0		0.1	00011	5.0	027	10	200		
11	0.0538	0.0009	0.382	0.021	0.052	0.003	8.92	0.11	54000	15000	826	11	90.4	1.4	49	3.5	338.3	5.6	325	15	200	120	-69.15
Z Plesovice	0.0000	0.0005	0.002	0.021	0.002	0.000	0.52	0.11	51000	10000	020		5011			0.0	00010	5.0	020	10	200	120	05.15
12	0.0529	0.001	0.368	0.025	0.0516	0.0035	11.47	0.15	51000	16000	722.8	9.1	72.2	1.2	24.8	2.6	332.1	6.2	311	18	150	130	-121.40
Z Plesovice																							
13 –	0.056	0.0011	0.427	0.03	0.0566	0.0041	9.61	0.13	52000	21000	771	10	82.2	1.4	33.4	3	351.1	6.9	351	21	290	140	-21.07
Z Plesovice																							
14	0.05302	0.0009	0.378	0.025	0.0518	0.0034	9.64	0.12	52000	17000	729.5	9.7	75	1.2	34	2.9	332.9	5.5	318	18	180	130	-84.94
Z_Plesovice_																							
15	0.05323	0.00089	0.383	0.02	0.053	0.0027	9.649	0.098	53000	16000	769.9	9.7	79	1.3	45.3	3.3	334.2	5.4	324	15	250	110	-33.68
Z_Plesovice_																							
16	0.05578	0.00097	0.391	0.02	0.0527	0.0028	9.22	0.1	50000	17000	791.7	8.9	84.3	1.2	53.8	3.5	349.8	5.9	334	15	240	110	-45.75
Z_Plesovice_																							
17	0.05242	0.00097	0.407	0.025	0.0581	0.0038	10.06	0.11	53000	12000	733.7	8.9	74.9	1.1	34.5	3	329.2	5.9	341	19	380	130	13.37
Z_Plesovice_																							
18	0.0536	0.0011	0.387	0.026	0.0536	0.0036	10.12	0.13	51000	19000	759	9.5	78.4	1.3	26.5	2.7	336.6	6.7	324	19	210	130	-60.29
Z_Plesovice_																							
19	0.05466	0.00099	0.41	0.027	0.0555	0.0038	9.53	0.12	52000	20000	730.7	9.9	76.4	1.2	28.1	2.4	342.9	6.1	340	19	280	130	-22.46
Z_Plesovice_																							
20	0.05397	0.00084	0.381	0.021	0.0528	0.003	9.75	0.1	51000	17000	733	11	75	1.3	52	3.3	338.7	5.2	323	15	220	110	-53.95
Z_Plesovice_			a						=						a								
21	0.05354	0.00087	0.413	0.019	0.05/1	0.0027	9.358	0.092	58000	19000	890.1	8.3	95.9	1.1	84.2	4.8	336.1	5.3	348	14	412	98	18.42
2_Plesovice_	0.0533	0.00000	0.070	0.022	0.0525	0.0000	10.05	0.44	10000	46000	6 4 2 F	0.6				2.0		5.0	24-	10	400	120	75 -0
22	0.0532	0.00092	0.372	0.022	0.0525	0.0032	10.06	0.11	49000	10000	642.5	8.6	64.8	1.1	37.7	2.9	334	5.6	317	16	190	120	-/5.79

Z_Plesovice_ 23	0.05288	0.00094	0.415	0.021	0.059	0.003	9.64	0.1 Final_	53000	18000	789.2	9.6 Appro	81.4	1.1 Appro	49.3	3.3 Appro	332.1	5.8 FinalA	351	16 FinalA	460	110 FinalA	27.80
SA4	Final206 _238	Final206 _238_In t2SE	Final2 07_2 35	Final2 07_2 35_In t2SE	Final207 _206	Final207 _206_In t2SE	Final_ U_Th _Rati o	U_Th _Rati o_Int 2SE	Final206 _204	Final206 _204_In t2SE	Appro x_U_ PPM	x_U_ PPM_ Int2S E	Appro x_Th_ PPM	x_Th_ PPM_ Int2S E	Appro x_Pb_ PPM	x_Pb_ PPM_ Int2S E	FinalA ge206 _238	ge206 _238 _Int2 SE	FinalA ge207 _235	ge207 _235 _Int2 SE	FinalA ge207 _206	ge207 _206 _Int2 SE	
2_Plesovice_ 1	0.0536	0.001	0.355	0.022	0.0513	0.0032	10.14	0.12	50000	11000	745.7	9.7	74	1.1	32	2.6	336.2	6.4	304	17	160	120	-110.13
2_Plesovice_ 2	0.0534	0.00099	0.442	0.024	0.0633	0.0036	8.88	0.11	58000	13000	763.8	9.3	86.6	1.2	55.5	3.4	335.2	6	367	17	560	120	40.14
Z_Plesovice_ 3	0.0537	0.0011	0.378	0.024	0.0528	0.0032	10.33	0.16	51000	13000	776	15	77.1	1.1	36.6	2.9	337	6.9	319	18	220	120	-53.18
Z_Plesovice_ 4	0.0542	0.0011	0.374	0.022	0.0531	0.0033	10.47	0.14	50000	12000	761	11	74.1	1.1	35.5	2.7	339.9	6.5	320	17	230	120	-47.78
Z_Plesovice_ 5	0.0537	0.001	0.428	0.025	0.0604	0.0036	8.94	0.11	47000	11000	745.9	9.3	83.3	1.1	52.6	3.5	336.8	6.3	355	18	470	120	28.34
Z_Plesovice_ 6	0.05368	0.00099	0.383	0.023	0.054	0.0033	10.46	0.12	55000	11000	738.5	8.3	71.65	0.98	30.4	2.7	337	6	323	17	250	120	-34.80
Z_Plesovice_ 7	0.05322	0.00097	0.404	0.023	0.0576	0.0034	9.31	0.12	49000	12000	783	10	87.4	1.4	42.6	3.2	334.1	5.9	341	17	380	120	12.08
Z_Plesovice_ 8	0.05374	0.00098	0.388	0.023	0.0541	0.0032	10.15	0.14	55000	12000	762	11	78	1.3	38	2.9	337.3	6	327	17	270	120	-24.93
Z_Plesovice_ 9	0.054	0.001	0.374	0.023	0.0525	0.0034	10.27	0.13	48000	11000	750	10	73.2	1.2	35.2	3	338.6	6.2	318	17	180	120	-88.11
Z_Plesovice_	0.054	0.001	0 492	0 027	0.0694	0 0041	8 53	0 11	52000	11000	765 7	9.2	87 5	12	73.8	4.8	338.8	6.2	403	19	740	130	54.22
Z_Plesovice_	0.053/3	0.00094	0 387	0.024	0.0543	0.0033	10.42	0.14	48500	9800	714.2	9	68.2	1 1	30.9	2.9	335 5	5.7	325	18	260	130	-29.04
Z_Plesovice_	0.05345	0.000	0.307	0.024	0.0543	0.0033	0.72	0.14	70000	12000	000 0	0.0	95.4	1.1	20.2	2.5	242.2	5.7	225	10	200	130	71.10
Z_Plesovice_	0.0545	0.001	0.384	0.024	0.0523	0.0032	9.73	0.11	70000	12000	742.1	9.9	85.4 76.7	1.5	39.2	3.3	342.2	5.1	325	10	200	120	-71.10
I3 Z_Plesovice_	0.05359	0.00096	0.407	0.024	0.0561	0.0032	9.79	0.12	50000	11000	742.1	8.4	/6./	1.1	39	2.7	336.4	5.9	342	18	350	120	3.89
14 Z_Plesovice_	0.0534	0.0011	0.384	0.021	0.0538	0.0031	9.63	0.11	53000	11000	753.6	8.6	78	1.1	36.6	3.3	335.4	6.5	327	15	280	110	-19.79
15	0.05336	0.00092	0.373	0.023	0.0524	0.0033	9.65	0.11 Final_	46000	11000	756.3	8.8 Appro	78	1.1 Appro	40.7	3.1 Appro	335	5.6 FinalA	317	17 FinalA	180	120 FinalA	-86.11
		Final206	Final2	Final2 07_2		Final207	Final_ U_Th	U_Th _Rati		Final206	Appro	x_U_ PPM_	Appro	x_Th_ PPM_	Appro	x_Pb_ PPM_	FinalA	ge206 _238	FinalA	ge207 _235	FinalA	ge207 _206	
SA5	Final206 _238	_238_In t2SE	07_2 35	35_In t2SE	Final207 _206	_206_In t2SE	_Rati o	o_Int 2SE	Final206 _204	_204_In t2SE	x_U_ PPM	Int2S E	x_Th_ PPM	Int2S E	x_Pb_ PPM	Int2S E	ge206 _238	_Int2 SE	ge207 _235	_Int2 SE	ge207 _206	_Int2 SE	
Z_Plesovice_ 1	0.0547	0.0027	-0.07	0.3	-0.021	0.031	10.56	0.53	80000	49000	755	13	78.2	3.3	-78	73	342	17	120	240	-4030	970	108.49
Z_Plesovice_ 2	0.053	0.0024	0.409	0.077	0.054	0.01	9.94	0.43	118500	6800	758	15	78.9	3.2	53	14	332	15	300	54	-240	310	238.33
Z_Plesovice_ 3	0.0549	0.0027	0.452	0.084	0.073	0.015	9.29	0.4	47400	2700	753	10	76.8	2.9	34	9.2	345	17	313	54	30	340	- 1050.00

Z_Plesovice_ 4	0.0526	0.0026	0.419	0.069	0.071	0.013	10.01	0.41	48000	2500	756	16	76.1	2.6	35	8.2	329	16	316	48	120	320	-174.17
Z_Plesovice_	0.0522	0.000	0.004	0.074	0.055	0.014		0.45			762		00.7		54.4	0	222		204	10		240	256.45
5 Z_Plesovice_	0.0532	0.003	0.381	0.071	0.055	0.011	9.46	0.45	68900	4100	/63	25	82.7	2.7	51.1	9	333	18	281	48	-130	310	356.15
6 7 Plesovice	0.0543	0.0027	0.392	0.069	0.059	0.01	9.65	0.44	49800	2800	753	24	77.4	2.6	39.3	8.9	340	17	293	47	-100	290	440.00
Z_Flesovice_ 7	0.0536	0.0028	0.372	0.067	0.0498	0.0098	9.39	0.4	38300	2400	757	17	77.3	2.6	35.4	7.8	336	17	273	46	-340	290	198.82
Z_Plesovice_ 8	0.0538	0.0026	0.382	0.07	0.051	0.01	9.23	0.43	77600	3300	743	21	75.2	2.8	39.5	8.3	337	16	286	50	-280	300	220.36
Z_Plesovice_	0.054	0.0000	0.000	0.000	0.0504	0.0004		0.47	65200	2000	770	24	04.6	2.0	24.2	0.5	220	4.6	202	40	400	200	277.00
9 Z_Plesovice_	0.054	0.0026	0.398	0.068	0.0534	0.0094	9.7	0.47	65300	3000	//2	21	81.6	2.9	34.3	8.5	338	16	302	48	-190	280	277.89
10 7 Plesovice	0.0534	0.0025	0.411	0.073	0.055	0.01	9.4	0.39	45500	2400	746	21	78.1	2.6	40	9.7	335	15	307	50	-120	290	379.17
11	0.0525	0.0026	0.382	0.062	0.0559	0.0095	9.97	0.53	52400	3000	758	23	75	2.6	40.3	8.2	329	16	296	44	-80	280	511.25
Z_Plesovice_ 12	0.0545	0.0036	0.387	0.064	0.058	0.01	9.18	0.43	58300	3800	754	22	79.7	2.8	36.9	8.2	340	22	289	44	-90	280	477.78
Z_Plesovice_	0.0552	0.0042	0 5 2 5	0.001	0.071	0.010	0.7	0.64	41200	2000	660	20	76.0	2.0	46.7	0.7	245	25	266		100	200	01.67
I3 Z_Plesovice_	0.0553	0.0043	0.525	0.091	0.071	0.012	9.7	0.64	41200	2900	669	30	76.9	2.9	46.7	8.7	345	25	300	55	180	300	-91.67
14 7 Plesovice	0.0481	0.0021	0.33	0.056	0.056	0.01	9.38	0.33	87900	3500	1080	22	132.5	4	57	12	303	13	268	43	-170	280	278.24
15	0.0586	0.0042	0.62	0.16	0.129	0.043	11.49	0.8	31800	2900	474	22	44	3	44	15	365	25	323	82	-330	420	210.61
Z_Plesovice_ 16	0.0571	0.0031	0.356	0.089	0.049	0.013	10.62	0.5	45000	2900	745	19	73.8	3.6	29	10	357	19	236	59	-690	340	151.74
Z_Plesovice_	0.0584	0 0029	0 424	0.085	0.052	0.011	0.83	0.4	66800	2700	979	22	104	45	22	11	265	19	202	57	-370	220	108.65
17	0.0584	0.0029	0.434	0.085	0.052	0.011	5.05	Final_	00800	3700	878	Appro	104	4.5 Appro	55	Appro	505	FinalA	255	FinalA	-370	FinalA	198.05
		Final206	Final2	Final2		Final207	Final_	U_Th Rati		Final206	Annro	x_U_ PPM	Annro	x_Th_ PPM	Annro	x_Pb_ PPM	FinalA	ge206 238	FinalA	ge207 235	FinalA	ge207 206	
	Final206	_238_In	07_2	35_In	Final207	_206_In	_Rati	o_Int	Final206	_204_In	x_U_	Int2S	x_Th_	Int2S	x_Pb_	Int2S	ge206	_Int2	ge207	_Int2	ge207	_Int2	
SA7	_238	t2SE	35	t2SE	_206	t2SE	0	2SE	_204	t2SE	PPM	E	PPM	E	PPM	E	_238	SE	_235	SE	_206	SE	
2_Plesovice_ 1	0.05394	0.00096	0.393	0.027	0.0537	0.0037	9.65	0.13	49000	27000	820	11	87.4	1.5	45.2	5.8	338.6	5.9	328	20	210	140	-61.24
Z_Plesovice_	0.05214	0 00096	0 206	0 022	0.0549	0 0022	0 75	0.12	56000	19000	715	0.2	72.8	1 /	25.1	27	222.6	5.9	225	17	320	120	-4.25
Z_Plesovice_	0.05514	0.00030	0.390	0.022	0.0549	0.0032	5.75	0.15	50000	19000	/15	5.2	72.0	1.4	55.1	5.7	555.0	5.0	333	17	520	120	-4.25
3 Z Plesovice	0.0537	0.001	0.392	0.025	0.0518	0.0033	9.66	0.12	48000	22000	783	10	80.4	1.4	40.1	3.4	337	6.2	329	18	180	130	-87.22
4	0.05402	0.00089	0.392	0.024	0.0525	0.0033	9.64	0.12	54000	23000	737.2	9.2	75.8	1.2	40	3.5	339.1	5.5	329	18	190	130	-78.47
Z_Plesovice_ 5	0.0541	0.001	0.398	0.025	0.0562	0.0036	9.73	0.12	52000	27000	717.3	9.2	72.3	1.2	37.2	3.5	339.5	6.2	335	18	330	130	-2.88
Z_Plesovice_	0.05296	0 00094	0 394	0 022	0.0565	0.0033	9.64	0.12	52000	30000	744 8	9.2	76	1 2	39.6	3.6	332.6	57	334	16	340	120	2 18
Z_Plesovice_	5.05250	0.00004	0.354	0.022	0.0505	5.0035	5.04	0.12	52000	30000	74.0	5.2	,0	1.2	55.0	5.0	552.0	5.7	554	10	540	120	2.10
7 Z Plesovice	0.0541	0.0011	0.391	0.024	0.0508	0.0032	9.64	0.12	47000	28000	760.9	9.9	77.7	1.3	39.9	3.4	339.2	6.5	330	18	160	120	-112.00
8	0.0536	0.00093	0.398	0.024	0.0529	0.0031	9.99	0.12	51000	20000	703.1	9.5	71.1	1.1	33.6	3.8	336.4	5.7	334	17	240	120	-40.17

2 Plessore 10 0.0543 0.0094 0.391 0.051 0.003 0.031 0.003 0.031
10 0.0343 0.004 0.031 0.03 0.03 0.01 0.03 0.03 0.01 0.03 0.03 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.003 0.01 0.01 0.003 0.01 0.01 0.003 0.01 0.003 0.01 0.01 0.003 0.004 0.01 0.001 0.001 0.01 0.003 0.01 0.003 0.004 0.01 0.001 0.003 0.004 0.01 0.003 0.004 0.01 0.001 0.003 0.004 0.01 0.003 0.004 0.01 0.003 0.004 0.01 0.000 0.003 0.000 0.000 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.010 0.004
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SA8 2.38 !258 35 !128 .206 !258 .204 !258 PPM E PPM E .238 SE .235 SE .206 SE Z.Plesovice 0.054 0.001 0.002 0.0017 0.0053 0.0017 0.0053 0.003 9.003 9.69 0.10 67000 753 13 78 1.6 39.8 3.8 33.58 6.7 33.5 19 20 20 1.0 1.0 2.0 2.0 1.0 1.0 2.0 1.0 1.0 2.0 1.0 1.0 2.0 1.0 1.0 2.0 1.0 1.0 2.0 1.0 1.0 1.0 2.0 1.0 1.0 2.0 1.0 1.0 2.0 2.0 1.0 1.0 1.0 1.0 3.0 3.0 3.0 3.0 3.0 1.0 1.0 1.0 1.0 1.0 1.0 3.0 3.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0<
2 Plesovice 0.054 0.001 0.402 0.027 0.0553 0.003 9.68 0.12 9700 6700 753 13 78 1.6 39.1 3.4 338.9 6.7 335 19 20 100 15.5 2 100 100 761.5 8.9 78.8 1.3 39.8 3.8 6.4 337 20 20 140 15.7 17.9 100 100 761.5 8.9 78.8 1.3 39.8 3.8 6.4 337 20 20 140 15.7 17.9 100 100 100 761.5 8.9 78.8 1.3 39.8 3.8 6.4 337 20 20 140 15.7 100 100 76.8 1.5 38.9 4.2 337.7 7.2 312 1 300 150 11.70 100 75.3 9.6 78.8 1.3 38.7 4.2 337.7 7.2 312 21 90 150 17.7 12 1.3 14.1 1.3 1.4 1.3 1.4 <
Z-Plesovice_1 0.0535 0.001 0.403 0.028 0.056 0.0039 9.69 0.13 6900 9100 761.5 8.9 78.8 1.3 39.8 3.8 335.8 6.4 337 20 290 140 -15.79 Z_Plesovice_1 0.0534 0.001 0.41 0.03 0.0568 0.0042 9.63 0.14 -400000 130000 749.2 9.3 77.6 1.3 37.9 4 335.1 6.4 339 21 300 150 -11.70 Z_Plesovice_1 0.0538 0.0012 0.37 0.029 0.0503 0.004 9.74 0.15 -5000 230000 751 10 76.8 1.5 38.9 4.2 337.7 7.2 312 21 90 150 -275.22 2.Plesovice_1 0.0538 0.0012 0.38 0.027 0.0528 0.0038 9.65 0.14 300000 27000 759.3 9.6 78.8 1.3 38.7 4.2 337.7 7.2 328 20 190 140 -78.42
2 0.0535 0.001 0.403 0.028 0.0056 0.0039 9.69 0.13 69000 761.5 8.9 78.8 1.3 39.8 3.8 335.8 6.4 337 20 290 140 -15.79 2_Plesorice 0.0534 0.01 0.41 0.03 0.0568 0.0042 9.63 0.14 -40000 13000 749.2 9.3 77.6 1.3 37.9 4 335.1 6.4 339 21 300 150 -11.70 2_Plesorice 0.0538 0.012 0.37 0.029 0.053 0.04 9.74 0.15 5000 759.3 9.6 78.8 1.3 38.9 4.2 337.9 7.2 312 21 90 150 -275.22 2_Plesorice 0.053 0.011 0.402 0.038 9.65 0.14 30000 757.3 9.6 78.8 1.3 38.7 4.2 339.9 7.2 328 20 190 140 -78.42 2_Plesorice 0.053 0.011 0.42 0.053
Z_Plesovice_ 0.0534 0.001 0.41 0.03 0.0568 0.0042 9.63 0.14 -40000 13000 749.2 9.3 77.6 1.3 37.9 4 335.1 6.4 339 21 300 150 -17.0 2_Plesovice_ 0.0538 0.0012 0.37 0.029 0.0503 0.004 9.74 0.15 -5000 230000 751 10 76.8 1.5 38.9 4.2 337.7 7.2 312 21 90 150 -275.22 Z_Plesovice_ 0.054 0.0012 0.387 0.027 0.058 0.038 9.65 0.14 30000 27000 759.3 9.6 78.8 1.3 38.7 4.2 339 7.2 328 20 190 140 -275.22 Z_Plesovice_ 0.0535 0.0011 0.402 0.33 0.04 9.67 0.14 180000 210000 757.3 9.4 78.8 1.3 41.2 4.6 335.9 6.6 333 22 200 150 52.68
S plesovice 0.054 0.012 0.37 0.029 0.053 0.004 9.74 0.15 -5000 230000 751 10 76.8 1.5 38.9 4.2 337.7 7.2 312 21 90 150 -275.22 Z-Plesovice_ 0.054 0.0012 0.387 0.027 0.0528 0.0038 9.65 0.14 30000 210000 757.3 9.4 78.2 1.3 41.2 4.6 335.9 6.6 333 22 220 150 -52.68 Z-Plesovice_ 0.054 0.0012 0.389 0.026 0.0037 9.66 0.14 2000 10000 75
4 0.0538 0.0012 0.37 0.029 0.0503 0.004 9.74 0.15 -5000 23000 751 10 76.8 1.5 38.9 4.2 337.7 7.2 312 21 90 150 -275.22 2_Plesovice_ 0.054 0.0012 0.387 0.027 0.0528 0.0038 9.65 0.14 30000 27000 759.3 9.6 78.8 1.3 38.7 4.2 339 7.2 328 20 190 140 -78.42 2_Plesovice_ 0.0535 0.0011 0.402 0.03 0.054 0.0042 9.71 0.14 18000 21000 757.3 9.4 78.2 1.3 41.2 4.6 335.9 6.6 333 22 220 150 -52.68 2_Plesovice_ 0.0536 0.0012 0.389 0.029 0.053 0.0037 9.66 0.13 50000 11000 749.6 9.7 76.9 1.4 38.2 4 336.5 6.2 329 20 190 140 -77.11
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6 0.0535 0.0011 0.402 0.03 0.0544 0.0042 9.71 0.14 18000 210000 757.3 9.4 78.2 1.3 41.2 4.6 335.9 6.6 333 22 220 150 -52.68 Z_Plesovice_ 0.054 0.0012 0.389 0.029 0.053 0.004 9.67 0.14 -2000 150000 756 10 78.4 1.4 37.9 3.9 339.1 7.3 324 21 180 150 -88.39 Z_Plesovice_ 0.0536 0.001 0.392 0.028 0.053 0.0037 9.66 0.13 50000 11000 749.6 9.7 76.9 1.4 38.2 4 336.5 6.2 329 20 190 140 -77.11 Z_Plesovice_ 0.0532 0.001 0.376 0.053 0.037 9.66 0.14 56000 84000 737 11 75.1 1.4 38.2 3.6 334.3 6.1 323 20 170 140 -96.65 2_Ples
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Z_Plesovice_ 9 0.0532 0.001 0.376 0.026 0.051 0.0036 9.66 0.14 56000 84000 737 11 75.1 1.4 38.2 3.6 334.3 6.1 323 20 170 140 -96.65 Z_Plesovice_ - - - - - - - - - - - - 96.65
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10 0.0535 0.001 0.391 0.028 0.0528 0.0037 9.87 0.13 1400 77000 756.7 8 77.6 1.1 38 3.1 336 6.2 326 20 190 140 -76.84
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11 0.05412 0.00093 0.389 0.023 0.0519 0.0031 9.4 0.11 122000 73000 820.1 9.4 92.5 1.3 48.7 3.6 339.7 5.7 327 17 180 120 -88.72 Z Plesovice
12 0.0535 0.0011 0.413 0.029 0.0562 0.0041 10 0.14 52000 45000 704.5 9.5 70.1 1.1 35.2 3.4 335.9 6.7 344 21 280 140 -19.96
Z_Plesovice_
13 0.05347 0.00096 0.399 0.028 0.0544 0.0039 9.62 0.12 48000 38000 760 10 78.7 1.3 37.2 3.9 335.7 5.9 332 20 240 140 -39.88 7 Plesovice
14 0.0535 0.0012 0.398 0.027 0.0543 0.0037 9.66 0.14 53000 36000 765 10 79.7 1.5 40.5 3.9 336.1 7.1 332 20 250 140 -34.44
Z_Plesovice_
15 0.0539 0.0011 0.388 0.027 0.0514 0.0036 9.74 0.13 56000 35000 753 10 77 1.4 37.4 3.9 338.5 6.9 324 20 140 140 -141.79
16 0.0537 0.001 0.374 0.028 0.0508 0.004 9.67 0.13 54000 36000 728 10 75 1.3 38.8 3.7 336.9 6.4 313 20 80 140 -321.13
Z_Plesovice_
17 0.0545 0.001 0.413 0.023 0.0544 0.003 9.64 0.13 51000 44000 796 11 84.4 1.5 40 3.5 341.9 6.2 347 17 300 120 -13.97
18 0.05304 0.00099 0.406 0.025 0.0551 0.0034 9.66 0.12 57000 42000 763.7 9.9 79.5 1.2 42.5 3.7 333 6.1 339 18 290 130 -14.83
Z_Plesovice_
19 0.0536 0.0011 0.386 0.027 0.0526 0.0036 9.77 0.14 52000 36000 730 10 73.9 1.4 35.2 3.6 336.1 6.7 326 20 180 140 -86.72
2_Presovice

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Z_Plesovice_ 21	0.0541	0.001	0.378	0.028	0.0501	0.0038	9.75	0.13	52000	33000	740.4	9.3	75.8	1.3	37.3	4	339.2	6.4	319	21	90	140	-276.89
2_Plesovice_ 22 7_Plesovice	0.05384	0.00098	0.394	0.026	0.0533	0.0036	9.55	0.12	34000	35000	792	10	83	1.2	45.2	4.4	338.6	6.1	332	19	210	140	-61.24
23 7 Plesovice	0.053	0.0011	0.366	0.025	0.0495	0.0034	9.84	0.14	61000	29000	728	9.2	73.2	1.3	34.8	3.8	332.8	6.6	311	19	110	130	-202.55
24	0.0539	0.001	0.413	0.029	0.0555	0.004	9.65	0.11 Final_	57000	31000	767	10 Appro	79.9	1.3 Appro	40.5	3.9 Appro	338.2	6.3 FinalA	344	21 FinalA	270	140 FinalA	-25.26
	Final206	Final206 238 In	Final2	Final2 07_2 35_In	Final207	Final207 206 In	Final_ U_Th Rati	U_Th _Rati o_Int			Appro x U	x_U_ PPM_ Int2S	Appro x Th	x_Th_ PPM_ Int2S	Appro x Pb	x_Pb_ PPM_ Int2S	FinalA	ge206 _238 Int2	FinalA	ge207 _235 Int2	FinalA	ge207 _206 Int2	
SA10 Z_Plesovice_	_238	t2SE	35	t2SE	_206	t2SE	0	2SE			PPM	E	PPM	E	PPM	E	_238	SE	_235	SE	_206	SE	
1 Z_Plesovice_	0.05377	0.00039	0.386	0.01	0.0537	0.0015	9.915	0.053			737.9	6.6	75.6	0.76	31.1	1.2	337.7	2.3	328.8	7.7	293	59	-15.26
2 Z_Plesovice_	0.05358	0.00038	0.408	0.01 0.009	0.0571	0.0015	9.603	0.045			757.4	7	79.93	0.87	44.2	1.5	336.6	2.4	346	7.4	430	56	21.72
3 Z_Plesovice_	0.05369	0.00038	0.378	7	0.0523	0.0014	9.699	0.047			795.4	8.3	82.27	0.96	35.9	1.4	337.3	2.3	323.2	7.1	247	55	-36.56
4 Z_Plesovice_	0.05368	0.00037	0.406	0.011 0.009	0.0567	0.0015	9.787	0.048			724.6	6.8	73.76	0.81	46.7	1.8	337.2	2.3	344	7.9	420	58	19.71
5 Z_Plesovice_ 6	0.05368	0.00035	3 0.408 1	7 0.009 2	0.0552	0.0014	9.595	0.049			796	8.2 7.6	84.63	0.96	42.0	1.4	337 1	2.2	346 5	6.8	338	51	2/ 59
Z_Plesovice_ 7	0.05366	0.00030	0.390	2 0.009 5	0.0574	0.0014	9.204	0.043			704.6	6.7	71 98	0.30	34.6	1.7	336.9	2.2	333.6	7.1	326	54	-3 34
Z_Plesovice_ 8	0.05369	0.00036	0.391 6	0.009 6	0.0524	0.0013	9.774	0.05			772	8.4	79.64	0.97	37.9	1.3	337.1	2.2	333.2	7	260	52	-29.65
Z_Plesovice_ 9	0.05369	0.00037	0.385 7	0.009 8	0.0535	0.0014	9.817	0.048			760.3	7.1	76.86	0.76	35.1	1.2	337.1	2.2	328.8	7.2	288	55	-17.05
Z_Plesovice_ 10	0.05365	0.00038	0.372 6	0.009 8	0.0528	0.0014	9.597	0.052			850.4	9.3	87.2	1	36	1.4	336.9	2.3	319.1	7.2	261	55	-29.08
Z_Plesovice_ 11	0.0537	0.00039	0.423	0.011	0.0563	0.0015	9.716	0.057 Final			725.7	5.9 Appro	75.4	0.76	42.6	1.5	337.1	2.4 FinalA	356.8	7.9 FinalA	398	58 EinalA	15.30
		Final206	Final2	Final2 07 2		Final207	Final_ U Th	U_Th Rati		Final206	Appro	x_U_ PPM	Appro	x_Th_ PPM	Appro	x_Pb_ PPM	FinalA	ge206 238	FinalA	ge207 235	FinalA	ge207 206	
SA21C	Final206 _238	_238_In t2SE	07_2 35	35_In t2SE	Final207 _206	_206_In t2SE	_Rati o	o_Int 2SE	Final206 _204	_204_In t2SE	x_U_ PPM	Int2S E	x_Th_ PPM	Int2S E	x_Pb_ PPM	Int2S E	ge206 _238	_Int2 SE	ge207 _235	Int2 SE	ge207 _206	Int2 SE	
Z_Plesovice_ 1	0.05362	0.0009	0.445	0.02	0.0609	0.0029	10.17	0.1	370000	170000	837	13	88.2	1.5	51.8	2.8	336.6	5.5	369	14	532	97	36.73
2_Plesovice_ 2 7_Plesovice	0.05361	0.00087	0.385	0.02	0.0527	0.0028	10.58	0.11	135000	74000	675.9	9.9	68.3	1.2	27.5	3	336.5	5.3	327	15	220	110	-52.95
3 Z Plesovice	0.05365	0.00081	0.373	0.014	0.0506	0.0018	9.045	0.079	102000	39000	832	14	89	1.7	49.7	2.6	336.8	5	319	11	178	75	-89.21
4	0.05367	0.00082	0.386	0.015	0.0523	0.002	9.128	0.078	54000	19000	755	11	77.8	1.2	51.1	2.9	336.9	5	329	11	243	80	-38.64

	1																						1
Z_Piesovice_	0.05385	0 00096	0 394	0.018	0.0534	0.0025	9 97	01	53000	16000	752	11	77 8	12	37	23	338	59	333	13	260	96	-30.00
Z Plesovice	0.000000	0.00000	0.001	0.010	0.0001	0.0025	5157	0.1	55000	10000	/52					2.0	000	5.5	000	10	200	50	50.00
6	0.05414	0.00091	0.376	0.019	0.0505	0.0025	9.92	0.1	44000	17000	756	14	78.1	1.6	29.9	2.2	339.8	5.5	320	14	141	99	-140.99
Z_Plesovice_																							
7	0.05343	0.00086	0.449	0.022	0.0601	0.0027	9.65	0.1	57000	20000	755	11	78	1.3	47.1	2.7	335.4	5.3	371	15	521	99	35.62
Z_Plesovice_																							
8	0.05317	0.00089	0.379	0.02	0.0517	0.0027	9.89	0.11	46000	17000	755	12	78	1.4	28.4	2.2	333.9	5.4	321	15	200	110	-66.95
Z_Plesovice_	0.05202	0.00004	0 270	0.010	0.0500	0.0000	0.72	0.11	F 4000	15000	75.4	10	70.4	1.0	20.0	2.2	220 5	5.2	222	45	170	100	00.12
9 7 Blocovico	0.05393	0.00084	0.379	0.019	0.0508	0.0026	9.73	0.11	54000	15000	/54	13	/8.1	1.6	28.8	2.2	338.5	5.2	323	15	170	100	-99.12
2_Plesovice_	0.05374	0 00083	0 386	0.018	0.0518	0 0024	10 13	0 11	93000	32000	755	11	77 9	13	29.2	21	337 3	51	327	13	197	95	-71 22
Z Plesovice	0.05574	0.00005	0.500	0.010	0.0510	0.0024	10.15	0.11	55000	52000	755		77.5	1.5	25.2	2.1	557.5	5.1	527	15	157	55	, 1.22
11	0.05358	0.00088	0.432	0.019	0.0583	0.0026	9.06	0.1	151000	48000	758	13	78.4	1.5	61.8	3	336.3	5.4	360	14	436	95	22.87
Z_Plesovice_																							
12	0.05399	0.00092	0.415	0.019	0.0554	0.0024	10.4	0.11	43000	31000	751	11	77.7	1.3	34.1	2.3	338.8	5.6	348	14	349	90	2.92
Z_Plesovice_																							
13	0.05369	0.00078	0.397	0.015	0.0537	0.002	9.847	0.086	-200000	200000	748	11	77	1.2	53.6	2.8	337.1	4.8	337	11	295	80	-14.27
Z_Plesovice_	0.0500	0.00076	0.000	0.017	0.0522	0.0000	0 4 0 7	0.070	420000	62000	007	10	06.0		67 7		220.2		227	40	222		52.20
14 7. Dissouries	0.0539	0.00076	0.386	0.017	0.0523	0.0023	9.197	0.079	138000	62000	827	10	86.2	1.2	67.7	3.3	338.3	4.7	327	12	222	91	-52.39
2_Plesovice_	0.05267	0 00080	0 282	0.021	0.0518	0 0020	10.27	0.11	56000	21000	652.2	07	66.8	1 2	26.8	2.1	226.0	5.4	272	15	100	110	-77 22
7 Plesovice	0.05507	0.00089	0.365	0.021	0.0518	0.0023	10.57	0.11	50000	31000	055.2	5.7	00.8	1.2	20.8	2.1	330.9	5.4	525	15	190	110	-77.52
16	0.05325	0.00086	0.381	0.016	0.0519	0.0022	9.416	0.09	26000	38000	917	15	95.1	1.8	46.2	2.9	334.4	5.3	324	12	226	87	-47.96
NIST 610																							

							Final_				Appro		Appro		Appro
			Final2			Final_	U_Th				x_U_		x_Th_		x_Pb_
	Final206	Final2	07_2		Final207	U_Th	_Rati			Appro	PPM_	Appro	PPM_	Appro	PPM_
Final206	_238_In	07_2	35_ln	Final207	_206_In	_Rati	o_Int			x_U_	Int2S	x_Th_	Int2S	x_Pb_	Int2S
_238	t2SE	35	t2SE	_206	t2SE	0	2SE			PPM	E	PPM	E	PPM	E
_				_		0.828								1060	
0.2469	0.0016	30.25	0.2	0.9097	0.0049	1	0.003			585.1	7.9	723	12	0	110
							0.003								
0.2453	0.0017	30.18	0.2	0.9095	0.0049	0.849	1			524.9	6.3	618.5	8.4	9980	120
						0.848	0.002							1765	
0.2456	0.0015	30.4	0.19	0.9097	0.005	2	9			677.8	6.2	830.2	7.9	0	110
						0.835	0.003							1192	
0.245	0.0017	30.36	0.21	0.9096	0.0049	4	1			709.3	9.7	913	14	0	280
							Final				Appro		Appro		Appro
			Final2			Final	U Th				хU		x Th		x Pb
	Final206	Final2	07 2		Final207	U Th	Rati		Final206	Appro	PPM	Appro	PPM	Appro	PPM
Final206	238 In	07 2	35 In	Final207	206 In	Rati	o Int	Final206	204 In	хÜ	Int2S	x Th	Int2S	x Pb	Int2S
238	t2SE	35	t2SE	206	t2SE	0	2SE	204	t2SE	PPM	Е	PPM	Е	PPM	Е
-				-			0.005	-						1143	
0.2506	0.0033	32.19	0.38	0.926	0.0077	0.771	5	11840	310	582	11	745	14	0	190
						0.774	0.005							1113	
0.2527	0.0032	32.04	0.34	0.9136	0.0084	6	3	17640	540	564	10	718	13	0	180
	Final206 _238 0.2469 0.2453 0.2456 0.2456 0.245 Final206 _238 0.2506 0.2527	Final206 Final206 _238 t2SE 0.2469 0.0016 0.2453 0.0017 0.2456 0.0015 0.245 0.0017 Final206 Final206 _238_ln t2SE 0.2506 0.0033 0.2527 0.0032	Final206 Final220 Final206 _238 10 _238 t2SE 35 0.2469 0.0016 30.25 0.2453 0.0017 30.18 0.2456 0.0015 30.4 0.2455 0.0017 30.36 Final206 _238_ln 07_2 2.238 t2SE 35 0.2455 0.0017 30.36 Final206 _238_ln 07_2 _238 t2SE 35 0.2506 0.0033 32.19 0.2527 0.0032 32.04	Final206 Final2 Final2 Final206 238 10 77.2 35.1n 238 t2SE 35 t2SE 0.2469 0.0016 30.25 0.2 0.2453 0.0017 30.18 0.2 0.2456 0.0015 30.4 0.19 0.2455 0.0017 30.36 0.21 Final206 238.1n 07.2 35.1n 1.2456 0.0017 30.36 0.21 Final206 238.1n 07.2 35.1n 1.238 t2SE 35 t2SE 0.2450 0.0017 30.36 0.21 Final206 238.1n 07.2 35.1n 1.258 35 t2SE 35 t2SE 0.2506 0.0033 32.19 0.38 0.2527 0.0032 32.04 0.34	Final206 Final2206 Final206 Final207 7_2 35_1n Final207 238 t2SE 35 t2SE _206 _2097 0.2469 0.0016 30.25 0.2 0.9097 0.2453 0.0017 30.18 0.2 0.9095 0.2456 0.0017 30.36 0.21 0.9096 Final206 _238_1n 07_2 35_1n Final207 0.2456 0.0017 30.36 0.21 0.9097 0.2456 0.0017 30.36 0.21 0.9096 Final206 _238_1n 07_2 35_1n Final207 238 t2SE 35 12SE _206 0.2506 0.0033 32.19 0.38 0.926 0.2527 0.0032 32.04 0.34 0.9136	Final206 Final2 Final207 Final207 Final207 Stal207 Tinal207 Stal207 Tinal207 O.0049 O.049 O.049 O.049 O.049 O.049 O.049 O.049 O.049 O.049 O.0049 O.0049 O.0049 O.0049 O.0049 O.005 O.0049 O.0049	Final206 Final2 Final207 U_Th Final206 _238_ln 07_2 35_ln Final207 _206_ln _Rati _238 t2SE 35 t2SE _206 t2SE 0 0.828 0.2469 0.0016 30.25 0.2 0.9097 0.0049 1 0.2453 0.0017 30.18 0.2 0.9095 0.0049 0.848 0.2456 0.0015 30.4 0.19 0.9097 0.005 2 0.2456 0.0017 30.36 0.21 0.9096 0.0049 4 Final206 Final206 Final2 07_2 Final207 206_ln _Rati 1 1 0.2455 0.0017 30.36 0.21 0.9096 0.0049 4 Final206 Final206 Final2 07_2 Final207 206_ln Rati 238 t2SE 35 t2SE 206 12SE 0 0.2506 0.0033	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						

							0.785	0.005							1102	
G_NIST610_3	0.2521	0.0034	31.93	0.41	0.9141	0.0085	1	4	31930	930	551.7	9.6	695	13	0	180
							0.866	0.006								
G_NIST610_4	0.249	0.0033	30.81	0.35	0.9019	0.008	8	9	-3910	99	445.7	7.6	508.5	9.1	7960	140
							0.868									
G_NIST610_5	0.2481	0.003	30.88	0.35	0.9063	0.0076	7	0.006	-3588	82	441.9	7.5	501.7	9	7770	120
							0.880									
G NIST610 6	0.2471	0.0033	30.62	0.35	0.9047	0.008	8	0.006	-3260	81	440.3	6.8	491.3	7.9	7570	120
								Final_				Appro		Appro		Appro
				Final2			Final	U Th				хU		x Th		x Pb
		Final206	Final2	07 2		Final207	U Th	Rati		Final206	Appro	PPM	Appro	PPM	Appro	PPM
	Final206	238 In	07 2	35 In	Final207	206 In	Rati	o Int	Final206	204 In	хU	Int2S	x Th	Int2S	x Pb	Int2S
SA21C	238	t2SE	35	t2SE	206	t2SE	0	2SE	204	t2SE	PPM	Е	PPM	Е	PPM	Е
					_		0.929	0.008								
G NIST610 1	0.2417	0.0032	31.39	0.46	0.914	0.014	3	5	7590	340	437	5.9	476.1	6.9	5823	74
							0.929	0.007								
G NIST610 2	0.2501	0.0036	32.08	0.48	0.905	0.015	6	5	9180	320	401.3	5.5	426.7	6.3	7189	92
							0.930	0.008								
G NIST610 3	0.2403	0.0033	30.92	0.4	0.909	0.012	1	1	14950	720	304.8	4.3	338.9	5.1	7409	97
							0.924	0.007								
G NIST610 4	0.2462	0.0032	31.64	0.39	0.905	0.012	1	2	19640	900	399.1	5.8	417	6.6	7960	100
							0.917	0.007								
G NIST610 5	0.2418	0.0034	31.36	0.39	0.913	0.012	1	8	29000	1200	312.5	3.7	349.2	4.4	7827	93
								0.007								
G NIST610 6	0 2476	0.0032	32 02	0 42	0 913	0.012	0 917	9	44900	1900	511 6	71	581 7	9	8260	110
							0.905	-						-		
G NIST610 7	0 2437	0.0034	31 18	0 41	0 904	0.013	4	0.007	51700	2500	402.6	5	427 7	57	8065	92
							0.906	0.007				-				
G NIST610 8	0.2494	0.0031	32.08	0.39	0.911	0.011	5	5	40000	1700	458.7	6.4	525.1	8.2	8490	110
							0.904	0.007								
G NIST610 9	0.2445	0.0035	31.1	0.4	0.903	0.012	5	2	24800	1100	428.8	6.2	451.8	7.1	8350	120
G NIST610 1							0.898	0.007								
0	0.2481	0.0031	32.08	0.39	0.918	0.012	5	9	14990	530	468.1	6.8	546.3	8.7	8680	130
G NIST610 1							0.896	0.007								
1	0.2438	0.0033	31.49	0.41	0.916	0.012	3	8	11100	430	457.7	6.1	508.2	7.4	8680	110
G NIST610 1							0.894	0.007								
2	0.2491	0.0032	31.64	0.41	0.902	0.012	6	1	8740	300	476.5	7	555.8	8.7	8820	120
G NIST610 1								0.006								
3	0.2488	0.0035	31.87	0.4	0.913	0.013	0.889	9	7470	320	548.9	7.3	635.6	9.1	8890	110
G NIST610 1							0.888	0.007								
4	0.2493	0.0032	31.66	0.4	0.906	0.013	9	8	6780	270	424.9	6.5	456.4	7.7	9040	130
								Final				Appro		Appro		Appro
				Final2			Final	UTh				хU		x Th		x Pb
		Final206	Final2	07 2		Final207	UTh	Rati		Final206	Appro	PPM	Appro	PPM	Appro	PPM
	Final206	238 In	07 2	35 In	Final207	206 In	Rati	o Int	Final206	204 In	хU	Int2S	x Th	Int2S	x Pb	Int25
SA3.1	238	t2SE	35	t2SE	206	t2SE	0	2SE	204	t2SE	PPM	E	PPM	E	PPM	E
							0.824	0.007				-		-		-
G NIST610 1	0.2487	0.0038	31.11	0.43	0.91	0.012	5	1	15750	540	650	11	811	14	9860	140
						-	-			-						-

	1															
C NUCTCAR 2	0.2450	0.0000	20.04	~ • •	0.005	0.04	0.853	0.006	4050	100	502.0		576.0	0.0		
G_NIS1610_2	0.2458	0.0036	30.64	0.44	0.905	0.01	2	1	4950	180	502.6	8	576.2	9.6	9990	140
	0 2447	0.0025	20.67	0.42	0.012	0.011	0.859	0.006	65.00	220		0	E04	0.6	0700	150
G_M31010_5	0.2447	0.0055	50.07	0.42	0.912	0.011	0 860	/	0380	220	506.5	0	594	9.0	9700	150
	0 2428	0.0035	20 54	0.41	0.012	0.01	0.809	0.007	7250	260	525.8	7 9	614	10	0620	140
0_101010_4	0.2430	0.0035	30.34	0.41	0.912	0.01	0 883	0.007	7250	200	525.0	7.0	014	10	3030	140
G NIST610 5	0 2447	0.0036	30.64	0.43	0 913	0.011	5	8	4150	140	456 5	69	513 5	85	9540	130
0_11151010_5	0.2447	0.0050	50.04	0.45	0.515	0.011	0.887	0.006	4150	140	450.5	0.5	515.5	0.5	5540	150
G NIST610 6	0.2498	0.0038	31.06	0.45	0.908	0.011	4	6	5830	190	434	6.2	485.9	7.7	9380	130
								0.006								
G NIST610 7	0.2434	0.0031	30.38	0.4	0.913	0.011	0.867	7	8170	290	509.5	7.8	584.9	9.7	9440	140
							0.848	0.006								
G_NIST610_8	0.2446	0.0035	30.25	0.42	0.901	0.01	1	9	7610	270	580.7	8.5	687	11	9200	130
							0.838	0.006								
G_NIST610_9	0.2436	0.0034	30.07	0.42	0.899	0.01	3	3	8280	290	641	10	787	13	9090	130
G_NIST610_1							0.848	0.006								
0	0.2445	0.0034	30.53	0.39	0.916	0.012	3	2	5460	190	498.9	7.5	581	10	8940	120
G_NIST610_1							0.834	0.006								
1	0.243	0.0033	30.28	0.43	0.913	0.011	4	8	3950	140	429.2	6.5	497.5	8.2	9050	130
G_NIST610_1								0.005								
2	0.2432	0.0034	30.28	0.4	0.911	0.011	0.777	9	5830	180	530.7	8.1	765	13	8830	120
G_NIS1610_1	0 2 4 2 4	0.0025	20.24	0.42	0.014	0.01	0.767	0.005	0070	220	c20.2	0.4	05.0		0070	120
3 C NIETC10 1	0.2431	0.0035	30.24	0.43	0.914	0.01	5	5	9070	320	630.3	9.4	850	14	8870	120
	0 2422	0 0027	20.24	0.20	0.019	0.011	0.819	0.006 6	75.90	270	E00 7	0.1	722	12	0000	120
4 G NIST610 1	0.2425	0.0057	50.24	0.59	0.918	0.011	0 880	0 006	7560	270	596.7	9.1	122	12	8800	120
5	0 2435	0 0034	29 97	04	0 909	0.011	0.880	5	4890	170	451.4	69	506.6	85	8790	140
G NIST610 1	0.2455	0.0034	25.57	0.4	0.505	0.011	0 893	0.006	4000	1/0	451.4	0.5	500.0	0.5	0/50	140
6	0.2451	0.0033	30.02	0.44	0.906	0.011	5	9	4340	140	405.1	6.2	444.4	7.3	8710	130
G NIST610 1				••••			0.839	0.006				•				
7	0.2431	0.0034	30.14	0.43	0.914	0.01	9	9	4340	130	513.1	7.8	620	10	8570	130
G_NIST610_1							0.811	0.006								
8	0.2451	0.0037	29.84	0.39	0.903	0.011	5	9	7360	250	650.5	9.2	840	14	8570	120
G_NIST610_1							0.830	0.006								
9	0.2446	0.0034	30.25	0.38	0.917	0.011	5	9	8610	280	589.9	9	709	11	8470	120
G_NIST610_2							0.880	0.007								
0	0.247	0.0034	29.99	0.41	0.901	0.011	8	2	4610	140	395.9	6.5	447.1	7.9	8440	130
G_NIST610_2							0.908	0.006								
1	0.2435	0.0034	29.85	0.41	0.914	0.011	9	8	3300	100	317.5	4.9	351.1	5.8	8350	120
G_NIST610_2							0.904	0.006								
2	0.2439	0.0035	29.65	0.4	0.9035	0.0092	6	6	4420	140	408.3	5.8	458.5	7.2	8310	120
G_NISI610_2	0.246	0.0026	20.12	0.4	0.012	0.011	0.874	0.007	5150	100	475 4	6.0	F 4 2 0	0.2	8200	120
э	0.246	0.0030	30.12	0.4	0.913	0.011	2	1 Einal	2120	190	475.4	0.9 Appro	542.8	J.Z Appro	8200	120
				Final?			Final	II Th				v II		v Th		v Ph
		Final206	Final2	07 2		Final207	U Th	Rati		Final206	Annro	PPM	Appro	PPM	Annro	PPM
	Final206	238 In	07 2	35 In	Final207	206 In	Rati	o Int	Final206	204 In	x U	Int2S	x Th	Int2S	x Pb	Int2S
SA4	238	t2SE	35	t2SE	206	t2SE	0	2SE	204	t2SE	PPM	E	PPM	E	PPM	E
					-				-							

1																
G_NIST610_1	0.2396	0.0036	28.66	0.37	0.913	0.012	0.969 3	0.009 4	2275	95	444.2	6.6	460.7	7.4	5511	76
G NIST610 2	0 2418	0.0036	29.05	0 36	0 913	0.012	0.968 4	0.007 8	2133	84	405 9	6	419 7	6.8	5780	85
0_11101010_2	0.2410	0.0050	25.05	0.50	0.515	0.012	0.967	0.009	2155	04	405.5	0	415.7	0.0	5700	05
G_NIST610_3	0.2433	0.0035	29.14	0.39	0.908	0.012	5	1	2143	83	391	5.6	413.7	6.9	5890	80
G NIST610 4	0.2419	0.0034	29.13	0.38	0.912	0.013	0.955	0.008	2094	81	403.6	5.2	433.9	6.1	6052	72
							0.948	0.007								. –
G_NIST610_5	0.2449	0.0036	29.25	0.39	0.901	0.011	1	9	2033	79	422	5.5	443.9	6.6	6103	81
G NIST610 6	0 2444	0.0038	29.61	0 39	0 916	0.013	0.941	0.007	2020	84	427 1	63	459 3	71	6207	84
0_11151010_0	0.2444	0.0050	25.01	0.55	0.510	0.015	0.935	0.007	2020	04	427.1	0.5	455.5	/.1	0207	04
G_NIST610_7	0.2436	0.0032	29.36	0.39	0.907	0.013	3	7	1898	70	402.3	5.8	444.2	7.1	6221	80
	0 2440	0.0024	20.9	0.41	0.011	0.012	0.927	0.007	1000	75	400.2	го	445 1	7.2	6206	01
G_10121010_8	0.2449	0.0034	29.8	0.41	0.911	0.013	5	° 0.008	1909	/5	400.2	5.8	445.1	7.5	0390	81
G_NIST610_9	0.2461	0.0035	29.45	0.39	0.899	0.012	0.927	1	1943	76	426.2	6	462.2	6.9	6585	83
G_NIST610_1							0.929	0.008						_		
0 G NIST610 1	0.2455	0.0035	29.89	0.42	0.911	0.011	9	3	1870	76	444.4	6.3	464.2	7	6559	88
1	0.2466	0.0032	30.22	0.38	0.913	0.011	0.910	4	1812	65	464.9	5.8	499.2	6.7	6806	81
G_NIST610_1							0.901	0.007								
2	0.2434	0.0036	29.84	0.4	0.912	0.012	1	1	1752	74	427.5	6.4	485.3	7.7	6781	94
G_NIS1610_1 3	0 2456	0.003	30.2	0.39	0 912	0.011	0.884	0.006 9	1712	63	129 1	5 9	1Q1 /	77	7090	95
G NIST610 1	0.2450	0.005	50.2	0.55	0.512	0.011	0.875	0.007	1/12	05	425.4	5.5	451.4	7.7	7050	55
4	0.2468	0.0035	30.24	0.43	0.908	0.012	2	6	1687	59	430.8	5.7	491.1	7.3	7310	110
G_NIST610_1	0.2462	0.0022	20.24	0.20	0.01	0.012	0.864	0.006	1620	64	404 F	6.5	402.7	7.0	7400	110
5	0.2462	0.0032	30.21	0.39	0.91	0.012	0	4 Final	1639	64	421.5	6.5 Annro	483.7	7.8 Annro	7400	Appro
				Final2			Final_	U_Th				x_U_		x_Th_		x_Pb_
		Final206	Final2	07_2		Final207	U_Th	_Rati		Final206	Appro	PPM_	Appro	PPM_	Appro	PPM_
CAF	Final206	_238_In	07_2	35_In	Final207	_206_In	_Rati	o_Int	Final206	_204_In	x_U_	Int2S	x_Th_	Int2S	x_Pb_	Int2S
5A5	_238	t2SE	35	t25E	_206	t25E	0	25E	_204	t25E	PPIVI	E	PPIVI	E	1452	E
G_NIST610_1	0.2335	0.0075	41.8	1.2	0.944	0.038	0.814	0.016	-57000	35000	486.2	6.9	613	9.9	0	280
G_NIST610_2	0.2405	0.0063	31.04	0.87	0.911	0.033	0.798	0.014	11200	8900	556.5	7.8	673.6	9.6	9830	200
G_NIST610_3	0.2358	0.007	25.88	0.71	0.898	0.03	0.814	0.014	25000	11000	614.8	8.8	681.2	9.4	8010	140
G_NIST610_4	0.2355	0.0068	25.1	0.79	0.898	0.035	0.817	0.015	1100	3600	502.6	7.7	601.3	9.3	6770	120
G_NIST610_5	0.2378	0.0071	26.07	0.82	0.891	0.034	0.806	0.016	8800	5500	440.8	7	541	8.2	6170	120
G_NIST610_6	0.2339	0.0065	29.06	0.86	0.92	0.034	0.807	0.016	8200	7800	455.9	6.1	544.8	9	6280	110
G_NIST610_7	0.2373	0.006	30.7	0.86	0.894	0.03	0.802	0.015	3100	3700	512.9	7.3	581	8.8	6840	140
G NIST610 8	0.236	0.0066	31.43	0.98	0.919	0.031	0.807	0.016	10800	5500	476.1	7.2	533.6	8.7	6880	140

G_NIST610_9	0.2326	0.0073	29.89	0.96	0.916	0.036	0.81	0.015	18100	9500	374.3	5.4	456	6.7	6170	110
0 0	0.2377	0.0072	28.71	0.85	0.902	0.034	0.807	0.017	5000	3400	365.3	5.8	428.4	6	5504	97
1 G_NIST610_1	0.2318	0.0073	28.58	0.93	0.943	0.036	0.815	0.017	8000	4200	341	5.2	396.2	5.1	4704	84
2 C_NIST610_1	0.2265	0.0063	26.67	0.79	0.912	0.033	0.806	0.015	7100	4400	411.9	6.5	488.5	8.4	5630	110
G_NIST610_1	0.2306	0.0064	27.26	0.8	0.893	0.031	0.81	0.013	-500	3000	418.4	6.8	563.8	8.5	6370	110
4	0.2255	0.0076	28.8	1.2	0.918	0.04	0.827	0.019 Final	11200	8800	767	13 Appro	960	16 Appro	9510	240 Appro
SA7	Final206 _238	Final206 _238_In t2SE	Final2 07_2 35	Final2 07_2 35_In t2SE	Final207 _206	Final207 _206_In t2SE	Final_ U_Th _Rati o	U_Th _Rati o_Int 2SE	Final206 _204	Final206 _204_In t2SE	Appro x_U_ PPM	x_U_ PPM_ Int2S E	Appro x_Th_ PPM	x_Th_ PPM_ Int2S E	Appro x_Pb_ PPM	x_Pb_ PPM_ Int2S E
G_NIST610_1							0 022	0.006							1115	
G_NIST610_2	0.2456	0.0034	30.62	0.42	0.916	0.01	0.852	6 0.006	11700	430	611.1	8.4	729	11	1113 0 1132	150
G_NIST610_3	0.2481	0.0035	31.88	0.48	0.909	0.011	0.836 0.845	6 0.006	11450	450	597.8	8.6	706	11	0 1145	160
G_NIST610_4	0.2494	0.0037	31.45	0.41	0.899	0.011	7 0.838	5 0.007	12140	420	590.9	8.1	693	11	0 1124	160
G_NIST610_5	0.2454	0.0036	29.64	0.37	0.916	0.011	8 0.845	2 0.006	13480	450	583.2	8.6	680	11	0 1074	170
G_NIST610_6	0.2477	0.0038	29.93	0.39	0.907	0.012	1 0.843	7 0.005	14960	550	579.3	8.9	670	11	0 1008	160
G_NIST610_7	0.2484	0.0035	31.51	0.41	0.901	0.011	1 0.864	8 0.006	13910	480	563.2	8.6	655	10	0	150
G_NIST610_8	0.2481	0.0036	31.68	0.41	0.918	0.011	4	6 Final_	10080	340	544.8	7.8 Appro	632.8	9.6 Appro	9220	130 Appro
	5in - 1200	Final206	Final2	Final2 07_2	5 :1207	Final207	Final_ U_Th	U_Th _Rati	Fig. 120 C	Final206	Appro	x_U_ PPM_	Appro	x_Th_ PPM_	Appro	x_Pb_ PPM_
SA8	_238	_238_In t2SE	07_2 35	t2SE	_206	_206_In t2SE	_Kati 0	2SE	_204	_204_In t2SE	x_U_ PPM	E	x_In_ PPM	E	X_PD_ PPM	E
G_NIST610_1	0.2408	0.0036	29.74	0.45	0.915	0.012	0.800	7	33900	1300	465.7	7.1	581	9.6	8520	120
G_NIST610_2	0.2415	0.0035	29.7	0.36	0.904	0.012	0.783	0.006 5	50000	1700	547.4	8.1	697	11	1033	140
G_NIST610_3	0.2438	0.0036	30.14	0.43	0.903	0.011	0.775	5	86600	3100	639	10	818	14	1240	180
G_NIST610_4	0.246	0.0034	30.81	0.44	0.912	0.011	0.749	4	156900	5600	720	12	949	16	1459 0 1512	220
G_NIST610_5	0.2439	0.0035	30.42	0.43	0.907	0.013	0.742	2	208700	7800	731	11	982	16	1313	210
C NUCTCAD C	0.0454	0.0004	20 70	0.00	0.044	0.040	0.737	0.005	470700	5000	705			46	1504	24.0
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G_NIS1610_6	0.2451	0.0034	30.79	0.39	0.911	0.012	9 0 744	5	1/2/00	5900	/35	11	994	16	0 1490	210
G_NIST610_7	0.243	0.0034	30.59	0.44	0.906	0.011	8	9	121300	4900	733	11	983	17	0	230
G_NIST610_8	0.2451	0.0034	30.97	0.4	0.91	0.011	6	0.006	77000	2700	703	11	909	15	0	200
G_NIST610_9	0.2444	0.0035	30.94	0.41	0.912	0.012	0.784 9	0.006 2	54300	1800	610.7	9.5	763	13	1114 0	170
G_NIST610_1 0	0.2426	0.0033	31.26	0.41	0.927	0.011	0.820 2	0.006 3	40900	1600	510	8.2	622	10	9330	140
G_NIST610_1								0.007								
1 G NIST610 1	0.2436	0.0033	30.81	0.4	0.908	0.012	0.881 0.821	6 0.006	31900	1200	480.3	7.6	579	10	8760 1022	130
2	0.241	0.0033	30.31	0.41	0.903	0.01	8	3	26470	940	570.5	8.9	698	11	0	150
G_NIS1610_1	0 2402	0.0033	30.82	0.4	0 923	0.011	0.771	0.006 4	23030	820	656	10	842	14	1268	180
G_NIST610_1	0.2402	0.0035	30.02	0.4	0.525	0.011	0.754	0.005	23030	020	050	10	042	14	1394	100
4	0.2411	0.0033	30.5	0.37	0.908	0.011	8	9	23020	900	686	10	906	14	0	210
G_NIST610_1	0.0405	0.0004	20.00	0.07	0.000	0.044	0.750	0.006	24700	750	702	4.0	000	45	1408	200
5 G NIST610 1	0.2425	0.0034	30.68	0.37	0.908	0.011	8 0 770	8	21700	750	703	10	929	15	0 1286	200
6	0.2446	0.0035	30.82	0.4	0.906	0.012	5	0.006	21370	760	662	11	849	14	0	190
G_NIST610_1							0.793	0.005							1170	
7	0.2444	0.0032	30.5	0.38	0.895	0.011	1	4	21710	720	583.3	8.6	745	11	0	160
G_NIST610_1	0.242	0.0024	20.07	0.44	0.010	0.011	0.793	0.006	22420	050	575.0	0.0	722		1186	170
8 G NIST610 1	0.242	0.0034	30.87	0.44	0.916	0.011	3 0 770	1 006	22420	850	5/5.8	8.0	/33	11	0 1393	170
9	0.247	0.0034	31.33	0.4	0.911	0.01	5	3	21850	750	649.8	9.5	833	13	0	200
G_NIST610_2							0.762	0.006							1477	
0	0.2475	0.0033	31.01	0.42	0.9	0.011	8	3	22340	760	687	10	892	15	0	220
G_NIST610_2	0 2422	0.0025	21 24	0.4	0.026	0.012	0.759	0.005	21610	910	680	10	001	15	1432	210
G NIST610 2	0.2433	0.0035	51.24	0.4	0.920	0.012	0.760	0.006	21010	810	085	10	501	15	1352	210
2	0.2482	0.0034	31.57	0.42	0.91	0.011	4	1	19920	710	671	12	885	16	0	210
G_NIST610_2							0.747	0.005							1377	
3 C NISTG10 2	0.2486	0.0031	31.29	0.39	0.902	0.011	7	9	18470	650	692	11	910	14	1228	200
4	0.2455	0.0034	31.31	0.37	0.915	0.011	0.779	0.006	16050	510	633.7	9.8	808	13	1238	180
								Final_				Appro		Appro		Appro
		F: 1000	5: 10	Final2		5. 1207	Final_	U_Th				x_U_		x_Th_		x_Pb_
	Final206	238 In	Final2	07_2 35_ln	Final207	Final207	U_IN Rati	_Rati			Appro	PPIVI_ Int2S	Appro	PPIM_ Int2S	Appro	Int2S
SA10	238	_238_111 t2SE	35	t2SE	206	t2SE	0	2SE			PPM	E	PPM	E	PPM	E
	-				-		0.874	0.003								
G_NIST610_1	0.2437	0.0014	29.65	0.16	0.9098	0.005	9	4			451.4	4.9	525	6.6	6781	64
	0 2414	0.0014	20.42	0.17	0 0097	0.0055	0.876	0.003			150 F	E /	525	7	7225	77
2_0101010_2	0.2414	0.0014	29.43	0.17	0.9087	0.0055	7 0,876	1 0.003			430.5	5.4	525	/	1225	//
G_NIST610_3	0.24	0.0014	29.27	0.17	0.9111	0.0052	9	2			454.2	5.4	516.5	6.9	7445	79

C NUCTC10 4	0.242	0.0014	20.10	0.17	0.0005	0.005	0.873	0.003			440 C		507.2	6.0	7650	02
G_NIS1610_4	0.242	0.0014	29.18	0.17	0.9085	0.005	ı 0.872	2 0.003			449.6	5.5	507.2	6.9	7658	82
G_NIST610_5	0.2425	0.0014	29.41	0.17	0.9095	0.0048	7	1			456.2	5.3	514.4	6.7	7856	81
G_NIST610_6	0.2448	0.0014	29.95	0.17	0.9101	0.0049	0.871 9	0.003			465.8	5.4	537.1	7	7986	82
G_NIST610_7	0.2425	0.0014	30.57	0.17	0.9097	0.005	0.869	0.003			477.2	5.4	553.8	7.1	8063	82
G_NIST610_8	0.2445	0.0013	30.19	0.17	0.9095	0.0049	0.865	0.002 9			494.6	6.1	568.2	7.9	8084	91
G_NIST610_9	0.2426	0.0014	28.94	0.16	0.9093	0.0048	0.862	0.003			529.5	6.2	603.5	7.9	8061	87
G_NIST610_1 0	0.211	0.0012	26.83	0.16	0.9098	0.0046	0.862 7	0.003 1			607.2	7.8	708	10	8143	95
G_NIST610_1	0 1 9 4 9	0.001	24.04	0.15	0.01	0.005	0.859	0.002			606 E	74	022	10	0000	70
G_NIST610_1	0.1040	0.001	24.94	0.15	0.91	0.005	0.859	5			080.5	7.4	052	10	8008	78
2	0.1844	0.0011	24.94	0.14 5ipal2	0.9093	0.0046	5 Final	0.003 Final_			713	7.7 Appro	866	11 Appro	8263	83 Appro
		Einal206	Einal 2			Einal207	Filiai_	D_III Poti		Einal206	Appro		Appro		Appro	
	Final206	238 In		35 In	Final207	206 In	Bati		Final206	20/1 In		Int2S	x Th	Int2S	v Ph	Int2S
SA21C	238	_230_111 +25F	35	+2SE	206	_200_111 +25F		25F	204	_204_111 +25F	A_O_	F		F		F
JAZIC	_230	LZJL	35	LZJL	_200	LZJL	0 916	0.006	_204	LZJL	FFIVI	L	FFIVI	L	FFIVI	L
G_NIST610_1	0.2489	0.0034	29.65	0.37	0.8717	0.0081	2	6	10970	290	610	12	772	17	8170	130
G_NIST610_2	0.2511	0.0034	29.83	0.35	0.8683	0.0076	0.908	0.000 7	18680	470	563.7	9.3	659	11	8760	130
G_NIST610_3	0.2526	0.0033	29.91	0.36	0.8641	0.0085	0.901	9	-14120	340	496.4	7.5	560.4	8.6	8650	120
G_NIST610_4	0.2505	0.0031	29.92	0.31	0.8668	0.0076	0.876 9	0.006 1	-4104	88	387.6	6.8	410.6	7.4	8870	140
G NIST610 5	0.2494	0.0031	30.01	0.34	0.8711	0.0075	0.858 5	0.005 8	-4262	99	517.1	8.7	613	10	8960	140
							0.839	0.005								
G_NIST610_6	0.2502	0.0029	30.42	0.33	0.8771	0.0076	6 0.827	9 0.005	-5900	160	620	11	763	14	9020	150
G_NIST610_7	0.2511	0.0029	30.25	0.34	0.8676	0.0074	1 0.808	9 0.005	-6460	160	677	11	814	13	9330	140
G_NIST610_8	0.249	0.003	30.15	0.33	0.8714	0.0079	3	3	-6130	140	700	11	879	14	9570	150
G_NIST610_9	0.2501	0.0033	30.43	0.35	0.8757	0.0081	0.802	0.005 9	-5300	120	684	11	852	14	9540	140
G_NIST610_1							0.803	0.005								
0	0.2477	0.0032	30.19	0.36	0.876	0.0076	1	7	-8020	200	619	10	808	13	9590	140
G_NIS1610_1							0.806	0.006								
1	0.2483	0.0032	30.28	0.36	0.8772	0.0078	6	1	16190	400	592.2	9.8	688	12	9640	150
	0.2485	0 0022	20.2	0.36	0.8761	0 0070	0.810 C	0.005	11520	260	502	10	764	14	0270	150
∠ G_NIST610_1	0.2405	0.0052	50.2	0.50	0.0701	0.0079	0.825	+ 0.005	11330	200	392	10	704	14	9370	130
3	0.2491	0.0032	30.26	0.32	0.8783	0.0082	3	3	-224000	11000	387.3	6.9	486.8	8.7	9810	150

Appendices

i																
G_NIST610_1							0.841	0.005								
4	0.2495	0.003	30.34	0.33	0.882	0.0076	6	5	-15110	370	350.7	5.8	394.5	7.1	9890	160
G_NIST610_1							0.846									
5	0.2496	0.0034	30.18	0.37	0.8797	0.0087	7	0.006	-13500	340	436.6	6.4	514.3	7.5	9720	150
G_NIST610_1							0.850	0.005							1017	
6	0.2492	0.003	30.34	0.33	0.8871	0.0076	8	4	-12670	290	535.3	7.5	660.8	9.2	0	150

6.3 Appendix 3

6.3.1 Palaeocurrents

Palaeocurrent data is measured from cross bedding at localities during sample collection and analysis. Measurements are taken to provide additional context to the study, however it is now understood that individual measurements likely form parts of larger structures such as accretionary bars and are not representative of the regional flow direction.

Palaeoflow	Locality	GPS
270°	SA20	N57.40596 W005.68389
180°	Log 4	In log section
140°	SA18	In log section
320°	Log 15	In log section
270°	Log 11	In log section
240°	SA15	In log section
270°	SA14	In log section
290°	SA13	N57.40806 W005.68418
240°	Log 3	N57.40762 W005.68536
180°	SA21	N57.46629 W005.78862
270°	SA23	N57.41926 W005.76290
135°	SA24	N57.41926 W005.60925